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SSD-TDR-62-127 - Volume II

INFRARED TRANSMISSION STUDIES

FINAL REPORT, VOLUME II

THE INFRARED ABSORPTION OF WATER VAPOR

P. J. Wyatt

V. R. Stull

G. N. Plass

Contract No. AF 04(695)-96 Project No. 4479-730F

as an extension to

Contract No. AF 19(604)-7479
Project No. 4479
Task No. 447904

20 September 1962



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Prepared for

SPACE SYSTEMS DIVISION
AIR FORCE SYSTEMS COMMAND
Los Angeles, California

as an extension to work sponsored by

GEOPHYSICS RESEARCH DIRECTORATE
AIR FORCE CAMBRIDGE RESEARCH LABORATORIES
Office of Aerospace Research
United States Air Force
Bedford, Massachusetts

AERONUTRONIC DIVISION FORD MOTOR COMPANY

Newport Beach, California

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ABSTRACT

The infrared absorption of water vapor has been calculated over a wide r age of path length, pressure, and temperature from 1000 to $10,000\,\mathrm{cm^{-1}}$. The results are presented in extensive tables which give the transmission over intervals of $2.5\,\mathrm{cm^{-1}}$ at wave numbers below 3400 cm⁻¹. The average transmission over intervals of 20, 50, and $100\,\mathrm{cm^{-1}}$ is given over the complete frequency range. The calculated data representing the intensity, position, and number of spectral lines in a given frequency interval is tabulated in a form which is useful for transmission calculations. All lines from all isotopic species having an intensity greater than 10^{-8} of the strongest line in an absorption region were included in the calculation. The quasi-random model for the representation of band spectra is discussed in detail. Among its features are the possibility of representing the absorption by a series of lines which are arranged neither at random nor in a regular way.

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SECTION 1

INTRODUCTION

The amount of infrared radiation which is transmitted through the earth's atmosphere is determined largely by the behavior of two molecules: water vapor and carbon dioxide. In this report a method by which the spectral transmission of water vapor has been calculated over a wide range of infrared frequencies is described. The results which were calculated on high speed digital computers are presented in the form of extensive tables. A companion report (SSD-TDR-62-127 - Volume III) presents similar data for carbon dioxide.

The most extensive transmission tables which have been previously calculated are those of Ballard, Larmore, and Passman. 1 Their tables cover a wavelength range from 0.3 to 7.0 μ at intervals of 0.1 μ . The results are for one temperature (300°K) and one pressure (1 atmosphere). They assumed that the transmission is given by the Elsasser model. In particular, they used the error function approximation for the Elsasser model which is of limited accuracy at the higher pressures and shorter path lengths. Furthermore, the Elsasser model itself is a poor representation of the water vapor spectrum because the individual lines are not arranged with the regularity required by this model.

Tables of water vapor transmissions averaged over 20 cm⁻¹, 50 cm⁻¹, and 100 cm⁻¹ are presented respectively in three groups. Entries for the 20 cm⁻¹ averages are presented every 10 cm⁻¹ from 1000 cm⁻¹ to 10,000 cm⁻¹. The 50 cm⁻¹ and 100 cm⁻¹ average entries

¹ S. S. Ballard, L. Larmore, S. Passman, Fundamentals of Infrared for Military Application, The Rand Corporation, R-297, March 31, 1956 (C).

are presented every 25 cm⁻¹ and 50 cm⁻¹ respectively in the same frequency range. These tables contain results for three different temperatures (300°K, 250°K, and 200°K) with entries for each temperature at seven pressures and fifteen amounts of $\rm H_2O$. The range of temperatures, pressures and path lengths cover the range of values which occur in the earth's atmosphere.

Tables of the transmission at intervals of 2.5 cm⁻¹ from 1000 cm⁻¹ to 3400 cm⁻¹ are also presented. These calculations were carried out using the quasi-random model which is capable of representing the spectral transmission of molecular gases quite accurately. A detailed description of this model is given in Section 3.

In Section 2 the molecular structure of $\rm H_2O$ is described together with the rotational and vibrational motions. The intensities and frequencies of the spectral lines are described.

SECTION 2

MOLECULAR STRUCTURE OF WATER VAPOR

2.1 VIBRATIONAL ANALYSIS

The water molecule is a non-linear molecule with three non-degenerate eigen-vibrations, two of which are symmetric and the other antisymmetric. The vibrational potential constants have been measured to second order. The vibrational energy to this order is given by

$$G_{o}(v_{1}, v_{2}, v_{3}) = \sum_{i=1}^{3} \omega_{i}(v_{i}^{+\frac{1}{2}}) + \sum_{i=1}^{3} \sum_{j>i} x_{ij}(v_{i}^{+\frac{1}{2}})(v_{j}^{+\frac{1}{2}})$$
(1)

where the constants ω_i , x_{ij} are listed in Table 1. G_o is the vibrational energy in cm⁻¹ and v_i are the vibrational quantum numbers. The data for the main isotopic species HHO¹⁶ (abundance 0.998) were obtained by Darling and Dennison.²

¹G. Herzberg, Infrared and Raman Spectra (D. Von Nostrand Company, Inc., New York, 1945).

²B. T. Darling and D. M. Dennison, Phys. Rev. <u>57</u>, 128 (1940).

TABLE 1
VIBRATIONAL CONSTANTS

Isotope	нно ¹⁶	нно ¹⁸	нно ¹⁷	HD0 ¹⁶
ω ₁ (cm ⁻¹)	3825.32	3816.82	3820.52	2824.32
ω ₂	1653.91	1647.21	1650.41	1440.21
ω ₃	3935.59	3919.69	3927.19	3889.84
*11	- 43.8	- 43.6	- 43.7	- 43.4
*12	- 20.0	- 19.9	- 19.9	- 8.6
*13	-155.0	-154.0	-154.5	- 13.1
*22	- 19.5	- 19.3	- 19.4	- 11.8
*23	- 19.8	- 19.6	- 19.7	- 20.1
*33	- 46.8	- 45.9	- 46.1	- 82.9

For the species $\rm HH0^{18}$ (abundance .002) and $\rm HH0^{17}$ (abundance .0004) the constants were calculated directly from the relations 1

$$\omega_{3}^{2} = \frac{1}{4\pi^{2}c^{2}} \left(\frac{1}{m(H)} + \frac{2\sin^{2}\alpha}{m(0)} \right) 8.520 \times 10^{5}$$

$$\omega_{1}^{2} + \omega_{2}^{2} = \frac{1}{4\pi^{2}c^{2}} \left(\frac{14.690\times10^{5} - 6.140\times10^{5}\sin\alpha}{m(H)} + \frac{21.232\times10^{5}\cos^{2}\alpha}{m(0)} \right)$$
(3)

$$\omega_1^2 \omega_2^2 = \frac{1}{16 \pi^4 c^4} \left(\frac{2m(H) + m(0)}{[m(H)]^2 m(0)} \quad 33.824 \times 10^5 \cos^2 \alpha \right) \tag{4}$$

and

$$x_{y}^{(isotope)} = x_{y}^{(isotope)} \frac{\omega_{i}^{(isotope)} \omega_{j}^{(isotope)}}{\omega_{i} \omega_{j}}$$
 (5)

where m(H) and m(O) are the masses (in grams) of the hydrogen and oxygen atoms respectively and $2\alpha=105^{\circ}$ is the angle between the H atoms at the position of the O atom. The numerical constants in Eqs. (2 - 4) and the value of α are obtained from the measured values of ω_{i} for HHO¹⁶. The constants for the species HDO (abundance 3×10^{-4}) were obtained by Benedict, Gailar and Plyler. The other isotopic species of water are not sufficiently abundant to be considered here.

For many molecules accidental degeneracies occur when two or more vibrational states have the same symmetry type and nearly the same energy (see Chapter II.5c of reference 1 or SSD-TDR-62-127 - Volume III). This situation does not occur in H_2O for any of the fundamental vibrational states but does occur for the states (002) and (200) and for all subsequent pairs of states $(v_1 - 2, v_2, v_3 + 2)$ and (v_1, v_2, v_3) . For the CO_2 molecule, which is considered in SSD-TDR-62-127 - Volume III, this resonance occurs between the fundamental state (100) and the state (020). Furthermore for CO_2 the perturbation associated with the resonance is produced by the third order terms in the potential while for H_2O the first contribution comes from the fourth order terms. Thus the effect is less significant for H_2O than for CO_2 . Darling and Dennison have shown that the off-diagonal elements in the vibrational energy matrix for H_2O are given by

$$W_{v_1-2,v_2,v_3+2}^{v_1,v_2,v_3} = \frac{\gamma}{2} \sqrt{v_1(v_1-1)(v_3+1)(v_3+2)}$$
 (6)

where γ = 74.4 cm⁻¹. For the species HDO, $2\omega_1 \neq 2\omega_3$, but

 $^{^3}$ W. S. Benedict, N. Gailar and E. K. Plyler, J. Chem. Phys. $\underline{24}$, 1139 (1956).

 $2\omega_2\approx\omega_1$, thus the resonance occurs between the states (v₁ + 1, v₂ - 2, v₃), (v₁, v₂, v₃). Benedict, Gailer and Plyler³ have shown that for HDO

$$w_{v_1+1, v_2-2, v_3}^{v_1, v_2, v_3} = \frac{\gamma}{2} \sqrt{(v_1+1)v_2(v_2-1)}$$
 (7)

where $\gamma = 26.1 \text{ cm}^{-1}$.

The elements of the vibrational energy matrix can be evaluated from Eqs. (1) and (6) or (7). The energies of the vibrational level are the eigenvalues of this matrix. A calculation of the vibrational energies has been programmed for the IBM 709 computer. The vibrational energies have been obtained in this manner for all four isotopic species up to the level (013). Levels of higher energy than this were not considered because for the temperatures of interest ($\leq 300^{\circ}$ K) only the levels (000) and (010) are significantly populated. Furthermore, the vibrational transitions between (010) and all levels higher than (013) correspond to frequencies greater than 10,000 cm⁻¹ which is beyond the frequency range considered in the current study.

2.2 ROTATIONAL ANALYSIS

In regard to rotation the water molecule is an asymmetric top molecule since its three principal moments of inertia are different. For such a molecule the rotational energies cannot be expressed as simple functions of the rotational quantum numbers. I, Unlike the symmetric rotator there are no rotational degeneracies in the energy levels of the asymmetric rotator. In addition there is no "good" quantum number comparable to the component of angular momentum about the molecular axis of the symmetric top molecule. Thus the spectrum of rotational energy levels which is associated with each vibrational level cannot be described by an analytic expression.

For a given asymmetric molecule an equivalent symmetric top molecule is defined as one for which the two smaller moments of inertia are equal. This moment is taken to be the arithmetic average of the two smaller moments of the asymmetric molecule. In order to describe the rotational energy spectrum of an asymmetric molecule it has been customary to use the equivalent symmetric top molecule, with its good

quantum numbers and analytic energy expressions, as an approximation. 1,4 It is clear that this is permissible only if the asymmetry is slight. For H₂0, which is quite asymmetric, the equivalent symmetric top approximation cannot in general be used to obtain the correct rotational structure. However, in the present study, the exact details of the rotational spectrum are not needed. The detailed arrangement of the spectral lines within a finite frequency interval is not needed, if the number and intensity of the lines in the interval is known. Thus the symmetric top approximation has an application here for the calculation of positions and intensities of the weaker spectral lines. However, it is clear that there will be a lower limit on the size of the frequency interval which may be used. This point is discussed in more detail in section 2.3.

In the present calculation of water vapor transmission the actual asymmetric lines were used for the strongest lines in the lower portion of the frequency range considered. The equivalent symmetric top approximation was used only for the weak lines in this portion of the spectrum and for the frequency range above 3400 cm⁻¹ where theoretical calculations of the actual water vapor spectrum are not available. This aspect of the calculations is discussed in detail in section 2.3.

It can be shown that for a symmetric top molecule the rotational energy is given by $^{\mbox{\scriptsize l}}$

$$F_{v}(J,K) = \overline{B}_{v_{2}} J(J+1) + (B_{v_{1}} - \overline{B}_{v_{2}})K^{2}$$
 (8)

where F_V , B_{V_1} , \overline{B}_{V_2} are all measured in cm⁻¹, J is the total angular momentum quantum number which takes on the values K, K + 1, ..., and K is the component of angular momentum about the symmetry axis. If the symmetric top is used as an approximation for an asymmetric molecule, then the rotational constant B_{V_2} is

$$\overline{B}_{v_2} = \frac{1}{2} (B_{v_2} + B_{v_3}) \tag{9}$$

⁴P. C. Cross, R. M. Hainer and G. W. King, J. Chem. Phys. $\underline{11}$, 27 (1943); Ibid. $\underline{12}$, 210 (1944).

where $\mathbf{B}_{\mathbf{V},\mathbf{j}}$ are the rotational constants of the asymmetric molecule given by $^{\mathbf{j}}$

$$B_{v_n} = B_{e_n} - \sum_{m=1}^{3} \alpha_{nm} (v_m + \frac{1}{2})$$
 (10)

where $B_{e_n} = \frac{h}{8\pi^2 c I_n^e}$, n = 1,2,3 and I_n^e are the principal moments of

inertia corresponding to the equilibrium position of the vibrating molecule. The constant α_{nm} describes the effect of variation of the moments of inertia caused by the vibration. The integer n refers to the 3 principal axes of rotation and m refers to the 3 modes of vibration.

The numerical values of the rotational constants have been determined by Benedict, Gailar and Plyler³ and from the isotopic formulas

$$B_{e_n}^{\text{(isotope)}} = B_{e_n} \begin{pmatrix} 3 \\ 77 \\ m=1 \end{pmatrix}^{2/3}$$
 (11)

and

$$\alpha_{nm}^{(isotope)} = \alpha_{nm}(\rho_n)^3$$
 (12)

where $\rho_n = \frac{\omega_n}{\omega_n}$ (isotope) . This data is given in Table 2.

TABLE 2
ROTATIONAL CONSTANTS

Species	нно ¹⁶	нно ¹⁸	нно ¹⁷	ндо ¹⁶
Constant (cm-1)			• • • • • • • • • • • • • • • • • • • •	
$^{\mathtt{B}}\mathbf{v}_{1}$	27.379	27.1910	27.2790	22.6906
B _{v2}	22.0550	11.9722	12.0109	7.8398
α ₁₁	0.750	0.745	0.747	0.253
α 21	-2.941	-2.905	-2.922	-1.798
α ₃₁	1.253	1.238	1.245	1.087
$\overline{\alpha}_{12}$ +	0.2199	0.2185	0.2191	0.1544
\overline{a}_{22} +	-0.0104	-0.0103	-0.0104	-0.3800
a ₃₂ +	0.1113	0.1099	0.1106	0.0503

 $[\]overline{\alpha}_{n_2} = \frac{1}{2}(\alpha_{n_2} + \alpha_{n_3})$, which corresponds to using Eq. (9) directly.

2.3 INFRARED SPECTRUM

The infrared spectrum of water vapor consists of spectral lines corresponding to transitions between various vibration-rotation energy levels. The frequency of a given line ω , is proportional to the difference in the vibrational plus rotational energy of the final

and initial states. The intensity of a line can be characterized by the integrated absorption per unit pressure given by 5

$$S = \frac{8\pi^3}{3hc} \omega \frac{N}{Qp} \exp \left[-\frac{E_{vR}}{kT} \right] | M |^2 \left[1 - \exp(-\frac{h\omega}{kT}) \right]$$
 (13)

where N is the number of molecules per unit volume, Q is the partition function, p is the pressure, M is the dipole matrix element corresponding to the transition, and $E_{\rm VR}$ is the vibrational plus rotational energy of the initial state.

The selection rules which govern allowed transitions for a triatomic asymmetric molecule, such as H_20 , are given by Herzberg. For the molecular species HHO there are just two types of rotational transitions allowed. These correspond to the so-called parallel (ΔK = 0) and perpendicular (ΔK = $\frac{1}{2}$ 1) transitions of a symmetric top molecule. Bands made up of transitions of one of these types approach as limits the parallel or perpendicular bands of the equivalent symmetric top molecule. They also have the same general structure. For an asymmetric molecule such as HDO, a given vibrational band will contain rotational transitions of both types. The corresponding band of the equivalent symmetric top molecule will be a hybrid band containing both ΔK = 0 and ΔK = $\frac{1}{2}$ 1 transitions. (The vibrational bands of HHO molecules are not hybrid bands.) The familiar rotational selection rule ΔJ = 0, $\frac{1}{2}$ 1, applies to all transitions.

In addition to the transition frequency ω , the matrix element M cannot be expressed explicitly in terms of "good" quantum numbers for an asymmetric top molecule. Thus the expression for the integrated absorption, Eq. (13) is quite untractable. On the other hand, Eq. (13) becomes relatively simple for the symmetric top molecule. In fact for the temperatures of interest here the interaction of vibration and rotation may be neglected in the matrix element M. Furthermore at infrared frequencies, exp $\left[-\frac{h\omega}{kT}\right] << 1$. Taking these simplifications into account, Eq. (13) for a symmetric top molecule reduces to

$$S_{VKJ}^{V'K'J'} = C_{V}^{V'} \frac{\omega_{VKJ}^{V'K'J'}}{\omega_{V}^{V'}} \exp \left[\frac{hcF_{V}(J,K)}{kT}\right] \quad S(J,K)$$
 (14)

where $\omega \frac{v', K', J'}{v', K, J}$ is the frequency of the line, $\omega \frac{v'}{v}$ is the vibrational

S. S. Penner and A. Thomson, Tech. Rep. No. 25, Contract No. Nonr-220(03) NR 015401, Guggenheim Jet Propulsion Center, Calif. Inst. Tech.

frequency, i.e. the difference between the vibrational energies of the final and initial states, $F_{\mathbf{V}}(J,K)$ is the rotational energy of the initial state given by Eq. (8), S(J,K) are the squares of the pure rotational matrix elements given by I

$$S(J,K) = \begin{cases} \frac{(J+2 \pm K)(J+1 \pm K)}{2(J+1)} & \Delta J = +1 \\ \frac{(J+1 \pm K)(J \pm K)(2J+1)}{2J(J+1)} & \Delta J = 0 \end{cases}$$

$$\frac{(J-1 \pm K)(J \pm K)}{2J} \qquad \Delta J = -1$$

and

$$S(J,K) = \begin{cases} \frac{(J+1+K)(J+1-K)}{J+1} & \Delta J = +1 \\ \frac{(2J+1)K^2}{J(J+1)} & \Delta J = 0 \end{cases}$$

$$\frac{(J+K)(J-K)}{J} \qquad \Delta J = -1$$

and the amplitude $C_{V}^{V'}$ is given by

$$C_{\mathbf{v}}^{\mathbf{v'}} = \frac{8 \pi^3}{3 \text{hc}} \quad \omega_{\mathbf{v}}^{\mathbf{v'}} \quad \frac{N}{Qp} \quad \exp \left[-\frac{\text{hcG}(\mathbf{v})}{kT}\right] \quad |R_{\mathbf{v}}^{\mathbf{v'}}|^2$$
 (17)

where G(v) is the vibrational energy of the initial state and $R_{V}^{V^{'}}$ is the purely vibrational matrix element.

Thus it follows that the amplitude $C_V^{V'}$ for a particular vibrational transition at a particular temperature is related to that of any other vibrational transition at another temperature by

$$C_{v}^{v'}(T) = \frac{\left|R_{v}^{v'}\right|^{2}}{\left|R_{v*}^{v'**}\right|^{2}} C_{v*}^{v'**}(T_{o}) \frac{N(T)Q(T_{o})}{N(T_{o})Q(T)} \exp \left[\frac{hcG(v*)}{kT_{o}} - \frac{hcG(v)}{kT}\right] (18)$$

It can be assumed that N(T) \sim (p/T) and the partition function is given by 1

$$Q(T) = \int_{i=1}^{3} \left(1 - \exp\left[-\frac{h\omega_{i}^{0}}{kT}\right]^{-1} \exp\left[-\frac{hcB_{e_{2}}^{\frac{1}{2}}B_{e_{3}}^{\frac{1}{2}}}{4kT}\right] X$$

$$\left[\frac{\pi(kT/hc^{3})}{B_{e_{1}}^{B}B_{e_{2}}^{B}B_{e_{3}}}\right]^{\frac{1}{2}} - 1 + \frac{1}{12}\left[1 - \frac{B_{e_{2}}^{\frac{1}{2}}B_{e_{3}}^{\frac{1}{2}}}{B_{e_{1}}}\right] \frac{hcB_{e_{2}}^{\frac{1}{2}}B_{e_{3}}^{\frac{1}{2}}}{kT} \exp\left[-\frac{hcG(0)}{kT}\right]$$
(19)

where ω_1^o are the frequencies of the three fundamental vibrational modes. This expression neglects the interaction of vibration and rotation and assumes $B_{V_n} \approx B_{e_n}$. These assumptions are reasonable for T $\simeq 300^{\circ}$ K.

If the matrix elements $R_V^{V'}$ could be calculated, the intensity of any spectral line could be deduced from Eq. (14). However, quantum mechanical expressions for $R_V^{V'}$ have never been derived for polyatomic molecules such as H_2O ; therefore a semi-empirical solution is required. In this regard, absolute measurements are available of the integrated transmission over large frequency intervals in the infrared. These measurements demonstrate that the vibrational bands of water vapor

J. N. Howard, D. F. Burch and D. Williams, Sci. Rep. #1, AF19(604)-516 The Ohio State University, Dec. 1954.

occur in essentially seven separable groups in the frequency range between 1000 and 10,000 cm⁻¹. Each group is characterized by one or two relatively intense vibrational transitions of HHO¹⁶ which dominate all the isotopic and higher order bands. Thus integrated transmission measurements cannot be made for a given vibrational band individually, since such measurements necessarily include all of the weaker bands in a given group which occur in the same frequency interval with the most intense transitions. These groups are identified with the most intense band in a frequency interval and by the wavelength which describes the approximate location of the peak absorption. Using the latter designation, the seven groups of the water vapor spectrum are $6.3\,\mu$, $3.2\,\mu$, $2.7\,\mu$, $1.87\,\mu$, $1.38\,\mu$, $1.1\,\mu$, and $.94\,\mu$. The complete list of member vibrational transitions of these groups is given in Table 3.

The measurements can be used to determine one normalization constant for each of the seven groups by comparison of the calculated integrated transmission over the transitions in the group for a particular value of pressure and amount of water vapor with measured values of this quantity. Details of this normalization procedure are given in section 4. After this constant is determined. Eq. (18) may be used to calculate the intensity of each vibrational transition in the group provided the ratio of relative intensities $(|R_{v}^{v'}|^{2}/|R_{v}^{v'}|^{2})$ is known for the transitions. These relative intensities have been measured by several high resolution studies 3,7,8,9 for many of the vibrational transitions. For other bands the relative intensities may be inferred from the two empirical rules discussed by Herzberg: 1 (1) the relative intensity of a difference band, e.g. $(010) \rightarrow (100)$, is approximately equal to the Boltzmann factor for the initial state times the relative intensity of the corresponding summation band, e.g. $(000) \rightarrow (110)$, (2) the relative intensity of bands such as $(010) \rightarrow (110)$ is approximately equal to the Boltzmann factor for the initial state times the relative intensity of corresponding fundamental bands such as (000) - (100). Furthermore bands which correspond to the accidental resonance discussed previously can be assumed to have the same intensity, e.g. $(000) \rightarrow (200)$ and $(000) \rightarrow (002)$. The relative intensities of all the bands for the species HHO^{16} are given in Table 3 for $T = 300^{\circ}K$.

W. S. Benedict, Bull. Amer. Phys. Soc. <u>23</u>, 54 (1948).

⁸W. S. Benedict, Phys. Rev. <u>74</u>, 1246 (1948).

W. S. Benedict, H. H. Claassen, and J. H. Shaw, J. Res. Nat. Bur. Stand. <u>49</u>, 91 (1951).

TABLE 3 VIBRATIONAL TRANSITIONS OF HHO¹⁶ AT T = 300°K

Group	Transition	Relative Intensity	<u> </u>
6.3 μ	000 → 010	1.00	± 1
	010 → 020	9.6×10^{-4}	± 1
	010 → 100	$1.9 \times 10^{-5(9)}$	† 1
	010 → 001	9.6×10^{-5}	0
3.2μ	000 → 020	1.00	<u>†</u> 1
	010 → 030	4.8×10^{-4}	± 1
2.7μ	000 → 001	1.00	0
	000 → 100	.10(3)	± 1
	010 → 011	4.8×10^{-4}	0
	010 → 110	4.8×10^{-5}	<u>†</u> 1
1 . 87 μ	000 → 011	1.00	0
	000 → 110	2.0×10^{-2} (7)	<u>†</u> 1
	000 → 030	6.7×10^{-3}	± 1
	010 → 021	4.8×10^{-4}	0
	010 → 120	9.6 x 10 ⁻⁶	± 1
	010 → 040	3.2×10^{-6}	† 1
	010 → 101	4.8×10^{-4}	0
	010 → 200	3.8 x 10 ⁻⁵	<u>†</u> 1
	010 → 002	5.8 x 10 ⁻⁵	± 1
		2-12	

TABLE 3 (Continued)

1

Group	Transition	Relative Intensity	
1.38µ	000→ 101	1.00	0
	000 → 021	1.0×10^{-1} ⁽⁷⁾	0
	000 → 120	1.3×10^{-2} ⁽⁷⁾	± 1
	000 → 040	4.3×10^{-3}	± 1
	000 → 200	2.5×10^{-1} ⁽⁷⁾	± 1
	000 → 002	2.5×10^{-1}	<u>†</u> 1
	010→ 111	4.8×10^{-4}	0
	010 → 031	4.8×10^{-5}	0
	010→ 130	6.2×10^{-6}	<u>†</u> 1
	010 → 050	2.1×10^{-6}	± 1
	010 → 210	1.2×10^{-4}	<u>+</u> 1
	010 → 012	1.2×10^{-4}	<u>†</u> 1
1.1μ	000 → 111	1.00	0
	000 → 031	3.3×10^{-1} (8)	0
	000 → 130	6.0×10^{-2} (8)	<u>†</u> 1
	000 → 050	2.0×10^{-2}	‡ 1
	000 → 210	8.0×10^{-2}	± 1
	000 → 012	1.2 x 10 ⁻¹⁽⁸⁾	‡ 1
	010 → 121	4.8×10^{-4}	0
	010 → 041	1.6×10^{-4}	0

TABLE 3 (Continued)

Group	Transition	Relative Intensity	△ K
1.1μ	010 → 140	2.9 x 10 ⁻⁵	<u>† 1</u>
	010 → 060	9.6×10^{-6}	± 1
	010 → 220	3.8×10^{-5} (8)	† 1
	010 → 022	5.8 x 10 ⁻⁵⁽⁸⁾	± 1
	010 → 300	3.2×10^{-6}	± 1
	010 → 003	3.2×10^{-6}	0
	010 → 201	6.4×10^{-6}	0
	010 → 102	9.6×10^{-6}	‡ 1
. 94 μ	000 → 121	1.00	0
	000 → 041	8.3×10^{-2}	0
	000 → 140	1.1×10^{-2}	<u>†</u> 1
	000 → 060	3.7×10^{-3}	± 1
	000 → 220	2.5×10^{-1}	± 1
	000→ 022	2.5×10^{-1}	† 1
	000→ 300	2.1×10^{-1}	<u>†</u> 1
	000→ 003	2.1×10^{-1}	0
	000 → 102	4.2×10^{-1} (8)	‡ 1
	000→ 201	4.2×10^{-1}	0
	010 → 131	4.8×10^{-4}	0

TABLE 3 (Continued)

Group	Transition	Relative Intensity	∆ K
. 94 μ	010 → 051	4.0 x 10 ⁻⁵	0
	010 → 150	5.3×10^{-6}	<u>†</u> 1
	010 → 070	1.8×10^{-6}	‡ 1
	010 → 230	1.2×10^{-4}	± 1
	010 → 032	1.2×10^{-4}	± 1
	010 → 013	1.0×10^{-4}	± 1
	010 → 310	1.0×10^{-4}	0
	010 → 211	2.0×10^{-4}	0
	010 → 112	2.0×10^{-4}	± 1

For the other isotopic species the relative intensities are the values in this table multiplied by the relative abundances.

The intensity of any spectral line can be obtained from the appropriate normalization constant, the data in Table 3 and Eqs. (18) and (14). However, these lines correspond to the equivalent symmetric top representation of the water molecule. Thus, it is in order to determine the limitations of this approximation for the calculation of the water vapor transmission. In this regard, it is recalled that the equivalent symmetric top representation introduces a double degeneracy into the spectrum of rotational energy levels such that a given transition represents a pair of transitions in the actual asymmetric molecule spectrum, except for those transitions associated with the levels K = 0 for which there is a one-to-one correspondence.

If the asymmetry is slight, a given pair of transitions will occur close together in frequency and very near the frequency of the corresponding symmetric molecule line. Furthermore the intensity of the symmetric molecule line will be approximately equal to the sum of the intensities of the pair. For molecules which have a considerable asymmetry such as H_2O , the latter statement remains valid. This can be seen from the work of Cross, Hainer and King. They have calculated and tabulated the asymmetric molecule matrix elements corresponding to S(J,K) of Eqs. (15) and (16) for values of J up to J=11. These calculations are based on the expressions characteristic of an asymmetric molecule.

On the other hand, the frequencies of the asymmetric molecule lines and those of the equivalent symmetric molecule become farther displaced from each other as the asymmetry increases. This is the major difficulty of the equivalent symmetric molecule approximation. Clearly this displacement of the spectral lines tends to define a lower limit on the frequency interval over which the approximation may be used to calculate transmission. A determination of this displacement for the lines of several $\rm H_{20}$ bands has been made. It has been found to range from one up to about $\rm 100~cm^{-1}$ toward both lower and higher frequencies. In general the larger values occur for transitions associated with the larger values of the quantum number J; for the strongest transitions ($\rm J \le 4$) the displacements are less than approximately $\rm 20~cm^{-1}$. Thus it appears that the equivalent symmetric top approximation may certainly be used to calculate accurate average transmission values for $\rm H_{20}$ when the frequency interval of interest is $\rm 50~cm^{-1}$ or greater.

Fortunately it was possible in the present study to calculate the transmission for frequency intervals much smaller than 50 $\rm cm^{-1}$ below

3400 cm⁻¹. Benedict, Classen and Shaw and Nielsen have measured and identified the frequencies and intensities of the significant lines of the strongest H2O bands corresponding to the vibrational transitions: (000) \rightarrow (010) and (000) \rightarrow (020) of the 6.3 μ and 3.2 μ groups. Their calculations were based on the asymmetric top molecule calculations of Cross, Hainer and King. 4 The lines tabulated by Benedict, Claassen and Shaw9 and Nielsen10 have been used in the present study. For the weaker lines corresponding to the isotopic and higher order bands which are not included in their tabulation, the equivalent symmetric top approximation has been used. Hence in the 6.3 μ and 3.2 μ regions (frequencies below 3400 cm⁻¹) the transmissions were calculated using frequency intervals of 5 cm⁻¹ (see Appendix B). This is permissible because the Benedict, et al and Nielsen tabulations include all the strong lines, and the weaker less significant lines are very numerous so that the displacements toward both higher and lower frequencies tend to average out.

For all the bands occurring beyond 3400 cm⁻¹ the symmetric top approximation has been used. Thus for frequencies in this range the average transmissions have been tabulated for 20 cm⁻¹, 50 cm⁻¹, and 100 cm⁻¹ intervals. In Appendix A the coefficients which were used in the quasi-random model have been tabulated for 5 cm⁻¹ intervals for frequencies out to 10,000 cm⁻¹. The transitions were originally calculated for a 5 cm⁻¹ interval throughout the spectrum from this data. These results for 5 cm⁻¹ intervals were averaged to obtain the transmissions over 20 cm⁻¹, 50 cm⁻¹, and 100 cm⁻¹ given in appendices C, D, and E respectively.

Another difficulty inherent in the equivalent symmetric top approximation is the following: For the asymmetric molecule there are allowed transitions, but with low intensity, which correspond to the $|\Delta K| \ge 2$ transitions for the symmetric top molecule. These are forbidden by the selection rules for the symmetric top, Eqs. (15) and (16), and not represented when the equivalent symmetric top approximation is used. However, such transitions are many orders of magnitude less intense than those corresponding to $|\Delta K| = 0,1.4$ Hence, in general they contribute insignificantly to the absorption and their exclusion is not expected to cause serious errors in the calculations of transmission.

Finally, it should be noted that the rotational levels of a molecule such as $\rm H_2O$ are alternatively symmetric and anti-symmetric

¹⁰ H. H. Nielsen, Phys. Rev. <u>59</u>, 565 (1941).

and the ratio of the statistical weights of these two types of states is given by $(\frac{s+1}{s})$, 11 where s is the spin of the two identical nuclei in the molecule. Since the spin of the proton is 1/2, the antisymmetric levels of H₂O are weighted 3 times as much as the symmetric levels. Neglecting other functional dependencies, transitions with anti-symmetric initial states are 3 times as intense as those with symmetric initial states. When the equivalent symmetric top approximation is used, the intensities given by Eq. (14) for transitions with K or K' = 0 must be multiplied alternatively by the factors 1 and 3, since there is a one-to-one correspondence between these and the transitions of the asymmetric molecule. When K and K' are greater than zero, a given equivalent symmetric molecule transition corresponds to a pair of transitions, one symmetric and the other anti-symmetric, of the asymmetric molecule and thus is weighted by the factor 4. For the HDO molecule, this intensity alternation does not occur and the weighting factors are taken to be 2, 2, and 4 rather than 1, 3,

¹¹ L. I. Schiff, Quantum Mechanics, McGraw-Hill, New York (1949).

SECTION 3

THE QUASI-RANDOM MODEL OF BAND ABSORPTION

3.1 THE QUASI-RANDOM MODEL

Several different spectral models have been derived which represent the average transmission of radiation absorbed by a group of spectral lines which occur within a finite frequency interval. However, the previous models often do not adequately represent the actual transmission over a wide range of pressures and path lengths. The first difficulty is that the assumed arrangement of the spectral lines within the frequency interval does not correspond adequately with the actual spectrum. Secondly, the contributions from lines lying outside the interval are incorrectly taken into account. Furthermore the variation in intensity of the lines is usually represented by inaccurate approximations. Other approximations which are only valid in certain limited cases are sometimes introduced in order to simplify the calculations.

For example, the statistical model^{1,2,3} is based on the assumption of a random arrangement of the spectral lines while the Elsasser model assumes a constant spacing between the lines. For the statistical model an expression for the transmission is readily derived from the assumption that each line center has an equal probability of falling at any frequency within the interval. However, in the spectrum of an actual molecule a given frequency

¹ H. Mayer, Methods of Opacity Calculations, Los Alamos, LA-647, Oct. 31, 1947.

²R. M. Goody, Quart. J. Roy. Met. Soc. <u>78</u>, 165 (1952).

³G. N. Plass, J. Opt. Soc. Amer. <u>48</u>, 690 (1958); <u>50</u>, 868 (1960).

interval is generally characterized by the occurrence of a relatively small number of stronger lines. These strong lines occur neither at random nor are they regularly arranged. A model is required which localizes the stronger spectral lines so that their positions relative to each other and the interval are taken into account. The quasi-random model localizes the lines to within a frequency interval which is small compared to the final interval of interest.

The quasi-random model is characterized by the following six features which are discussed in more detail later in the report.

- 1. The stronger spectral lines are well localized by the use of small frequency intervals of width D. Within this small interval D the lines are assumed to be arranged at random. The transmission over larger frequency intervals $\triangle \nu > D$ is calculated by averaging the results from the smaller intervals.
- 2. The removal of artificial effects due to the arbitrary division of the spectrum into frequency intervals. This is done by the displacement in frequency of the mesh which divides the spectrum. The transmission is first calculated for one mesh, which defines a certain set of frequency intervals. The calculation is repeated for another mesh which is shifted in frequency by ½D relative to the first set. In principle, the mesh can be shifted n times by an amount D/n. The final calculated transmission is the average of the results for each of these meshes.
- 3. The transmission is calculated from expressions which are valid for a finite and possibly small number of spectral lines in the interval. The expression is not used which is valid in the limit as the number of lines becomes very large.
- 4. The spectral lines in each frequency interval are divided into intensity subgroups which are fine enough to simulate the actual intensity distribution. In the calculation the average intensity of all the lines in each subgroup is used together with the actual number of lines.
- 5. The Landenberg-Reiche approximation assumes that the frequency interval is infinitely wide. This expression cannot be used

⁴R. Landenberg and F. Reiche, Ann. Physik 42, 181 (1913).

in this calculation because of the small frequency intervals into which the spectrum is divided. Instead more general expressions have been derived which are valid for a finite frequency interval, and these are used with the quasi-random model.

6. The contribution from the wings of the spectral lines whose centers are outside a given interval is included. The wing effect is treated in the same detailed manner as the contribution from the lines within the interval.

The grouping of spectral lines within small frequency intervals is basic to the quasi-random model. If these intervals are chosen small enough, a transmission characteristic of each interval can be obtained by assuming a random position for the lines within the small interval. An integrated average transmission over much larger frequency intervals can be obtained by averaging the results over the small intervals.

As the size of a frequency interval is decreased, the relative position of the lines with respect to one another within the interval becomes less and less important. Each line may be said to be localized within an error defined by the interval size, D. The lines within the small interval D are considered to occupy random positions within the interval. This assumption cannot be made for larger frequency intervals $\Delta \nu$ where the random hypothesis can introduce errors for several reasons. First, the spacing between the lines may be fairly uniform, in which case the random hypothesis overestimates the overlapping of the lines. Second, the strong lines may all occur near one end of the larger frequency interval. In this case for large path lengths the random hypothesis might predict almost complete absorption, whereas in actuality only a small part of the interval in the region of the strong lines is strongly absorbing and the rest of the interval is nearly transparent.

In both of these cases, if the original interval is subdivided into sufficiently small intervals, each of which may contain only one or at most a few strong lines, the transmission can then be calculated accurately by assuming the random placement of the spectral lines within the small interval. Of course, if the lines are arranged nearly at random in the original large interval, then nothing is lost by a subdivision into finer intervals. Since the model localizes the lines within the smaller frequency interval D, while calculating the absorption for a larger interval $\triangle\nu$, it is called quasi-random.

If the frequency spectrum is divided into small intervals, D, the transmission T in each of these small intervals is calculated from the equations of the statistical model. 1,2,3 If there are n_k lines in the interval D_k with their line centers at the frequencies ν_i ($i=1,2,\ldots,n_k$), then the transmission at the frequency ν is affected by these n_k lines so that

$$T_{n_k}(\nu) = \frac{1}{D^{n_k}} \prod_{i=1}^{n_k} \int_{D_k} e^{-S_i ub(\nu, \nu_i)} d\nu_i$$
 (20)

where S_i is the intensity of the $i\underline{th}$ line, u is the amount of absorbing gas per unit area, and b is the line shape factor. The transmission is calculated at some frequency ν which for convenience is usually taken at the center of the interval D_k . Since this transmission corresponds to the average of all permutations of the positions of the spectral lines within the interval, it is also assumed to represent the most probable transmission for the entire interval.

In principle the transmission of each spectral line should be calculated from its intensity and position and then substituted into Eq. (20). Because of the very large number of spectral lines which were considered in the present calculation, it was not practical to do this even with a presently available high speed digital computer. Thus some method must be found to simulate the actual intensity distribution. A comparison of calculated intensity distributions with those which have been suggested for use with the statistical model¹,² shows that there is usually poor agreement between the two.

The procedure for intensity simulation adopted here is to divide the lines in each frequency interval into subgroups by intensity decades. When the line intensities are calculated, the results are grouped according to these intensity decades. The average intensity of the lines in each decade is then calculated.

Test calculations have shown that only the first five intensity decades for each frequency interval influence the value of the transmission. Thus only the data for the five strongest intensity decades need be retained for each frequency interval. It should be emphasized that the numerical range of the intensity decades retained are quite different for a frequency interval which contains strong lines than for one which has weak lines. The criterion is applied separately to each frequency interval.

Thus the transmission can be calculated from the average value of the intensity $S_{\underline{i}}$ together with the number of lines $n_{\underline{i}}$ in each intensity decade from the equation

$$T_{n_{k}}(\nu) = \mathcal{T} \left\{ \frac{1}{D} \int_{D_{k}} e^{-\overline{S}_{i}ub(\nu, \nu_{i})} d\nu_{i} \right\}^{n_{i}}$$
(21)

The number of lines $n_{\rm L}$ in the frequency interval is given by

$$n_{k} = \sum_{i=1}^{5} n_{i}$$
 (22)

Of course, the lines could be grouped by intensity using a smaller or larger factor than the decade of intensity adopted here. However, this choice seemed reasonable since it yields intensity subgroups which are sufficiently small intervals so that the average value is never much different from the actual intensity of the lines in the decade, while on the other hand the interval is sufficiently large so that the number of different variables used in the calculation are still within the memory limitations of a modern digital computer. All of the lines which occur in a particular intensity group are considered to occur at random in the frequency interval $D_{\bf k}$, as is indicated by Eq. (21). Furthermore each intensity group is treated independently of any other.

The integral in Eq. (21) represents the transmission over the finite interval D_k of a single spectral line representative of the average intensity of the decade. For the small intervals used in the present calculation, it is important to separate the absorption caused by a given spectral line into two parts: the absorption which it produces within the interval which contains its line center and the absorption produced by it in all other frequency intervals arising from its wings. For the calculation of the absorption within the frequency interval which contains the line center the Landenberg-Reiche⁴ equation cannot be used. It assumes an infinite frequency interval, whereas the intervals in the present calculation are not necessarily large compared to the effective width of the line. Although equations for the absorption of lines over finite intervals have been obtained previously in certain limits, a general expression

has not been available. This result is given in section 3.2, Eqs. (27), (30), and (32). Because of the small number of strong lines in the smaller frequency intervals, it is important to calculate the transmission of each line which represents an intensity decade and then to multiply these transmissions as indicated in Eq. (21). Accordingly, the exponential expression for the transmission derived from the statistical model when the number of lines approaches infinity may not be used since the number of lines in an intensity decade in these smaller frequency intervals may be small.

The transmission at a frequency ν is also influenced by the wings of spectral lines whose centers are outside of the interval D_k which contains the frequency ν . The wing transmission T_{n_1} from each of these intervals D_i is calculated by assuming a random distribution of the lines within the intervals D_i . Thus by the random hypothesis the transmission at the frequency ν is the product of all transmissions calculated for the lines with centers in other intervals taken with the transmission for the given interval itself, so that

$$T(\nu) = \prod_{i=1}^{\infty} T_{n_i}(\nu)$$
 (23)

where the subscript n_1 indicates that there are n_1 lines in the frequency interval D_1 . The transmission for the lines whose centers are in the interval D_1 are given by Eq. (21). The lines in sufficiently distant intervals from the particular frequency ν have a negligible effect on the transmission, so that in practice the product (Eq. 23) usually needs to be evaluated only over a few terms. Approximate expressions for the wing transmission T_{n_1} are given in section 3.2, Eqs. (27) and (29) for the Lorentz line shape and in section 3.3, Eq. (42), for the Benedict modification of the Lorentz line shape.

Finally, it is necessary to remove the artificial effects arising from the arbitrary division of the spectrum into frequency intervals. In order to illustrate this effect consider a set of six equally intense lines spanning a frequency range of 10 cm⁻¹. If the lines, for simplicity, be nearly evenly spaced, the transmission calculated at the center of the two intervals containing them might be expected to be equal. This would be the case if three lines fell into each 5 cm⁻¹ interval, for the model subsequently

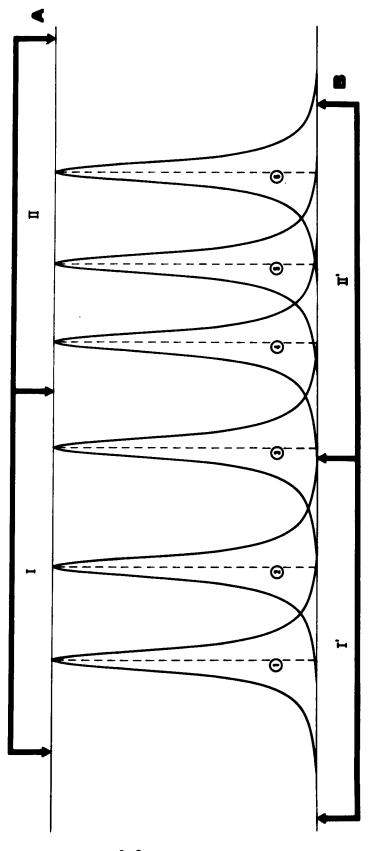
attributes a random distribution to each set of lines falling within the chosen intervals. But since the uniform mesh is started at some arbitrary position, it is conceivable that two lines might fall into one interval and four into the other. This situation is illustrated in Fig. 3.1 where the mesh labeled "A" represents the former case while "B" illustrates the latter. The six bars schematically represent the lines and the arrows the frequency divisions.

The transmissions calculated at the centers of the intervals in case "B" differ appreciably from those in case "A", whereas physically one would expect them to be nearly equal for lines with such uniform spacing. The disparity, of course, may be blamed firmly upon the positioning of line 3. As far as the model is concerned, the fact that line 3 lies very close to the artificial mesh boundary is of no consequence; in case "A" it has a random probability of being anywhere within interval I whereas in case "B" it may lie anywhere within II'. Thus the model does not take into account such borderline situations. The introduction of such an error is of no practical importance if the results of a number of frequency intervals are to be averaged to obtain the integrated average transmission over a larger interval. However, if the detailed average effective transmission is required over smaller frequency intervals, then the model must be suitably modified.

The modification of the transmission calculations necessary to remedy these artificial errors is extremely simple. The transmission is calculated twice using two meshes one of which has been displaced D/2 cm⁻¹ with respect to the other. Thus the first calculation yields values at $\nu_{\rm O}, \nu_{\rm O}$ + D, $\nu_{\rm O}$ + 2D, ... while the second produces transmission values at $\nu_{\rm O}$ + D/2, $\nu_{\rm O}$ + 3D/2, $\nu_{\rm O}$ + 5D/2, ..., where $\nu_{\rm O}$ corresponds to the lowest frequency at which the transmissions are calculated. Thus transmission values are calculated at the following frequencies:

Figure 3. 1

EFFECT OF MESH DISPLACEMENT



The correct average transmissions at a particular frequency $\nu_{\rm n}$ subsequently are calculated from these values by the following simple formula:

$$\overline{T}(\nu_n) = \frac{T(\nu_{n-1}) + T(\nu_n) + T(\nu_{n+1})}{3}$$
 (24)

where the T's refer to the effective transmissions calculated by the dual mesh scheme and labeled as shown in the table above. Such a procedure automatically compensates for the artificial errors introduced by the arbitrary mesh positioning and provides an excellent representation of the average transmission over small frequency intervals. All of the average effective transmission values given in this report are averaged in this manner using two meshes shifted relative to each other by ½D.

3.2 THE TRANSMISSION FOR A FINITE FREQUENCY INTERVAL

In this section an expression is derived for the transmission of a finite frequency interval for spectral lines with the Lorentz line shape. A finite number of spectral lines are assumed to be in the interval. Expressions have been derived previously for the transmission according to the statistical model for a finite number of spectral lines^{1,2,3} and in certain limits for a finite frequency interval. However, in practical calculations which use the statistical model the assumption seems to have always been made that the equations for an infinite number of spectral lines and an infinite frequency interval are sufficiently accurate. Such expressions cannot be used for the small frequency intervals which are used in the present calculation.

Therefore a general expression for the transmission for finite frequency intervals and a finite number of spectral lines is derived. In this section it is assumed that the Lorentz line shape

$$b(\nu, \nu_i) = \frac{\alpha/\pi}{(\nu - \nu_i)^2 + \alpha^2}$$
 (25)

describes the actual line contours, where α is the pressure broadened half-width of the line whose center lies at ν_1 . When pressure broadening is the dominant effect, the lines of $\rm H_2O$ are well described by

the Lorentz line shape. For ${\rm CO_2}$ the wings of the lines seem to be described better by the Benedict modification of the Lorentz line shape. This is described further in section 3.3. Consider a frequency interval D which lies between the frequencies $\nu_{\rm O}$ and $\nu_{\rm O}$ + D. The following symbols are used in the derivation of the transmission over a finite frequency interval:

$$\xi_{k} = \frac{S_{k}u}{\pi \alpha}$$

$$\rho = 2\alpha / D$$

$$y = \nu_{k} - \nu_{o} - D/2$$

$$z = \nu - \nu_{o} - D/2$$

$$\eta = 2y/D$$

$$\epsilon = 2z/D$$
(26)

Thus for the Lorentz line shape the transmission, $\mathbf{T}_{\mathbf{n_l}}$, is given by

$$T_{n_{k}} = \frac{1}{D} \int_{0}^{\infty} \exp \left[S_{k} ub(\nu, \nu_{k}) \right] d\nu_{k} = \frac{1}{2} \int_{1}^{1} \exp \left[\frac{\rho^{2} \xi_{k}}{(\varepsilon - \eta)^{2} + \rho^{2}} \right] d\eta$$
(27)

Define ξ_{k_0} by the expression

$$\xi_{k} = \xi_{k_{o}} u/p = \frac{S_{k} p_{o} u}{\pi \alpha_{o} p}$$
 (28)

where a_0 is the half-width at the pressure p_0 . At a particular

⁵W. S. Benedict, private communication.

temperature, the coefficients ξ_k need be calculated only once for each frequency interval D_1 and intensity group. The coefficients ξ_k together with the number of spectral lines for each of the top five intensity groups represent sufficient information about the spectrum for the calculation of the absorption in a frequency interval. When ξ_{k_0} is known, then the coefficients for any pressure and path length combination may be readily calculated from Eq. (28). Indeed, this is one of the most important simplifications of the present model.

Because $\rho = 2\,\alpha/D$ is usually very small, Eq. (23) can be divided easily into two distinct parts. There is the direct contribution from the lines whose centers are within the given interval in addition to the wing contribution from the lines in all other intervals.

So long as ν is not chosen too close to the edge of an interval, which is generally taken to be large compared to the half-width of any line, then $(\varepsilon - \eta)^2 >> \rho^2$ for all the factors in Eq. (23) which correspond to lines whose centers are in other frequency intervals. Hence for the wing contributions ρ^2 may be neglected compared to $(\varepsilon - \eta)^2$. Thus the integral in Eq. (27) can be written as

$$\frac{1}{2} \int_{-1}^{1} \exp \left[-\frac{\rho^{2} \xi_{k}}{(\epsilon - \eta)^{2}}\right] d\eta$$

$$= \frac{1}{2} \left[(\epsilon + 1) e^{-A/(\epsilon + 1)^{2}} - (\epsilon - 1) e^{-A/(\epsilon - 1)^{2}} - \frac{\pi A}{2} \left[\operatorname{erf} \frac{\sqrt{A}}{\epsilon - 1} - \operatorname{erf} \frac{\sqrt{A}}{\epsilon + 1} \right] \right]$$
(29)

where $A = \rho^2 \xi_k$ and $\epsilon > 1$. Thus Eq. (29) represents a readily evaluated quantity.

The direct contribution, on the other hand, is more difficult to evaluate. Let

$$\bigcap (\xi_k, \delta) = \frac{1}{a} \int_0^a \exp \left[-\left[\frac{\rho^2 \xi_k}{\eta^2 + \rho^2} \right] d\eta \right] d\eta = \int_0^1 \exp \left[-\left[\frac{\delta^2 \xi_k}{y^2 + \delta^2} \right] dy \right] \tag{30}$$

where $\delta = \rho/a$. Therefore returning to the direct contribution one finds

$$\frac{1}{2} \int_{-1}^{1} \exp \left[-\frac{\rho^{2} \xi_{k}}{(\epsilon - \eta)^{2} + \rho^{2}}\right] d\eta$$

$$= \frac{1}{2} \left\{ \int_{0}^{1 - \epsilon} \exp \left[-\frac{\rho^{2} \xi_{k}}{z^{2} + \rho^{2}}\right] dz + \int_{0}^{1 + \epsilon} \exp \left[-\frac{\rho^{2} \xi_{k}}{z^{2} + \rho^{2}}\right] dz \right\}$$

$$= \frac{1}{2} \left[(1 - \epsilon) \Omega (\xi_{k}, \delta) + (1 + \epsilon) \Omega (\xi_{k}, \delta') \right]$$

$$\delta = \rho/(1 - \epsilon), \quad \delta' = \rho/(1 + \epsilon)$$
(31)

In section 3.4 it is shown that for the general case

$$\Omega(\xi, \delta) = e^{-\xi \delta^{2}/(1+\delta^{2})} - \frac{\delta \xi}{2} e^{-\xi/2} \left[I_{0}(\xi/2) + I_{1}(\xi/2) \right] (\pi - \psi)
+ 2 \delta e^{-\xi/2} \sum_{n=1}^{\infty} I_{n}(\xi/2) \sin n \psi$$
(32)

+
$$\delta \xi e^{-\xi/2} \sum_{n=1}^{\infty} \left[I_n(\xi/2) + I_{n+1}(\xi/2) \right] \frac{\sin n\psi}{n}$$

where $\psi=2$ tan⁻¹ δ , $\delta=\rho/a$ and the I 's are the Bessel functions of imaginary argument. Although the sums in Eq. (32) are rapidly convergent, in the two cases when $\xi>>1$ and $\xi<1$ useful alternative forms may be found, whose derivation is also found in section 3.4.

Specifically for $\xi < 1$ one has

$$\Omega(\xi, \delta) = 1 - \delta \sum_{n=0}^{\infty} (-1)^n \frac{\xi^{n+1}}{(n+1)!} \mathbf{I}_n$$
(33)

where

$$\mathcal{A}_{n} = \frac{\delta^{2n-1}}{2n(1+\delta^{2})^{n}} + \frac{2n-1}{2n} \mathcal{J}_{n-1}$$

$$\mathcal{J}_{o} = \tan^{-1}(1/\delta)$$
(34)

The series in Eq. (34) is absolutely convergent for all ξ but is more useful when ξ is small.

When ξ is large, on the other hand, an asymptotic representation is

$$\int (\xi, \delta) = e^{-\xi \delta^{2}/(1+\delta^{2})} - \frac{\pi \delta \xi}{2} e^{-\xi/2} \left[I_{o}(\xi/2) + I_{1}(\xi/2) \right] + 2\delta \xi \sum_{m=0}^{p-1} \frac{(-\frac{1}{2})_{m-m}}{m!} + 2\delta \xi R_{p}$$
 (35)

where

$$\mathcal{J}_{m} = -\frac{\epsilon^{2m-1}}{2\xi} e^{-\delta^{2}\xi/(1+\delta^{2})} + \frac{2m-1}{2\xi} \mathcal{J}_{m-1}$$

$$\mathcal{J}_{o} = \frac{1}{2}\sqrt{\frac{\pi}{\xi}} \operatorname{erf}(\epsilon\sqrt{\xi})$$

$$\epsilon = \delta/\sqrt{1+\delta^{2}}$$
(36)

with the remainder term, R_D, given by

$$R_{p} = \frac{(-\frac{1}{2})_{p}}{(p-1)!} \int_{0}^{\epsilon} y^{2p} e^{-\frac{\epsilon}{2}y^{2}} dy \int_{0}^{1} \frac{(1-t)^{p-1}}{(1-y^{2}t)^{p-\frac{1}{2}}} dt$$
 (37)

and the Barnes' coefficient $(\alpha)_n$ defined by

$$(\alpha)_{n} = \alpha(\alpha+1)...(\alpha+n-1), (\alpha)_{0} = 1$$
 (38)

On the basis of Eqs. (29) and (31) the effective transmission at a particular frequency may now be written as

$$T(\nu) = T_{n_k}(\nu) \prod_{i \neq k} T_{n_i}(\nu)$$
(39)

where the subscript k refers to the particular interval in which lies and $T_k(\nu)$ is obtained from Eqs. (21), (27), (31), and (32) while $T_i(\nu)$, for $i \neq k$, is readily calculated from Eqs. (21), (27) and (29).

The water vapor and carbon dioxide (SSD-TDR-62-127 - Volume III) transmissions were all calculated on the basis of this formalism. The absorption from a single spectral line which represents an intensity group in a finite frequency interval was calculated from these equations. The other lines in a small frequency interval are assumed to be distributed at random so that the transmission of the various lines can be multiplied together according to Eq. (21). The transmissions calculated from the wing absorption of lines outside the interval are multiplied according to Eq. (39). Finally the results are calculated for two different frequency meshes shifted an amount ½D with respect to each other and these results are averaged to obtain the average effective transmission for the interval.

3.3 BENEDICT MODIFICATION OF THE LORENTZ LINE SHAPE

As mentioned in section 3.2, Benedict has proposed a modification of the Lorentz line shape for CO_2 on the basis of his experimental

examination of the absorption from some particular lines. He has found that the line shape in the wings drops off much faster than $|\nu-\nu_0|^{-2}$ as required by the Lorentz line shape. On the basis of these findings he has suggested the following semi-empirical line shape

$$b(\nu, \nu_i) = \frac{\alpha/\pi}{(\nu - \nu_i)^2 + \alpha^2}, |\nu - \nu| < d$$
 (40)

$$= \frac{A \alpha/\pi \exp[\alpha |\nu - \nu_i|^b]}{(\nu - \nu_i)^2 + \alpha^2}, |\nu - \nu_i| \ge d$$

where a = 0.0675, b = 0.7, d = 5.0 cm⁻¹ and A is a constant which makes the two forms continuous at $|v - v_i| = d = 5.0$ cm⁻¹.

The effective transmission is now calculated in a manner similar to that described in section 3.2 with one important change. Since the frequency interval chosen for these calculations is 5 cm⁻¹, the Lorentz line shape is still valid for lines whose centers are within the interval. This contribution can still be calculated as before from Eqs. (21), (27), (31), and (32). On the other hand, the wing contributions must be treated differently. Introducing the symbols defined in Eq. (26), the contributions from the wings will involve terms

$$T_{W_{p}}(\nu) = \frac{1}{D} \int_{\mathbf{k}} \exp \left[-\left[\frac{AS_{\mathbf{k}}u^{\alpha} \exp\left[-a|\nu - \nu_{\mathbf{k}}|^{b}}{\pi\left((\nu - \nu_{\mathbf{k}})^{2} + \alpha^{2}\right)^{b}}\right] d\nu_{\mathbf{k}}\right]$$

$$\approx \frac{1}{2} \int_{-1}^{1} \exp\left[-\left[\frac{A\xi_{\mathbf{k}} \rho^{2} \exp\left[-\left\{a(D/2)^{b}|\varepsilon - \eta\right|^{b}\right\}\right]}{(\varepsilon - \eta)^{2}}\right] d\eta$$
(41)

where ρ^2 has again been neglected compared with $(\epsilon - \eta)^2$ (see section 3.2). Equation (41) cannot be reduced to an analytic form as was done for the transmission from the wings of a line with the

Lorentz line shape, Eq. (29). Since the absorption drops off even more rapidly with frequency in the Benedict modification than with the Lorentz line shape, the wing contributions may be calculated to a high degree of accuracy by assuming that the lines are all located at an average position rather than a random one. The average position chosen was the center of the interval, i.e. $\eta = 0$. In this event Eq. (41) becomes

$$T_{W_{k}}(\nu) = \exp \left\{-\left\{\frac{A \xi_{k} \rho^{2} \exp \left[a(D/2)^{b} | \epsilon|^{b}\right]}{\epsilon^{2}}\right\}$$
(42)

The effective transmission for the Benedict modification of the Lorentz line shape at a particular frequency ν is now written as

$$T(\nu) = T_k(\nu) \int_{i\neq k} T_i(\nu)$$
 (43)

where the subscript k refers to the interval in which ν lies, $T_k(\nu)$ is calculated from Eq. (31) and the $T_1(\nu)$'s are calculated on the basis of Eq. (42).

The $\rm CO_2$ transmissions were all calculated on this basis. Nevertheless, for comparison purposes, they were recalculated using the Lorentz line shape at $300^{\rm O}{\rm K}$ and one atmosphere pressure. Appendix D of SSD-TDR-62-127 - Volume III gives the results of this calculation. It is interesting to note that there is a very small difference between the two calculations even for large path lengths.

3.4 DERIVATION OF THE TRANSMISSION EQUATIONS FOR THE DIRECT CONTRIBUTIONS

Consider now the evaluation of the integral occurring in Eq. (30), viz.

$$\Omega(\xi,\delta) = \int_0^1 \exp\left[-\left[\frac{\delta^2 \xi}{y^2 + \delta^2}\right] dy \tag{44}$$

Letting $y = \delta \sqrt{1-z^2}/z$, Eq. (44) becomes

$$\bigcap (\xi, \delta) = \delta \int_{\delta/\sqrt{1+\delta^2}}^{1} \frac{e^{-\xi z^2}}{z^2 \sqrt{1-z^2}} dz$$
(45)

Integrating by parts once

$$\int (\xi, \delta) = e^{-\xi \delta^2/(1+\delta^2)} - 2\delta \xi \int_{\delta/\sqrt{1+\delta^2}}^{1-z^2} e^{-\xi z^2} dz
 \tag{46}$$

Consider now

$$G_{1} = \int_{\delta/\sqrt{1+z^{2}}}^{1} e^{-\xi z^{2}} dz$$

$$= \int_{0}^{1} \sqrt{1-z^{2}} e^{-\xi z^{2}} dz - \int_{0}^{\delta/\sqrt{1+\delta^{2}}} e^{-\xi z^{2}} dz \qquad (47)$$

$$= G_{2} - G_{3}$$

Letting $z = \sin \theta$, the first integral becomes

$$G_{2} = \int_{0}^{\pi/2} \cos^{2} \theta e^{-\xi \sin^{2} \theta} d\theta$$

$$= \frac{e^{-\xi/2}}{4} \int_{0}^{\pi} (1 + \cos \phi) e^{-i\beta \cos \phi} d\phi \qquad (48)$$

$$= \frac{\pi e^{-\xi/2}}{4} \left[J_{0}(\beta) - iJ_{1}(\beta) \right]$$
3-17

where the substitutions $\phi = 20$ and $\beta = \frac{i\xi}{2}$ have been made to obtain the final result involving the usual Bessel functions.

Re-expressing the result in terms of Bessel functions of imaginary argument

$$G_2 = \frac{\pi e^{-\xi/2}}{4} \left[I_0(\xi/2) + I_1(\xi/2) \right]$$
 (49)

Letting $\epsilon=\sin^{-1}\delta/\sqrt{1+\delta^2}=\tan^{-1}\delta$, the second integral in Eq. (47) becomes

$$G_3 = \int_0^{\epsilon} \cos^2 \theta e^{-\xi \sin^2 \theta} d\theta$$
 (50)

where again the substitution $z = \sin \theta$ has been made. Once more let $\phi = 2 \theta$ to obtain

$$G_3 = \frac{1}{4} e^{-\frac{\xi}{2}} \int_0^{2\epsilon} (\cos \phi + 1) e^{\frac{\xi \cos \phi}{2}} d\phi$$
 (51)

Letting
$$G_4 = \int_0^{2\epsilon} \frac{\xi \cos \phi}{2} d\phi$$
 one has

$$G_3 = \frac{1}{4} e^{-\frac{\xi}{2}} \left[G_4 + 2 \frac{\partial G_4}{\partial \xi} \right]$$
 (52)

and hence it remains only to evaluate $G_{\underline{i}}$. Substituting $z = i \xi/2$, one has

$$G_{4} = \int_{0}^{2\epsilon} e^{-iz \cos \phi} d\phi$$

$$= \int_{0}^{2\epsilon} \cos(z \cos \phi) d\phi - i \int_{0}^{2\epsilon} \sin(z \cos \phi) d\phi \qquad (53)$$

However $\cos(z \cos \phi)$ and $\sin(z \cos \phi)$ may be represented by their absolutely convergent Jacobi⁶ expansions, viz.

Hence

$$G_{4} = J_{o}(z) \psi + 2 \sum_{n=1}^{\infty} (-1)^{n} J_{2n}(z) \frac{\sin 2n \psi}{2n}$$

$$- 2i \sum_{n=0}^{\infty} (-1)^{n} J_{2n+1}(z) \frac{\sin(2n+1) \psi}{2n+1}$$
(55)

where $\psi = 2\epsilon = 2 \tan^{-1} \delta$. Re-expressing in terms of ξ one has

$$G_{4} = I_{0}(\xi/2) \psi + 2 \sum_{n=1}^{\infty} I_{2n}(\xi/2) \frac{\sin 2n \psi}{2n}$$

$$+ 2 \sum_{n=0}^{\infty} I_{2n+1}(\xi/2) \frac{\sin(2n+1) \psi}{2n+1}$$

$$= I_{0}(\xi/2) \psi + 2 \sum_{n=1}^{\infty} I_{n}(\xi/2) \frac{\sin n \psi}{n}$$
(56)

⁶C.G.J. Jacobi, Journal fur Math. 15, 12 (1836).

Therefore

$$G_{3} = \frac{1}{4} e^{-\frac{\xi}{2}} \left\{ I_{0}(\xi/2) \psi + I_{1}(\xi/2) \psi + \frac{4}{\xi} \sum_{n=1}^{\infty} I_{n}(\xi/2) \sin n \psi + 2 \sum_{n=1}^{\infty} \left[I_{n}(\xi/2) + I_{n+1}(\xi/2) \right] \frac{\sin n \psi}{n} \right\}$$
(57)

If Eqs. (49) and (57) are substituted into Eq. (46) and (47), the previously quoted result, Eq. (32), is obtained.

Although Eq. (32) is absolutely convergent, when $\xi<1$ and $\xi>>1$ two simplified forms may be obtained (Eqs. 33 and 35). The former is obtained from Eq. (44) directly by expanding the kernel of the integral and integrating term by term. This procedure immediately produces Eq. (33) which is itself absolutely convergent.

When $\xi >> 1$, an asymptotic form may be obtained by starting from Eqs. (46) and (47) and expanding $\sqrt{1-z^2}$ under the integral sign via the binomial expansion theorem. Thus

$$\Omega(\xi, \delta) = e^{-\xi \delta^{2}/(1+\delta^{2})} - \frac{\delta \xi}{2} e^{-\xi/2} [I_{0}(\xi/2) + I_{1}(\xi/2)]
+ 2 \delta \xi \int_{0}^{\delta/\sqrt{1+\delta^{2}}} e^{-\xi z^{2}} dz$$
(58)

But

$$\int_{0}^{\delta/\sqrt{1+\delta^{2}}} e^{-\xi z^{2}} dz = \sum_{m=0}^{p-1} \frac{(-\frac{1}{2})_{m} - \frac{1}{m}}{m!} + R_{p}$$
 (59)

where ψ_m is given by Eq. (36) and R_p is the remainder term given by Eq. (37). The summation represents the first p integrals obtained by expanding $\sqrt{1-z^2}$ to order z^{2p-2} . The remainder term was obtained on the basis of a formalism apparently due to Graf and Gubler.

The second term in Eq. (58) is the familiar Landenberg and Reiche result⁴ which is valid when the exponential and integral term in this equation can be neglected. The expression for the absorption over a finite interval when the strong line approximation is valid³ is obtained from Eq. (58) by inserting an asymptotic expression for the Bessel functions and evaluating the leading term of the integral from Eqs. (59) and (36). The absorption over a finite interval when the weak line approximation is valid³ is obtained from Eqs. (33) and (34).

⁷J. H. Graf and E. Gubler, Einleitung in die Theorie der Besselshen Funktionen, 1, 86 (Bern, 1898).

SECTION 4

SPECIFIC DETAILS OF THE CALCULATION

Prior to calculating the transmissions based on the previously described model, a coefficient table was generated for the two frequency meshes at each of the temperatures considered. Each of these coefficient tables is composed of ξ_{Ok} and n_k as a function of frequency interval, where n_k is the number of lines in the intensity decade and ξ_{Ok} is defined by Eq. (28). At each frequency interval the coefficients were calculated for up to five intensity decade groups in the following manner:

- (1) The vibrational intensity factors CV of all contributing vibrational transitions were determined by a normalization procedure to be described subsequently.
- (2) On the basis of (1), the integrated intensities of all contributing vibration-rotation lines were calculated systemmatically.
- (3) As the intensity and frequency of each line was generated, the line was assigned to the frequency interval spanning it.
- (4) Once assigned to an interval, a given line was then grouped according to the intensity decade into which it fell. Within a particular decade a running count was made of the number of lines placed therein. Also retained was a net sum of the intensities of all those lines placed in each decade. If a line was generated with an intensity more than eight orders of magnitude below the strongest line already placed in the given frequency interval, it was ignored. On the other hand, if stronger lines were subsequently generated.

the data for weaker lines was dropped when they occurred in intensity groups which were more than four groups below the most intense. In short either the top five strongest groups were retained, or only enough groups to span eight orders of magnitude. The latter choice resulted in less than five groups when the lines in that portion of the spectrum were very weak.

(5) The coefficients $\xi_{\rm Ok}$ were then calculated for each frequency interval by dividing the intensity sums by the number of contributing lines and thence dividing the resulting average strengths by $\pi\alpha_{\rm O}$. For H₂0 the value $\alpha_{\rm O}$ = 0.10 cm⁻¹ was used.

Once the coefficients ξ_{Ok} and n_k were generated, the effective transmissions were calculated at frequencies corresponding to the centers of the chosen frequency intervals of width 5 cm⁻¹. ($\epsilon = 0$ in the notation of section 3.2.) Sequentially the coefficients ξ_k for various combinations of the pressure* and amounts of absorbing gas were calculated ($\xi_k = \xi_{Ok}$ u/p). From each of these sets the effective transmissions were calculated as follows:

- (1) All the transmissions were set equal to unity.
- (2) Starting with the lowest frequency interval, the direct contributions to the transmissions were calculated at the center of the interval for each intensity group contained therein using the formulation described in section 3.2 (specifically Eq. (32) and, if applicable its limiting forms, Eqs. (33) and (35)). These were then multiplied together and thence by the factor 1 initially set. Hence the resulting transmission represented the direct contributions from the five intensity groups which represent all lines having an intensity within 10^{-6} of the strongest line in the frequency interval.
- (3) Subsequent to the calculation of the direct contributions, the coefficients were used to calculate the wing contributions to the transmissions at the center of the interval of interest. The wing contributions from lines at both lower and higher frequencies

It should be mentioned that the term pressure is used here in the sense of Howard, Burch and Williams, viz for water vapor the effective broadening pressure is equal to the sum of the total pressure plus 5.3 times the partial water vapor pressure.

were considered. The calculation was made from Eq. (29) for the Lorentz line shape and, in the case of CO₂, from Eq. (42) for the Benedict modification. Thus as any contribution to the transmission at a given frequency was generated (be their origin direct or wing), its value was multiplied into those previously calculated at that frequency.

(4) The wing calculations were carried out at frequencies farther and farther from the chosen interval until their contributions to the transmissions exceeded 0.999.

Insofar as the normalization procedure was concerned, the detail yielded by the quasi-random model was not needed. This is because the normalization was based on a comparison of the calculated integrated absorptions with the measured integrated absorptions of Howard, Burch, and Williams for large frequency intervals (> 400 cm^{-1}). The correct normalization was obtained via a two step process. A large mesh size (20 cm⁻¹) was chosen to generate a separate coefficient table (similar to those indicated by Appendix A) for each of the seven transition groups in ${
m H_2O}$ and the twenty-two in ${
m CO_2}$ using the relative intensities as an initial starting point. Thence integrated transmissions were calculated (using the simplifications just mentioned) at various effective pressures and paths corresponding to experimental results of Howard, Burch and Williams (T was always chosen at 300°K). These were compared with the measured integrated transmissions and the squares of the deviations of ten to twenty such sets were summed. The coefficients $\xi_{\,\,0_{\bf k}}$ were then all multiplied by an arbitrary factor and the sum of the squares of the deviations were again calculated. Other multiplicative factors were subsequently chosen and plotted as a function of the corresponding sums of the squares of the deviations. The absolute minimum was then calculated graphically and a first approximation to the normalization constants C_0^{V} (300°K) deduced therefrom for each group. Using these first approximations, the procedure was then repeated using a finer mesh (5 cm⁻¹). Again a least squares fit yielded the best coefficients, which are listed in Table 4. In the event that two groups overlapped a two-dimensional generalization of the above least squares method was used.

TABLE 4
WATER VAPOR NORMALIZATION CONSTANTS

Spectral Region	C (300°K)
6.3 μ	888
3.2 μ	16.5
2.7 μ	1950
1.87 μ	203
1.38 μ	47.5
1.1 μ	1.87
. 94 μ	1.11

SECTION 5

USE OF APPENDICES AND INTERPOLATION PROCEDURES

5.1 USE OF APPENDICES

The five appendices following this section contain the results of the present calculation. Appendix A contains the coefficients ξ_0 (defined in Eq. (28)) and n the number of lines in the intensity decade for the top five intensity groups of each frequency interval as a function of frequency. A particular frequency entry corresponds to the center of an interval extending 2.5 cm⁻¹ in both directions from the center. Two sets of coefficients are included for each temperature and correspond to two meshes displaced 2.5 cm⁻¹ from each other. For identification purposes the meshes with a center wave number beginning at 1000 cm⁻¹ have been labeled "unshifted" while those starting at 1002.5 cm-1 have been labeled "shifted". As before the entries correspond to the frequencies at the center of two mesh points (e.g. the entries at 1997.5 cm⁻¹ were calculated from the spectral lines lying between 1995.0 and 2000.0 cm⁻¹, etc.). Note that beyond 3400 cm⁻¹ the coefficient tables should be used only with extreme caution unless the values are averaged over a wider frequency interval. Beyond 3400 cm⁻¹ the entries were calculated exclusively on the basis of the symmetric rotator model (see section 2.2). These entries may be used to obtain transmissions which are subsequently averaged over wider frequency intervals. However, the entries in themselves cannot be too significant for intervals of 5 cm⁻¹ since the positions of the lines on the symmetric rotator model may be in error by more than this amount. Nevertheless entries beyond 3400 cm⁻¹ have been included for completeness since they formed the basis for the tabulated average transmission values (Appendices C, D, and E).

Appendix B lists, as a function of frequency and path thickness (u, in precipitable centimeters) for three temperatures at seven different pressures, the average transmissions for 5 cm⁻¹ intervals calculated on the basis of the quasi-random model. Note that the entries terminate at 3400 cm⁻¹, since accurate frequencies for the stronger H₂O spectral lines were only available up to this frequency and furthermore that they are listed every 2.5 cm⁻¹.

Appendix C lists transmissions averaged over 20 cm⁻¹ at intervals of 10 cm⁻¹ for all the temperatures and pressures of Appendix B. However, the entries go out to 10000.0 cm⁻¹. The averaging has minimized the uncertainties in the frequencies of individual lines which is introduced by the symmetric rotator description. In effect the entries in Appendix C represent the average transmissions that a detector with an acceptance window of 20 cm⁻¹ and unit response would record if centered on the tabulated frequencies.

Appendices D and E are identical to Appendix C with the exception of the size of interval averaged over. Appendix D lists entries averaged over 50 cm $^{-1}$ while E lists entries averaged over 100 cm $^{-1}$. In these latter appendices entries occur every 25 cm $^{-1}$ and 50 cm $^{-1}$ respectively.

The experimental measurements of Burch et al 1 for the 2.7 μ and 6.3 μ bands of water vapor are compared with the theoretical calculations for two particular sets of values of path length and pressure in Figs. 5-1 and 5-2. The theoretical values plotted are averaged over 20 cm⁻¹.

5.2 INTERPOLATION PROCEDURES

The extensive transmission tables given in the appendices provide a suitable basis for interpolation in terms of pressure, temperature and path length. Interpolation in these parameters is readily achieved via analytic methods.

The simplest analytical procedure is that consisting of logarithmic interpolation between non-zero values of the absorption A. Express the absorption in the form

$$A = 1 - \tau = e^{-f(p,T,u)}$$
 (60)

where f is usually a complicated function of pressure (p), temperature (T),

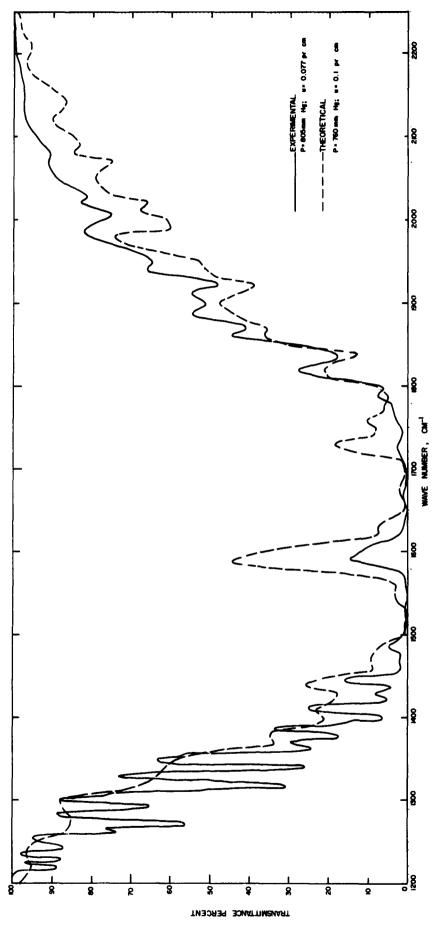


FIGURE 5-1. ABSORPTANCE OF 2.7 μ H 0 BAND

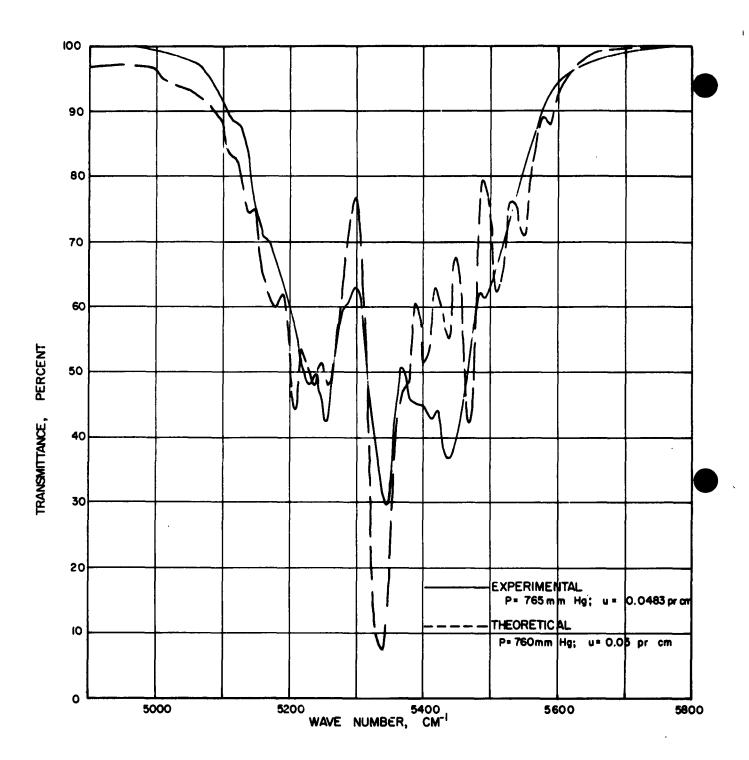


FIGURE 5-2. ABSORPTANCE OF 6.3μ BAND

and path length (u). At points where one or both of the tabular values of τ are identically equal to unity, linear interpolation on τ provides more than sufficient accuracy. Otherwise it is far more accurate to interpolate f(p,T,u). This is true because the main part of the functional dependence of the absorption on p, T, and u is usually represented by the exponential factor. As only three significant figures are given in the tables, a first order interpolation in general provides sufficient accuracy. It should be noted that the entries for varying pressure and path length are given in terms of values that are nearly equidistant when plotted on a logarithmic scale (e.g. 1.0, 0.5, 0.2, 0.1, 0.05, ...)

From Eq. (60) one has

$$f(p,T,u) = -\ln A$$
. (61)

When the absorptance at constant p is plotted against u on a log-log graph, the resulting curve has only a small curvature and displays long linear sections. Similar remarks apply to an absorptance curve at constant u plotted against p. For these reasons, the most accurate interpolation is obtained by taking equal logarithmic intervals for p and u so that

$$\Delta f = \frac{\partial f}{\partial x} \Delta x + \frac{\partial f}{\partial T} \Delta T + \frac{\partial f}{\partial y} \Delta y \qquad (62)$$

where $x = \ln p$ and $y = \ln u$. Thus

$$f(p + \Delta p, T + \Delta T, u + \Delta u) = f(p,T,u) + \Delta f$$
 (63)

and

$$\tau (p + \Delta p, T + \Delta T, u + \Delta u) = 1 - A(p + \Delta p, T + \Delta T, u + \Delta u) =$$

$$1 - \exp - (f + \Delta f) \tag{64}$$

The following examples illustrate the method described above.

```
a) Given: p = 1 atmosphere, T = 300^{\circ} K

at u = 0.1, \tau = 0.583, A = 0.417

at u = 0.2, \tau = 0.439, A = 0.561

Find: \tau at u = 0.17 for p = 1 atm., T = 300^{\circ} K

Procedure: A(0.1) = 0.417; f(0.1) = .8747

A(0.2) = 0.561; f(0.2) = .5780

\ln(0.1) = -2.3026

\ln(0.17) = -1.7720

\ln(0.2) = -1.6094

Hence: \Delta f = \frac{\partial f}{\partial (\ln u)} \Delta(\ln u) = \frac{0.5780 - 0.8747}{-1.6094 + 2.3026} (-1.7720 + 2.3026)

= \frac{-0.2967}{0.6932} 0.5306 = -0.2271

Therefore: f = f(0.1) + \Delta f = 0.8747 - 0.2271 = 0.6476

\tau(0.17) = 1 - e^{-0.6476} = 0.477
```

b) Given: p = 1 atmosphere, $T = 300^{\circ} K$ at u = 2.0, $\tau = 0.648$, A = 0.352at u = 5.0, $\tau = 0.425$, A = 0.575 p = 0.5 atmospheres, $T = 300^{\circ} K$ at u = 2.0, $\tau = 0.715$, A = 0.285at u = 5.0, $\tau = 0.545$, A = 0.455Find: $\tau(p,u)$ at u = 3.2, p = 0.75, $T = 300^{\circ} K$ Procedure: A(1,2.0) = 0.352; f = 1.0441A(1,5.0) = 0.575; f = 0.5534

A(0.5,2.0) = 0.285; f = 1.2553 A(0.5,5.0) = 0.455; f = 0.7875 ln(2.0) = 0.6931; ln(1.0) = 0.0000 ln(3.2) = 1.1631; ln(0.75) = -0.2877ln(5.0) = 1.6094; ln(0.5) = -0.6931

Hence:
$$\triangle f = \frac{\partial f}{\partial (\ln u)} \quad \triangle (\ln u) + \frac{\partial f}{\partial (\ln p)} \quad \triangle (\ln p)$$

$$= \frac{0.5534 - 1.0441}{1.6094 - 0.6931} \quad (1.1631 - 0.6931)$$

$$+ \frac{1.2553 - 1.0441}{-0.6931 + 0.0000} \quad (-0.2877)$$

$$= -0.2517 + 0.0877 = -0.1640$$

Therefore:
$$f(0.75,3.2) = f(1,2.0) + \Delta f = 1.0441 - 0.1640 = 0.8801$$

 $\tau (0.75,3.2) = 1 - e^{-0.8801} = 0.585$

The data contained in the Appendices of this report is available on tape. Inquiries as to the availability of taped copies should be sent to Gilbert N. Plass, Aeronutronic Division of Ford Motor Company, Newport Beach, California.

APPENDIX A

THE COEFFICIENTS ξ_{o} AND n FOR THE TOP FIVE INTENSITY DECADES

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APPENDIX B

WATER VAPOR TRANSMISSIONS FOR FREQUENCIES LESS THAN 3400 ${\rm cm}^{-1}$ AT 300°K, 250°K, AND 200°K

PRESSURE	
ATMOSPHERE	
1.00	
VAPOR	
WATER	

T=300°K

0 059 0 020 0.010	0.235 0.438 0.410 0.156 0.358 0.410 0.156 0.471 0.381 0.150 0.410 0.381 0.150 0.410 0.381 0.150 0.300 0.300 0.121 0.300 0.300 0.121 0.300 0.300 0.102 0.300 0.410	0.027 0.136 0.275 0.009 0.002 0.132 0.009 0.002 0.132 0.009 0.002 0.138 0.010 0.008 0.019 0.127 0.258 0.537 0.008 0.008	0.20 0.22 0.23 0.23 0.23 0.23	24462	20.00	0.34 0.21 0.20 0.20 0.20	0.274 0.453 0.587 0.480 0.712 0.824 0.601 0.815 0.905 0.444 0.660 0.765 0.291 0.481 0.611	*****	0.535 0.535 0.551	0.55 0.55 0.15 0.15 0.15 0.15 0.15 0.15	0.23 0.23 0.24 0.357	0.553 0.224 0.156	0.263 0.565 0.555	0.120	0.424 0.424 0.424	0.532	0.225 0.418 0.563 0.462 0.654 0.767 0.648 0.804 0.479 0.754 0.682 0.935 0.701 0.845 0.912	0.107	9.6.0	0.00	0.598 0.751 0.832 0.701 0.827 0.889 0.801 0.899 0.903 0.735 0.889 0.905 0.928 0.781 0.835	0.554 0.648 0.740 0.584 0.741 0.824 0.514 0.478 0.770 0.515 0.410 0.550	0.298 0.199 0.418 0.519 0.707 0.789 0.755 0.857 0.905 0.884 0.918 0.972 0.848 0.977 0.940
U(PR.CM.) 0.500 0.200 0.100	0.001 0.026 0.101 0.000 0.000 0.000 0.001 0.012 0.100 0.001 0.026 0.100 0.001 0.025 0.100 0.001 0.025 0.000 0.000 0.000 0.001 0.000 0.000 0.001 0.000 0.000 0.001		0.000 0.002 0.018 0.000 0.002 0.017 0.000 0.002 0.018 0.000 0.004 0.035 0.000 0.004 0.035	000000	00000	99999	0.002 0.033 0.135 0.007 0.094 0.266 0.013 0.148 0.369 0.012 0.116 0.253 0.006 0.005 0.159	24488	0.00	0.024	00000	0.000	200000	20000	0.000	0.001 0.004 0.145 0.005 0.009 0.204 0.004 0.047 0.183 0.003 0.010 0.008	0.003 0.056 0.108 0.047 0.167 0.306 0.101 0.306 0.407 0.143 0.404 0.602 0.120 0.352 0.543	0.074 0.201 0.450 0.034 0.176 0.359 0.014 0.098 0.222 0.005 0.041 0.103 0.020 0.090 0.146	0.268	0.000 0.247 0.429 0.042 0.159 0.249 0.049 0.216 0.300 0.049 0.216 0.309	0.125 0.249 0.455 0.163 0.404 0.567 0.264 0.525 0.684 0.205 0.444 0.610 0.146 0.345 0.495	0.054 0.253 0.381 0.072 0.253 0.426 0.054 0.215 0.346 0.052 0.158 0.284	0.004 0.044 0.162 0.114 0.271 0.410 0.250 0.465 0.438 0.372 0.450 0.794 0.331 0.507 0.747
3 000 2 000 1 100	0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000	000000000000000000000000000000000000000	000000	00000	00000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	00000	00000	90000	000000	00000	00000	00000	0.000	90000	0.000 0.000 0.000 0.000 0.000 0.004 0.000 0.001 0.021 0.000 0.002 0.021	0.000	90000	000000	0.000 0.000 0.043 0.000 0.010 0.048 0.000 0.017 0.098 0.000 0.010 0.048		66666
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0.050 0 020 0.010		0.000	11222	55555	0.609 0.754 0.632 0.455 0.638 0.745 0.316 0.522 0.655 0.221 0.472 0.610	505.5	22423	0.212 0.417 0.614 0.349 0.356 0.690 0.340 0.358 0.690 0.366 0.625 0.151 0.291 0.415 0.602	22122	25000	11000	0.556	2000	0.276	9255	0.22	0.034 0.157 0.297 0.017 0.089 0.191 0.005 0.043 0.199 0.039 0.127 0.227 0.124 0.392 0.442	0.226	2000	0.180 0.385 0.535 0.173 0.373 0.528 0.229 0.410 0.545 0.453 0.675 0.733 0.673 0.863 0.829	0.792 0.481 0.936 0.760 D.878 0.932 0.410 0.767 0.835 0.892 0.481 0.794 0.509 0.698 0.808	0.569 0.744 0.857 0.414 0.785 0.872 0.455 0.794 0.875 0.547 0.752 0.847	25000
UPR CM.) 0.500 0,200 0.100	0.137 0.559 0.137 0.559 0.137 0.437 0.731 0.137 0.731 0.137 0.107 0.109 0.407 0.409 0.407 0.409 0.407 0.409	0.277 0.312 0.552 0.000 0.132 0.552 0.222 0.581 0.592 0.323 0.553 0.592 0.322 0.593 0.793 0.352 0.373 0.773	0.05 0.70 0.05 0.10 0.05 0.11 0.067 0.11	0.054 0.170 0.024 0.124 0.070 0.114 0.070 0.254	0.05	20.00	0.00	0.002 0.004 0.131 0.005 0.004 0.188 0.005 0.001 0.177 0.008 0.001 0.727 0.005 0.050	0.603 0.005 0.033 0.104 0.036 0.390 0.056 0.290	20000	00000	0.02	0.000	0.0000	00000	90.00	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000	90000	32425	172.1	0.044 0.234 0.414 0.044 0.254 0.414 0.044 0.273 0.444 0.044 0.210 0.392	22222
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0.050 0.020 0.010	0.161 0.872 0.926 0.906 0.904 0.938 0.908 0.907 0.908 0.909 0.902 0.908 0.809 0.909 0.908 0.189 0.819 0.918	0.914 0.915 0.016 0.018 0	0.712 0.874 0. 0.631 0.770 0. 0.581 0.627 0. 0.489 0.667 0.	0.781 0.881 0.781 0.871 0.781 0.871 0.875 0.860 0.975 0.960 0.975 0.960 0.975 0.960	000000000000000000000000000000000000000	0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61	0.520 0.530	0.80 0.40 9.797 0.40 9.754 0.411 0. 0.761 0.411 0.	0.782 0.483 0.787 0.483 0.483 0.480 0.701 0.483	00000	6.95 6.95 6.95 6.95 6.95 6.95 6.95 6.95	00000	701 0.000 0.	200	22. 0.402 p. 27. 0	727 0.682 0.
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WATER VAPOR AT 0.50 ATMOSPHERE PRESSURE

1=300 K

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PRESSURE	
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WATER VAPOR AT 0.10 ATMOSPHERE PRESSURE

T=300° K

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	UPP.CAL) 0.500 0.200 0.100	0,498 0,999 1,000 0,999 1,000 1,000 1,000 1,000 1,000 0,999 1,000 1,000 0,999 0,999	0.938 0.949 0.948 0.999 0.999 0.999	0.999 1.000 1.000 0.999 1.000 1.000 0.998 0.998 0.998 0.993 0.997 0.998	1,000 1,000 1,000 1,000 1,000 1,000		1,996 1,036 1,996 0,998 1,996 0,998 1,996 0,998	8888	0.992 0.998 0.998 1.000 1.000 1.000 0.998 0.998	*****			*****				*****	*****		11111		0.991 0.995 0.964 0.990 0.953 0.993 0.995 0.993	2.992 0.993 2.991 0.995 2.990 0.995 3.992 0.995	0.491 0.492 0.485 0.492 0.487 0.993	0.980 0.980 0.984 0.981 0.990 0.994 0.984 0.991 0.995 0.986 0.995 0.995 0.985 0.995	3,445 0,443 1,452 0,494 1,492 0,494 1,496 0,494
	5,000 2,000 1,000	0.994 0.994 0.994 0.994 0.998 0.999 0.999 0.999 1.000 0.998 0.999 0.999 0.991 0.995 0.997	0.931 0.989 0.993 0.931 0.989 0.991 0.981 0.989 0.998 0.987 0.998 0.999	0.996 0.999 0.999 0.994 0.999 0.998 0.981 0.989 0.998 0.971 0.983 0.989	0.000 0.000						0.968 0.993 0.995 0.964 0.938 0.988 0.936 0.938 0.978 0.956 0.933 0.981	0.093 0.993 0.998 0.083 0.993 0.998 0.913 0.987 0.991 0.984 0.978 0.988 0.981 0.978 0.984	0.91 0.981 0.987 0.972 0.985 0.995 0.962 0.973 0.987 0.935 0.902 0.905 0.914 0.949 0.967	0.907 0.944 0.963 0.901 0.945 0.969 0.837 0.836 0.927 0.837 0.867 0.908	0.769 0.662 0.402 0.842 0.647 0.927 0.916 0.948 0.963 0.974 0.984 0.989						0.676 0.922 0.946 0.681 0.925 0.948 0.922 0.952 0.988 0.931 0.977 0.986 0.98 0.981 0.988	0.942 0.944 0.946 0.907 0.942 0.940 0.898 0.936 0.936 0.926 0.934 0.949 0.944 0.938 0.946	0.961 0.976 0.984 0.942 0.964 0.974 0.933 0.959 0.972 0.960 0.972 0.974		00.000	0.936 0.960 0.913 0.932 0.938 0.933 0.942 0.996 0.936 0.955 0.933 0.982 0.966 0.980 0.982
	3, 50.00 20.00 10,00	6 0.982 0.984 0.985 0 0.990 0.996 0.998 5 0.979 0.996 0.998	.5 0.932 0.960 0.972 .5 0.940 0.941 0.943 .6 0.963 0.949 0.966 .5 0.983 0.992 0.905	0.982 0.991 0.994 0.912 0.985 0.950 0.913 0.960 0.913 0.901 0.913 0.918 0.905 0.911 0.959	2 0.940 0.944 0.975 0 0.972 0.985 0.992 0.971 0.985 0.992 0.971 0.985 0.998	0 0.885 0.926 0.947 0 0.924 0.953 0.967 0 0.924 0.953 0.967 0.941 0.978 0.965 0.941 0.979 0.966	5 0.461 0.976 0.985 5 0.876 0.920 0.945 0 0.873 0.920 0.945 5 0.913 0.942 0.945	0 0.939 0.937 0.984 0 0.933 0.986 0.993 0 0.938 0.945 0.993 0.933 0.945 0.953 0.947 0.952 0.930	5 0.442 0.902 0.930 0.902 0.942 0.959 0.912 0.955 0.950 0.974 0.955 0.940 0.947 0.955 0.940	.0 0.810 0.922 0.944 .5 0.839 0.047 0.923 .0 0.417 0.922 0.945 .0 0.976 0.968 0.992	0.934 0.934 0.982 0.886 0.929 0.940 0.840 0.844 0.927 0.863 0.913 0.938 0.934 0.939 0.922	0.975 0.988 0.992 0.951 0.972 0.962 0.916 0.950 0.908 0.877 0.924 0.948	0.885 0.924 0.952 0.886 0.958 0.959 0.866 0.917 0.943 0.730 0.825 0.976	0.713 0.513 0.808 0.046 0.503 0.860 0.052 0.707 0.832 0.557 0.694 0.775 0.475 0.628 0.722	0.567 0.710 0.713 0.587 0.710 0.785 0.710 0.645 0.987 0.910 0.945 0.962 0.911 0.959 0.973	0.848 0.934 0.935 0.848 0.904 0.935 0.838 0.847 0.928 0.868 0.917 0.928 0.903 0.900 0.959	0.910 0.945 0.963 0.852 0.93, 0.435 0.878 0.924 0.948 0.848 0.931 0.952 0.917 0.949 0.965	.0 0.947 0.969 0.919 .5 0.937 0.942 0.915 .0 0.848 0.937 0.95 .5 0.842 0.900 0.933 .0 0.827 0.889 0.922	5 0.84) 0.91) 0.93 0 0.919 0.951 0.963 15 0.944 0.981 0.988 10 0.945 0.988 0.979 15 0.835 0.842 0.923	0 0.721 0.613 0.865 0 0.721 0.600 0.855 0 0.789 0.862 0.902 0.931 0.838 0.929 0 0.745 0.831 0.878	5 0.649 0.763 0.628 0.762 0.772 0.635 0.765 0.917 0.443 0.865 0.917 0.443 5 0.881 0.929 0.952	.5 0.725 0.882 0.917 .5 0.725 0.818 0.869 .0 0.700 0.852 0.857 .5 0.776 0.854 0.896 .0 0.878 0.925 0.848	0 0.670 0.919 0.944 0 0.7818 0.8819 0.917 0 0.825 0.850 0.923 0 0.825 0.890 0.923	0 0.820 0.845 0.418 5 0.757 0.811 0.886 5 0.774 0.881 0.844 5 0.732 0.827 0.877	5 0.764 0.844 0.843 0 0.772 0.853 0.843 5 0.865 0.876 0.913 0 0.836 0.848 0.929 5 0.837 0.898 0.929	0 0.748 0.671 0.909 5 0.787 0.663 0.904 0 0.481 0.907 0.918 0 0.880 0.928 0.951
	- FE	2560.0 2562.5 2562.5 2562.6 2562.5 2576.6	25555	*****	20000	22222	22222		16222	44444	22222	2265	10000		iiii	iiiii		2762.5	******		274 280 280 280 280 280 280 280 280 280 280	2222	*****	2222	22222	2460.0 2462.5 2467.5 247.5 247.5
SSURE	0.005 0.002 0.003	00000	88888	88888	99999	888888	200000	88888	88888	88888	88888	88888	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	88888	000000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 0.947 1.000 1.000	888	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	30000	88888		1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000		86666	66666	96666
ATMOSPHERE PRESSURE 0° K	0.050 0.020 0.010	0.999 0.999 0.999 0.999 0.999 0.999	0.999 0.999 0.999 1.000 0.999 1.000 0.999 0.999	******	000000	500000	000000	88888	88888	99998	000000	88888		88888	88888			88888	88888		86668	88888	88888	666666	88888	88888
	UPR.CM.) 0.500 0.700 0.100												0.446 0.442 0.300 0.445 0.442 0.300 0.444 0.404 0.908 0.444 0.906 0.908 0.447 0.908 0.908										1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	0.404 1.000 0.444 1.000 1.000 1.000	2,447 0,498 0,449 2,447 0,498 0,499 2,498 0,499 0,499 3,498 0,499 0,499
Α	5,000 2,000 1,000			0.454 0.412 0.481 0.464 0.418 0.465 0.410 0.482 0.488 0.400 0.414 0.483		0.947 0.949 0.941 0.949 0.941 0.947 0.941 0.947	*****		0.446 0.441		0.414 0.401 0.444 0.471 0.401 0.400 0.400 0.416 0.418 0.411 0.418 0.414 0.414 0.487 0.401	0.946 0.948 0.949 0.949 0.949 0.938 0.949 0.996 0.998 0.949 0.994 0.998	0.995 0.497 0.416 0.494 0.416 0.991 0.416 0.991	0.445 0.444 0.444 0.447 0.448 0.444 0.445 0.448 0.444 0.444 0.448 0.448		0.993 0.998 0.999 0.981 0.993 0.992 0.988 0.988 0.992 0.988 0.981 0.988	0,941 0,988 0,992 0,992 0,994 0,997 0,992 0,994 0,497 0,995 0,994 0,499 0,998 0,499	0.498 0.498 1.000 0.480 0.984 0.494 0.480 0.988 0.492 0.481 0.988 0.492	0.916 0.999 0.499 0.918 0.948 0.949 0.918 0.948 0.949 0.917 0.918 0.949			0.995 0.996 0.999 0.993 0.996 0.997 0.994 0.996 0.997 0.996 0.996 0.999 0.999 1.000 1.000	0.999 1.000 1.000 0.999 1.000 1.000 0.998 0.999 1.000 0.998 0.999 0.995 0.997 0.499	0.945 0.947 0.949 0.945 0.948 0.949 0.948 0.999 0.999 0.948 0.999 1.000	0.441 0.441 0.448 0.441 0.445 0.447 0.445 0.448 0.449 0.445 0.448 0.449	0.940 0.494 0.994 0.940 0.994 0.994 0.940 0.994 0.994 0.987 0.495 0.995 0.987 0.492 0.495
WATER VAPOR	30.00 20.00 10.00	0.852 0.402 0.434 0.815 0.882 0.417 0.816 0.815 0.417 0.815 0.412	0.413 0.446 0.450 0.413 0.406 0.421 0.403 0.403 0.421 0.403 0.413 0.413	0.831 0.906 0.434 0.816 0.924 0.447 0.846 0.916 0.936 0.868 0.917 0.940				0.917 0.452 0.914 0.924 0.953 0.988 0.921 0.932 0.981 0.915 0.937 0.984 0.420 0.951 0.967	0.417 0.930 0.944 0.411 0.944 0.941 0.913 0.947 0.964 0.926 0.935 0.789	0.431 0.431 0.481 0.442 0.413 0.483 0.442 0.442 0.973 0.443 0.445 0.473	0,939 D.981 0,934 0,905 0.912 0,901 0,807 0.915 0,912 0,872 0.920 0,914	0.981 0.930 0.994 0.983 0.942 0.983 0.953 0.982 0.983 0.951 0.973 0.983	0.968 0.987 0.988 0.922 0.912 0.919 0.928 0.912 0.988 0.958 0.919 0.988	0.467 0.994 0.994 0.465 0.943 0.995 0.979 0.967 0.991 0.972 0.984 0.991	0.961 0.927 0.985 0.936 0.924 0.982 0.962 0.927 0.984 0.927 0.927 0.991 0.926 0.992 0.995	0.915 0.987 0.992 0.912 0.985 0.991 0.915 0.986 0.913 0.957 0.914 0.955 0.900 0.914 0.955	0.934 0.782 0.972 0.948 0.982 0.948 0.939 0.983 0.993 0.939 0.943 0.993	0,444 0,445 0,447 0,414 0,416 0,017 0,417 0,419 0,413 0,414 0,413 0,413	0.42/ 0.944 0.944 0.930 0.790 0.941 0.939 0.948 0.943 0.983 0.991 0.944 0.940 0.973 0.944	0.911 0.91		0.917 0.988 0.916 0.927 0.916 0.927 0.917 0.931	0.491 0.441 0.448 0.492 0.491 0.48 0.487 0.444 0.45 0.478 0.446 0.45	0.471 0.957 0.982 0.987 0.993 0.994 0.997 0.994 0.995 0.991 0.997 0.998	0.415 0.962 0.931 0.962 0.918 0.984 0.944 0.979 0.964 0.919 0.989 0.993	0.465 0.486 0.486 0.481 0.438 0.485 0.451 0.438 0.485 0.451 0.482 0.481 0.456 0.498 0.438
*	5	2252.0	22222	22722 2272 2072 2072		2362.5	210.2		20000	2000	2362.5 2362.5 2362.5 2362.5	707077	2345.5	2187.5 2185.5 2185.5 2185.5		2222	2412		7,550			22025 22025 22025 22025 22025	22222			2552 2552 2552 2553 62765
	0.003 0 002 0.001	0.91. 0.91 0.94 0.915 0.985 0.99 0.95 0.915 0.92 0.94 0.84 0.918 0.95 0.978 0.98	0.441 0.442 0.442 0.441 0.442 0.445 0.440 0.444 0.444	0.441 0.444 0.442 0.410 0.414 0.442 0.412 0.411 0.414	0.992 0.455 0.955 0.992 0.492 0.995 0.992 0.993 0.995 0.992 0.993 1.000	0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4%	0.447 0.442 0.445 0.445 0.447 0.444 0.447 0.448 0.444 0.446 0.448 0.449	0.984 0.992 0.993 0.984 0.992 0.993 0.978 0.987 0.993 0.974 0.984 0.989 0.981 0.988 0.992	0.942 0.995 0.994 0.942 0.995 0.997 0.945 0.946 0.948 0.997 0.948 0.998	0.41 0.44 0.44 0.41 0.44 0.44 0.41 0.44 0.44	0.444 0.497 0.434 0.404 0.414 1.000 1.000 1.000 1.000 0.404 1.000 1.000 0.404 0.404 0.404	0.008 0.002 0.005 0.017 0.006 0.000 0.017 0.006 0.000 0.006 0.002 0.004 0.005 0.007 0.006	0.946 0.998 0.998 0.946 0.998 0.998 0.947 0.998 0.498	0.446 0.998 0.934 0.416 0.402 0.403 0.416 0.402 0.403 0.946 0.401 0.403	0.492 0.492 0.493 0.497 0.493 0.494 0.497 0.493 0.494 0.497 0.493 0.494	0.945 0.942 0.944 0.941 0.944 0.944 0.994 0.994 0.998 0.944 0.994 0.994	0.994 0.998 0.999 0.994 0.998 0.999 0.999 0.999 0.999 0.999 0.999 0.999	0,941 0,445 0,442 0,944 0,944 0,944 0,944 0,444 0,444 0,444 0,444 0,444	0.444 0.444 0.444	0.005 0.007 0.006 0.007 0.006 0.006 0.008 0.009 1.000 0.009 0.009 1.000	0.444 0.444 1.000 0.944 1.005 1.000 0.944 0.944 1.000 0.949 0.944 1.000	0.447 0.448 0.444	0.999 1.000 1.000 0.999 0.999 0.999 0.999 0.999	0.997 0.998 0.999 0.998 0.998 (.000 0.999 1.000 (.000 1.000 1.000 1.000	1,000 1,000 1,000 0,999 1,000 1,000 0,999 0,999 1,000 0,994 0,999 1,000	0.444 0.449 1.000 0.444 0.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000
	0 030 0,020 0 010	0.427 0.428	0.410 0.479	0.015 0.073 0.042 0.073 0.043 0.050 0.043 0.050	0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010	00.000	0.457 0.453 0.481 0.982 0.984 0.493 0.990 0.994 0.494 0.986 0.992 0.994 0.911 0.482 0.994	0.916 0.916 0.985 0.916 0.916 0.918 0.926 0.955 0.948 0.918 0.948 0.945	0.93 0.93 0.98 0.93 0.93 0.98 0.91 0.91 0.99 0.98 0.99 0.99	0.481 0.489 0.443 0.459 0.413 0.481 0.438 0.481 0.473 0.438 0.450 0.471	0.455 0.451 0.094 0.445 0.497 0.498 0.447 0.494 0.493 0.446 0.498 0.497	0.928 0.916 0.922 0.928 0.913 0.967 0.925 0.913 0.967 0.916 0.972 0.961 0.918 0.990 0.993	0.98 0.992 0.994 0.98 0.990 0.994 0.986 0.991 0.974 0.988 0.992 0.995	0.982 0.990 0.993 0.981 0.985 0.983 0.981 0.980 0.883 0.985 0.983 0.987 0.986 0.991	0.40 0.494 0.494 0.40 0.492 0.493 0.44 0.492 0.493 0.44 0.492 0.493	0.980 0.988 0.992 0.975 0.985 0.990 0.974 0.986 0.990 0.983 0.990 0.994 0.987 0.993 0.994	0.462 0.443 0.443 0.403 0.444 0.444 0.446 0.444 0.444 0.446 0.444 0.444	0.940 0.940 0.984 0.940 0.941 0.983 0.940 0.941 0.988 0.940 0.948 0.993	0.941 0.940 0.934 0.945 0.992 0.995 0.945 0.995 0.995 0.980 0.986 0.993 0.981 0.986 0.993	0.91 0.91 0.92 0.97 0.99 0.99 0.99 0.99 0.99 0.92 0.99 0.99	0.494 0.497 0.448 0.407 0.448 0.499 0.448 0.497 0.949 0.448 0.497 0.348	0.445 0.442 0.445 0.947 0.493 0.495 0.947 0.994 0.497 0.947 0.999 0.999 0.998 0.999			0.000 0.000	0.994 0.994 0.994 0.999 0.999 0.999 0.999
	UPR.CM.) 0.500 0.200 0.100	0.117 0.952 0.448 0.774 0.844 0.849 0.840 0.751 0.818 0.578 0.704 0.185 0.400 0.771 0.855	0.652 0.873 0.910 0.011 0.901 0.93 0.892 0.913 0.95 0.900 0.918 0.93	0.014 0.948 0.484 0.819 0.882 0.918 0.738 0.872 0.870 0.748 0.831 0.877	0.957 0.915 0.984 0.955 0.976 0.987 0.985 0.980 0.980 0.972 0.985 0.990	0.91e 0.449 0.465 0.790 0.862 0.901 0.652 0.765 0.629 0.634 0.752 0.819 0.739 0.826 0.614	0.450 0.412 0.438 0.434 0.442 0.473 0.95 0.478 0.480 0.95 0.471 0.480	*****	19177	7777	:::::	*****	0.000	43334	*****	*****	*****	27522	0.911 0.413 0.914 0.914 0.914 0.918 0.918 0.918 0.918 0.918 0.918	0.939 0.941 0.973 0.941 0.944 0.754 0.941 0.180 0.973 0.944 0.989 0.973 0.987 0.989	0.982 0.448 0.942 0.989 0.994 0.995 0.912 0.495 0.993 0.944 0.990 0.993	0.936 0.949 0.978 0.936 0.933 0.981 0.936 0.986 0.989 0.990 0.994 0.990 0.931 0.995 0.994	0.987 0.982 0.985 0.981 0.988 0.982 0.985 0.989 0.985 0.952 0.984 0.985	0.941 0.941 0.942 0.934 0.943 0.942 0.936 0.945 0.940 0.936 0.947 0.948	0.487 0.493 0.993 0.913 0.949 0.993 0.913 0.982 0.989 0.910 0.982 0.988	0.913 0.914 0.919 0.312 0.914 0.993 0.914 0.913 0.993 0.934 0.934 0.991
	5.000 2.000 1.000	0.454 0.454 0.475 0.454 0.454 0.494 0.267 0.424 0.514 0.187 0.254 0.457	0.450 0.627 0.724 0.431 0.687 0.782 0.681 0.780 0.413 0.680 0.783 0.617 0.674 0.783 0.617	0.701 0.817 0.875 0.525 0.868 0.755 0.380 0.318 0.845 0.423 0.386 0.845 0.625 0.738 0.805	0.824 0.900 0.935 0.824 0.933 0.885 0.922 0.948 0.882 0.935 0.935	0.104 0.820 0.817 0.422 0.823 0.115 0.200 0.420 0.544 0.220 0.343 0.521 0.187 0.547 0.652	0.541 0.725 0.803 0.763 0.857 0.903 0.857 0.917 0.945 0.835 0.900 0.931 0.715 0.815 0.848	0.556 0.771 0.518 0.564 0.776 0.783 0.461 0.615 0.710 0.367 0.367 0.673 0.521 0.664 0.749	0.613 0.788 0.634 0.712 0.813 0.631 0.781 0.659 0.630 0.834 0.930 0.633	0.186 0.865 0.404 0.642 0.757 0.627 0.519 0.661 0.747 0.502 0.649 0.337	0.931 0.895 0.927 0.915 0.951 0.947 0.924 0.957 0.972 0.924 0.937 0.938	0.455 0.466 0.781 0.455 0.466 0.781 0.453 0.485 0.780 0.455 0.737 0.514 0.405 0.818 0.514	0.638 0.700 0.430 0.638 0.848 0.428 0.849 0.405 0.433 0.861 0.419 0.443	0.747 0.879 0.409 0.6071 0.779 0.619 0.500 0.719 0.744 0.617 0.772 0.819 0.747 0.647 0.649	0.816 0.923 0.947 0.882 0.927 0.949 0.836 0.908 0.935 0.811 0.875 0.935 0.824 0.867 0.920	0.786 0.880 0.900 0.731 0.836 0.887 0.785 0.844 0.887 0.875 0.849 0.918	0.421 0.444 0.417 0.439 0.479 0.427 0.448 0.429 0.450 0.436 0.442 0.434 0.431 0.402 0.430	0.704 0.850 0.851 0.844 0.718 0.823 0.718 0.811 0.845 0.792 0.884 0.904	0.617 0.887 0.914 0.61 0.889 0.928 0.625 0.837 0.918 0.605 0.877 0.908	0.812 0.813 0.914 0.819 0.883 0.914 0.859 0.909 0.915 0.913 0.945 0.942 0.913 0.945 0.948	0,939 0,942 0,914 0,944 0,948 0,948 0,948 0,947 0,977 0,948 0,947 0,973	0.846 0.910 0.329 0.845 0.913 0.938 0.917 0.947 0.945 0.345 0.919 0.945	0.954 0.973 0.981 0.935 0.740 0.972 0.889 0.939 0.930 0.851 0.905 0.931 0.820 0.854 0.918	0.820 0.884 0.917 0.884 0.919 0.940 0.924 0.931 0.986 0.975 0.982 0.988	0.955 0.971 0.981 0.917 0.941 0.913 0.910 0.944 0.941 0.904 0.939 0.938	0.915 0.944 0.942 0.945 0.944 0.945 0.945 0.945 0.946 0.946 0.948 0.948
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	0 2.000 1.000 0.50	0.987 0.984 0.986 0.986 0.986 0.986 0.986 0.986 0.986	0.979 0.993 0.971 0.988 0.973 0.988 0.980 0.993 0.988 0.994	95.00	0.985 0.996 0.985 0.996 0.986 0.995 0.985 0.995 0.989 0.981	0.932 0.967 0.932 0.966 0.956 0.960 0.983 0.993	0.981 0.992 0.942 0.971 0.905 0.951 0.905 0.951 0.943 0.971	0.980 0.992 0.981 0.992 0.928 0.962 0.877 0.934	0.878 0.934 0.929 0.963 0.980 0.992 0.956 0.979	0.856 0.945 0.861 0.925 0.867 0.939 0.479 0.932	0.470 0.986 0.911 0.953 0.851 0.926 0.932 0.931	0.474 0.442 0.471 0.487 0.452 0.478 0.416 0.457 0.875 0.946	0.913 0.954 0.954 0.918 0.918 0.918 0.940	0.855 0.925 0.785 0.925 0.785 0.785 0.653 0.794 0.497 0.679	0.425 0.619 0.516 0.680 0.520 0.621 0.893 0.943	0.910 0.810 0.910 0.910 0.910 0.910 0.910	0.919 0.917 0.837 0.937 0.887 0.938 0.987 0.938	55555	0.859 0.922 0.417 0.997 0.431 0.440 0.431 0.478	0.440 0.814 0.681 0.809 0.798 0.884 0.867 0.430	0.475 0.415 0.635 0.414 0.437 0.412	0.865 0.928 0.786 0.870 0.743 0.857 0.826 0.906 0.824 0.944	0.415 0.415 0.415 0.415 0.415 0.415	3 0.801 0.947 0.947 7 0.851 0.925 0.942 8 0.808 0.901 0.950 1 0.823 0.907 0.954	0.841 0.931 0.075 0.930 0.895 0.949 0.884 0.951	0.857 0.627 0
	FREQ. 50.00 20.00 10.00 5.00	0.317 0.453 0.428 0.347 0.459 0.459 0.355 0.468 0.651 0.350 0.467 0.650		0.680 0.845 0.571 0.840 0.599 0.738 0.538 0.738	1591.5 0.223 0.609 0.192 0.002 1600.0 0.330 0.669 0.652 0.431 1600.0 0.331 0.670 0.633 0.931 1607.5 0.261 0.573 0.758 0.677	0.185 0.472 0.673 0.185 0.469 0.672 0.244 0.555 0.745 0.114 0.652 0.878 0.313 0.652 0.828	0.306 0.642 0.226 6.326 0.136 0.418 0.134 0.419 0.223 0.523	0.247 0.637 0.817 0.308 0.644 0.831 0.220 0.506 0.692 0.128 0.305 0.692		0.153 0.412 0.607 0.009 0.326 0.529 0.160 0.414 0.603 0.233 0.562 0.743 0.303 0.641 0.817	0.265 0.594 0.703 0.171 0.446 0.644 0.107 0.339 0.539 0.145 0.386 0.774	1685.0 0.787 0.486 0.816 0.919 1685.5 0.263 0.596 0.786 0.909 1690.0 0.205 0.599 0.795 1695.0 0.130 0.192 0.598 0.761	0.179 0.459 0.654 0.211 0.524 0.122 0.201 0.516 0.127 0.120 0.394 0.616 0.012 0.502 0.530	0.032 0.236 0.487 0.032 0.138 0.461 0.032 0.138 0.365 0.013 0.043 0.223	0.001 0.015 0.015 0.081 0.088 0.264 0.153 0.435 0.181 0.498	0.139 0.423 0.638 0.099 0.346 0.555 0.089 0.331 0.452 0.135 0.409 0.623 0.174 0.485 0.687	0.157 0.547 0.150 0.445 0.117 0.380 0.114 0.369	0.214 0.536 0.730 0.73, 0.542 0.747 0.153 0.455 0.477 0.091 0.338 0.557 0.010 0.287 0.494	0.128 0.373 0.565 0.190 0.491 0.685 0.247 0.600 0.797 0.201 0.537 0.738 0.124 0.356 0.531	783,6 0.056 0.180 0.127 0.485 7780,0 0.072 0.275 0.465 0.455 7782,5 0.082 0.252 0.535 0.714 7782,5 0.082 0.252 0.538 0.512	0.015 0.103 0.245 0.025 0.142 0.301 0.017 0.291 0.493 0.141 0.451 0.674	5000	0.140 0.431 0.645 0.040 0.320 0.533 0.080 0.340 0.464 0.083 0.315 0.429 0.121 0.405 0.429	0.100 0.357 0.537 0.068 0.271 0.462 0.074 0.174 0.340 0.034 0.197 0.404 0.052 0.254 0.477	0.054 0.270 0.444 0.064 0.300 0.529 0.100 0.394 0.579 0.112 0.384 0.405	0.044 0.242 0.045 0.243 0.050 0.342 0.115 0.347
-	100.0		_	000000000000000000000000000000000000000			000001	00001	000011	020011	900000	00001	1,000	1,000	1,000	0001 0001 0001 0001	0000 1,000 1,000 1,000	0001	888888	1.000	900011	1.000	1.600 1.000 1.000 1.000	1.000	1.000	000000
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•	5,000 2,000 1,000	0.814 0.412 0.411 0.783 0.414 0.413 0.787 0.427 0.443 0.620 0.427 0.464	0.844 0.444 0.481 0.884 0.439 0.987 0.884 0.431 0.993 0.884 0.438 0.984 0.839 0.444 0.478	0.837 0.440 0.434 0.851 0.452 0.467 0.857 0.450 0.467 0.858 0.456 0.467 0.858 0.456 0.464	0.674 0.947 0.990 0.885 0.949 0.990 0.880 0.942 0.984 0.870 0.942 0.984	0.840 0.456 0.483 0.876 0.465 0.484 0.876 0.465 0.488 0.888 0.472 0.491 0.887 0.478 0.493	0,407 0,481 0,444 0,401 0,474 0,444 0,841 0,473 0,441 0,840 0,472 0,491 0,894 0,475 0,493	0.405 0.478 0.494 0.403 0.478 0.494 0.402 0.402 0.495 0.402 0.477 0.495	0.895 0.975 0.992 0.896 0.975 0.991 0.896 0.976 0.993 0.905 0.913 0.993	0.414 0.485 0.494 0.418 0.485 0.497 0.420 0.485 0.407 0.417 0.485 0.497		0.925 0.486 0.998 0.925 0.986 0.998 0.925 0.986 0.998 0.924 0.486 0.998 0.925 0.986 0.997		0.424 0.984 0.498 0.924 0.988 0.446 0.924 0.489 0.948 0.928 0.488 0.998 0.928 0.489 0.998				0.933 0.990 0.993 0.908 0.973 0.991 0.908 0.973 0.991 0.908 0.978 0.991 0.933 0.984 0.994				0.937 0.990 0.997 0.935 0.988 0.997 0.937 0.989 0.997 0.936 0.989 0.997		0.437 0.484 0.497 0.433 0.434 0.497 0.438 0.497 0.497		8.434 0.445 0.445 0.432 8.444 0.444 0.431 8.444 0.445 0.431 8.442 0.444
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_	911			22222																		2322.5	22222	20222		
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	003 0.002 0.001	****		0.793 0.875 0.909 0.703 0.804 0.840 0.454 0.755 0.827 0.765 0.855 0.895		0.000	*****	27474		*****	0.115 0.117 6.45 0.713 0.415 6.45 0.708 0.412 0.45 0.863 0.913 0.437 0.824 0.887 0.427	00000	*****	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.450 0.455 0.461 0.450 0.471 0.481 0.406 0.404 0.461 0.830 0.404 0.431	2444	0.00	10000	124.22		0.414 0.444 0.444 0.421 0.444 0.444 0.421 0.430 0.444 0.421 0.427 0.444	*****	*****	7		£1111
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	90 00 30:00 10 00	0000 0000 00000	88888	0.000 0	00000	00000	0.000 0.000 0.000	99999	96666	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	00000	00000	00000	99999	0.000 0.000 0.001 0.000 0.000 0.001 0.000 0.000 0.001 0.000 0.000 0.000	88888	0.000	120000	00000	0.000	0.000 0.001 0.011 0.000 0.005 0.011 0.000 0.001 0.011 0.000 0.000 0.003	0.0000	00000	2000	22200	6,000 0.601 0.004 0.001 0.044 0.122 0.008 0.644 0.233 0.018 0.146 0.343
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	0.050 0.020 0.010	1111		0.418 0.451 0.454 0.418 0.454 0.454 0.404 0.454 0.444 0.444 0.454				0.893 0.895 0.892 0.893 0.800 0.932 0.787 0.884 0.908 0.784 0.852 0.894 0.738 0.824 0.877	0.742 0.831 0.829 0.728 0.897 0.889 0.804 0.881 0.918 0.894 0.909 0.940	0.857 0.914 0.944 0.752 0.617 0.884 0.445 0.778 0.841	0.734 0.843 0.890 0.805 0.886 0.414 0.806 0.878 0.415 0.831 0.897 0.430	0.442 0.775 0.834 0.874 0.775 0.834 0.848 0.984 0.991 0.948 0.994 0.991	0.519 0.884 0.906 0.782 0.884 0.906 0.654 0.746 0.830 0.510 0.647 0.719 0.443 0.614 0.710	0.582 0.707 0.783 0.730 0.828 0.879 0.811 0.884 0.920 0.788 0.867 0.908 0.708 0.867 0.861	0.574 0.711 0.708 0.592 0.723 0.747 0.707 0.608 0.642 0.812 0.884 0.421 0.640 0.891 0.924	0.652 0.754 0.834 0.652 0.764 0.834 0.637 0.757 0.826 0.627 0.796 0.826	0.342 0.442 0.723 0.472 0.732 0.823 0.389 0.725 0.802 0.411 0.619 0.712 0.374 0.445 0.654	0.441 0.414 0.712 0.574 0.721 0.403 0.573 0.717 0.744 0.411 0.413 0.744 0.544 0.413 0.744	0.370 0.342 0.453 0.434 0.394 0.709 0.341 0.703 0.744 0.409 0.734 0.410	0.502 0.439 0.731 0.345 0.530 0.440 0.277 0.451 0.573 0.347 0.524 0.432 0.3481 0.710 0.743	0.774 0.874 0.917 0.774 0.874 0.917 0.751 0.848 0.874 0.554 0.442 0.771 0.382 0.534 0.844	0.348 0.310 0.421 0.582 0.441 0.727 0.407 0.741 0.814 0.609 0.741 0.813	0.440 0.744 0.870 0.445 0.744 0.870 0.445 0.745 0.833 0.807 0.919 0.914	11111		17119
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	5,000 2,000	10000			0.524 0.55 0.524 0.696 0.402 0.585 0.274 0.454	0.145 0.244 0.186 0.244 0.283 0.481	1277	35555	25535	2000	25252		0.011 0.204 0.011 0.041 0.004 0.051 0.000 0.001		20121	10000	0.000	55555	0.0000	0.000	2000 C	2666		10.00		
	20,00 10,00	20000			0.260 0.457 0.172 0.377 0.117 0.251 0.057 0.118	0.014 0.024 0.024 0.034 0.014 0.014 0.014	0.001 0.001	000000	90000	00000	000000000000000000000000000000000000000	0.000	000000000000000000000000000000000000000	85566	00000		00000		99999	99969	000000000000000000000000000000000000000	90000	99999	0.000	00000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
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	FREG. 50.00 20.00 10.00	2540.0 0.973 0.987 0.997 2545.5 0.998 0.995 0.497 2545.0 0.998 0.998 1.000 2547.5 0.990 0.997 0.989 2770.0 0.884 0.998	0.947 0.971 0.971 0.914 0.984 0.995	0.914 0.914 0.974 0.991 0.925 0.939 0.921 0.933	0.934 0.424 0.938 0.441 0.937 0.442 0.935 0.442	2615.0 0.889 0.93 0.934 2615.0 0.931 0.932 0.933 2615.0 0.931 0.931 0.931 2617.3 0.931 0.987 0.993	0.94 0.94 0.94 0.94 0.94 0.912 0.912 0.912 0.912	0.465 0.483 0.474 0.491 0.474 0.488 0.847 0.416 0.820 0.885	0.872 0.886 0.873 0.983 0.975 0.989 0.976 0.989	0.147 0.401 0.147 0.400 0.812 0.401 0.411 0.440	0.453 G.972 0.860 G.912 0.753 G.861 0.413 C.865	0.475 0.484 0.913 0.474 0.915 0.475 0.642 0.915 0.460 0.915	0.831 0.844 0.931 0.944 0.831 0.887 0.772 0.856	0.758 0.848 0.704 0.604 0.573 0.703 0.424 0.583	0.354 0.532 0.415 0.625 0.442 0.787 0.475 0.925	0.858 0.413 0.784 0.413 0.784 0.847 0.634 0.867	0.400 0.41 0.643 0.417 0.623 0.640 0.870 0.420	0.923 0.937 0.920 0.954 0.782 0.915 0.783 0.982	0.002 0.034 0.005 0.034 0.012 0.004 0.777 0.001	0.725 0.737 0.735 0.633 0.735 0.633 0.635 0.730	0.554 0.554 0.593 0.721 0.738 0.027 0.678 0.027	7.000	0.83 0.932 0.870 0.988 0.774 0.988 0.879 0.982	0.255 0.413 0.784 0.844 0.644 0.813 0.740 0.823	0.767 0.810 0.810 0.903 0.903 0.913	0.831 0.900 0.810 0.883 0.884 0.904 0.885 0.934 0.885 0.934
	0.003 0.002 0.003	000110001	1,000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	2001	1.000 1	86666	1.000 1	0001	1.600 1.000 1	1.000 1.000	1.000 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1	1.000 1	1.000	1,000 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1	1.000 1.300 1.000 1	1.600 1.800 1.000 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000	000-1 000-1 000-1 000-1 000-1 000-1 000-1 000-1
	0.030 0.020 0.010	1.000 1.000	8888	90000	8888	88888	98888	88888	\$8888	88888	88988	88888	88888	00000	88888	88888	88666	88888	90000	88888	88888	88888	88888	88888		88888
2	UPP.CA.]	0.44 0.44 1.000 0.44 0.44 1.000 0.44 0.44 1.000 0.44 0.44 1.000	8888	86668	00000	88888	88888		88888	88808	88666	20000	9865	88888	2000	8888	8888	*****	33333			****	*****	88888	****	1.000 1.000
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	30 00 20,00 10,00	0.184 0.414 0.413 0.040 0.272 0.423 0.043 0.134 0.250 0.003 0.032 0.135 0.003 0.031		0.174 0.324 0.103 0.214 0.103 0.214 0.119 0.304	0.522 0.150 0.522 0.150 0.511 0.150 0.511 0.150	0.105 0.402	0.100 0.370 0.582 0.581	0.152 0.151	0.372	0.477 0.827 0.321 0.465 0.350 0.528 0.264 0.434 0.435 0.402	0.45 0.457 0.851 0.457 0.851 0.457 0.856 0.957 0.856 0.957	0.100 0.110	0.623 0.773 0.510 0.775 0.305 0.909 0.713 0.443	0.775 0.87	0.734 0.461 0.704 0.888 0.706 0.888 0.418 0.736	0.712 0.824	0.747 0.851 0.723 0.834 0.834 0.424 0.384 0.424	0.420 0.543 0.743 0.743 0.743 0.743 0.874	0.740 0.85	0.812	0.654 0.417	0.416 0.403 0.458 0.423 0.451 0.451 0.454 0.451	0.00	*****		22000
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WATER VAPOR AT 0.02 ATMOSPHERE PRESSURE

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	030 0.020 0.010	*****	22222	16883		46615	1111	22222	27272		45555	0.735 0.425 0.473 0.762 0.443 0.485 0.653 0.905 0.932 0.933 0.958 0.971 0.932 0.458 0.971	*****	1593	####		*****	*****	*****					11111		77711
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	200 2,000 1,000 0.	0.238 0.398 0.165 0.315 0.188 0.347 0.242 0.440	0.164 0.264 0.057 0.142 0.138 0.276 0.159 0.324	033 0-107 010 0-045 000 0-016 033 0-086	0.143 0.334 0.043 0.175 0.078 0.110	0.092 0.195 0.104 0.228 0.19 0.246 0.121 0.226	0.104 0.189 0.147 0.279 0.186 0.358 0.007 0.225	0.018 0.071 0.009 0.034 0.017 0.054 0.052 0.136 0.162 0.303	15111	0.314 0.472 0.558 0.474 0.501 0.601 0.323 0.601	0.2% 0.444 0.2% 0.429 0.277 0.419 0.129 0.244 0.107 0.223		0.108 0.439 0.128 0.539 0.285 0.423 0.102 0.210	0.052 0.142 0.250 0.254 0.251 0.405 0.251 0.405	0.463 0.599 0.527 0.500 0.367 0.506 0.188 0.314	0.169 0.302 0.286 0.430 0.546 0.542 0.544 0.668	0.507 D.425 0.503 0.624 0.725 0.618 0.725 0.648	0.422	0.437 0.5% 0.333 0.6% 0.234 0.54% 0.245 0.348		0.862 0.869 0.722 0.810 0.491 0.597 0.292 0.409 0.369 0.470	0.879 0.908 0.879 0.900 0.879 0.922 0.870 0.914 0.841 0.893	0.498 0.782 0.404 0.707 0.412 0.738 0.715 0.776	0.724 0.435 0.625 0.877 0.825 0.875 0.753 0.829	0.705 0.788 0.740 0.818 0.541 0.741 0.541 0.554	0.518 0.634 0.724 0.802 0.644 0.908 6.937 0.931 0.939 0.962
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APPENDIX C

WATER VAPOR TRANSMISSIONS AVERAGED OVER 20 cm⁻¹
WITH ENTRIES EVERY 10 cm⁻¹ FOR FREQUENCIES FROM
1000 cm⁻¹ TO 10,000 cm⁻¹ AT 300°K, 250°K, AND 200°K

0,902 0,901	******	20.000	2222	22223	0.443 0.751 0.541 0.701 0.345 0.515 0.153 0.243 0.105 0.244	0.124 0.441 0.417 0.444 0.452 0.465 0.417 0.409	0.810 0.872 0.719 0.882 0.445 0.759 0.453 0.757		0.772 0.888 0.795 0.842 0.806 0.812 0.816 0.877 0.816 0.877	*****	1111	****	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000				****	****	1.000 1.000	1,000 1,000		6.000 0.000 0.000 1.000 0.000 1.000 1.000 1.000			1.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.
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ŏ ⁷ 8	0.65 0.085 0.994 0.774 0.988 0.994 0.774 0.988 0.994 0.774 0.988 0.994	2.446 0.444 0.444 2.446 0.494 0.444 2.441 0.494 0.494 3.443 0.497 0.984	0.977 G.444 G.44 0.974 G.494 G.49 0.941 G.494 G.49 0.945 G.497 G.99	2.986 0.994 0.997 2.986 0.994 0.997 2.981 0.991 0.965 2.983 0.992 0.895 3.982 0.997 0.898	2.942 0.942 0.949 2.442 0.949 0.949 2.445 0.949 0.900 2.446 0.949 1.000 2.446 0.949 1.000	2.990 1.000 1.000 2.990 1.000 1.000 2.997 0.990 1.000 2.990 0.999 0.999			D. VR. D. VV. D.		0.055 0.056 0.055 0.056 0.052 0.056 0.054 0.077 0.09	2.942 0.465 0.99 2.942 0.465 0.99 2.947 0.987 0.99 2.942 0.985 0.99	0.945 0.945 0.948 0.945 0.975 0.988 0.917 0.911 0.974	0.857 0.424 0.434 0.829 0.402 0.434 0.839 0.808 0.442 0.784 0.872 0.414 0.750 0.848 0.848	7.00 0.847 0.84 0.705 0.814 0.87 0.874 0.835 0.83 0.831 0.844 0.93	0.718 0.850 0.89 0.513 0.511 0.116 0.384 0.557 0.67 0.540 0.676 0.74 0.711 0.824 0.88	0.512 0.713 0.144 0.534 0.480 0.748 0.594 0.790 0.807 0.387 0.514 0.573	0.216 0.411 0.55 0.516 0.611 0.55 0.512 0.616 0.61		*****	3.459 0.624 0.736 3.465 0.567 8.474 3.285 0.475 0.408 3.340 0.534 0.644	*****		3.264 0.478 0.420 3.200 8.404 0.541 3.144 0.557 0.511 3.103 0.275 0.431	1. 167 9. 362 0.51 2. 182 9. 258 0. 10 2. 028 9. 138 9. 27 2. 028 9. 129 9. 25
AT 1.0 T=	0.887 0.934 0.907 0.951 0.915 0.952 0.916 0.956 0.927 0.956			17172	*****	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	200000000000000000000000000000000000000	0.945 0.945 0.950 0.975 0.942 0.980 0.942 0.970	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	0.520 0.828 0.715 0.828 0.438 0.940	1865	19999		0.576 0.747 0.546 0.747 0.546 0.759 0.548 0.482	0.500 0.400 0.455 0.545 0.410 0.403 0.410 0.740	0.254 0.255 0.255 0.255 0.255 0.255 0.255 0.255	0.234 0.235 0.235 0.235 0.235 0.235		0.384 0.748 0.375 0.324 0.200 0.324 0.287 0.934	0.155 0.259 0.054 0.134 0.139 0.224 0.128 0.312	0.174 C.335 0.153 0.235 0.053 0.173 0.053 0.134	0.05 0.214 0.15 0.214 0.15 0.214 0.055 0.152	0.054 0.144 0.062 0.144 0.063 0.182 0.061 0.180		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
VAPOR	2777	2222	**************************************	*****	25552	2222		22422	0.762 0.833 0.764 0.833 0.764 0.875 0.774 0.875	14122	1445	13175	33553	18815	35653	20000	00000	00000 127 127 127 127	0.00.0	20000 20000 20000 20000 20000	00000	0.001 0.013 0.002 0.023 0.003 0.030 0.007 0.030	66666		000000000000000000000000000000000000000
ATER	24444						00.370 0.370 0.00 0.00 0.00 0.00 0.00 0.		0.0000000000000000000000000000000000000	0.0000 0.24 0.0000 0.20 0.0000 0.33 0.0000 0.33 0.0000 0.33 0.0000 0.33	0.22.0.5.5	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 0.25 0.00 0.25 0.00 0.25 0.00 0.25	000000	0.000	50000	000000000000000000000000000000000000000	99999	90000	96.69			2000		00000000000000000000000000000000000000
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.003 0.002 0.00)	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	00000	99999	2000	000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	200 0.000 0.000 200 0.000 0.000 200 0.000 0.000 200 0.000 0.000	.966 0.986 0.992 .962 0.984 0.992 .932 0.984 0.984 .932 0.986 0.984	.852 0.021 0.073 .856 0.021 0.058 .856 0.021 0.058 .768 0.850 0.027	0,774 0.865 0.875 0,778 0.850 0.891 0,777 0.865 0.895 0.873 0.895 0.895	.651 0.755 0.631 .656 0.780 0.636 .650 0.782 0.656 .640 0.774 0.656	. 153 0. 638 0. 73 . 178 0. 623 0.717 . 598 0. 386 0. 711 . 506 0. 664 0. 743 . 502 0. 647 0. 743	.516 D.684 D.775 .522 D.726 D.804 .804 D.800 D.018 .916 D.939 D.976	.741 G.651 0.902 .677 0.778 0.884 .657 0.781 0.849 .544 0.707 0.710	.523 0.681 0.777 .504 0.680 0.777 .504 0.680 0.758 .448 0.612 0.728	.444 D.408 C.716 .441 D.777 C.844 .735 C.828 D.800 .414 D.752 C.831	.451 D.780 O.855 .403 D.787 D.826 .400 D.787 D.832 .410 D.755 C.848	.75 0.457 0.477 .75 0.456 0.417 .75 0.454 0.406 .715 0.427 0.486	.879 0.493 0.932 .961 0.916 0.944 .989 0.916 0.944 .889 0.916 0.942	0.860 0.919 0.914 0.834 0.902 0.913 0.844 0.920 0.949 0.884 0.938 6.943	.926 0.942 0.978 .941 0.988 0.982 .954 0.958 0.952 .959 0.957 0.975	.014 0.471 0.484 .944 0.471 0.484 .947 0.985 0.993 .948 0.989 0.993	294 0.441 0.994 294 0.992 0.994 294 0.993 0.994 394 0.993 0.994			0001 0001 000 0001 0001 000 0001 0001 0
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NeR.CM.) NeR.CM.) 1 0.500 0.700 0.	00000	00000			6.0000		2222	0.151 0.151 0.051 0.151 0.051 0.151 0.052 0.158	55555	88888	99999	00000	38888	26666	88888	88888	20000	90000				17775	22.000	0.747 0.857 0.842 0.410 0.873 0.451 0.882 0.454	10717
3.000 2.000 1.000	0.416 0.476 0.401 0.410 0.476 0.400 0.428 0.462 0.495 0.426 0.481 0.495	*****	2222	0.586 0.450 0.021 0.617 0.800 0.845 0.559 0.756 0.850 0.601 0.776 0.860		10000	0.004 0.225 0.315 0.004 0.004 0.172 0.004 0.003 0.101 0.004 0.050 0.100 0.002 0.055 0.110	55250	00000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	90000	00000	00000	80000	00000	00000	0.050 0.000 0.002 0.000 0.000 0.002 0.000 0.000 0.001 0.000 0.000 0.001	93000	0.000 0.005 0.034 0.000 0.004 0.058 0.000 0.013 0.070 0.000 0.014 0.074 0.001 0.024		=====	0.100 0.200 0.330 0.100 0.230 0.330 0.100 0.315 0.475 0.125 0.315 0.470		0.273 D.NB4 D.434 0.666 B.461 D.744 0.520 B.709 B.804 0.553 B.724 B.818 D.NB5 B.475 B.782	0.175 0.445 0.775 0.555 0.775 0.856 0.411 0.784 0.475 0.455 0.814 0.886 0.738 0.815 0.929
00.00	0.642 0.818 0.646 0.807 0.878 0.837 0.682 0.825 0.630 0.803	0.557 0.738 0.557 0.738 0.550 0.747 0.553 0.747	0.113 0.13 0.171 0.170 0.182 0.187 0.187 0.588	0.29* 0.505 0.235 0.505 0.18* 0.372 0.20* 0.009 0.19* 0.509	0.079 0.209 0.089 0.232 0.080 0.232 0.080 0.224	0.001	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000	000000000000000000000000000000000000000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000	0.000 0.001 0.000 0.005 0.001 0.017 0.003 0.037	0.002 0.021 0.003 0.020 0.003 0.020 0.008 0.031	0.074 0.073	0.0% 0.132 0.1% 0.2% 0.1% 0.3% 0.1% 0.3%	0.22 0.314 0.22 0.394 0.24 0.434 0.347 0.434 0.347 0.573
TREQ. 50.00 1	1020.0 0.374 1020.0 0.353 1050.0 0.373 1060.0 0.354	9.252	26222	20.00	56666	90000	88888	000000	88808	38888		9999	99999	30000	00000	99999	98999	96000	99999	99999		22000	20000	00000	20000

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AVERAGED OVER 20cm-1	0.00 10.00 5.000 2.000 1.000																									
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ATMOSPHERE P r K	0.050 0.020 0.010	0.997 0.999 0.999 0.998 0.999 1.000 0.998 0.999 0.999 0.998 0.999 1.000	0.002 0.007 0.000 0			0.447 0.444 1.000 0.442 0.444 0.449 0.442 0.444 0.449																				
8	UPR.CM.) 0.500 0.200 0.100	0.412 0.412 0.445 0.455 0.455 0.455 0.455 0.455 0.455 0.455 0.455 0.455 0.455 0.455 0	*****			0.472 0.441 0.445 0.482 0.440 0.445 0.487 0.487 0.493																				
¥	3,000 2,000 1,000	0.445 0.455	200.00	0.012	0.0000	0.872 0.433 0.441 0.872 0.431 0.439 0.811 0.849 0.42 0.807 0.858 0.442																				
WATER VAPOR	FREG. 30,00 20,00 10,00 S.	5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.137 C.s.t 0.781 0.156 C.553 0.859 0.55 C.853 0.118 0.602 C.755 0.828 0.187 C.745 0.828	6.51 C.11 0.61	0.402 C.573 0.678 0.413 C.59C 0.664 0.324 C.644 0.743 0.363 C.724 0.803	0.342 6.735 0.423 0.347 6.713 0.405 0.421 6.402 0.710 0.426 6.406 0.714																				
	0.003 0.002 0.001	0.144 0.041 0.000 0.044 0.000 0	0.444 1.000 1.000 0.444 1.000 1.000 0.444 1.000 1.000 0.000 0.444 1.000 1.000	0.948 0.949 0.000 0.948 0.948 0.948 0.949 0.000	0.448 0.449 1.COO	0.404 0.404 0.404 0.404 0.404 0.404 0.405 0.405 0.404 0.405 0.405 0.404 0.405 0.405 0.404	0,407 0,404 0,404 0,407 0,404 0,404 0,407 0,404 0,404 0,407 0,404 0,404	0.493 2.448 0.494 0.492 0.494 0.494 0.492 0.494 0.494 0.495 0.494 0.494	0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444	0.445 0.442 0.440 0.445 0.444 0.444 0.445 0.444 0.444 0.445 0.444 0.445 0.446	0.49% 0.49% 0.49% 0.49% 0.49% 0.44% 0.49% 0.49% 1.000 0.49% 0.44% 1.000	0.414 1.600 1.000 0.414 1.500 1.000 0.414 1.700 1.000 0.414 0.414 1.000	90000	00000	900	86666		66666	000000	88888	99999	66668	88868	00000	800000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000
	0 050 0.020 0.010	0,192 0,141 0.494 0,182 0,144 0.497 0,182 0,144 0.497 0,182 0,142 0.497 0,182 0,143 0,144	0.001 0.004 0.008 0.001 0.004 0.008 0.002 0.004 0.008 0.007 0.009	200 0 200 0 100 0	0.474 0.441 0.445 0.413 0.441 0.445 0.413 0.444 0.445 0.443 0.444 0.445	0.444 0.484 0.444 0.444 0.484 0.444 0.447 0.484 0.484	0.175 0.480 0.481 0.487 0.482 0.481 0.487 0.482 0.481 0.402 0.482 0.483	0.450 0.847 0.445 0.424 0.364 0.485 0.474 0.449 0.445 0.474 0.449 0.445	0.457 0.485 0.482 0.457 0.485 0.482 0.455 0.427 0.488 0.485 0.382 0.483	7.0% 0.0% 0.0% 7.0% 0.0% 0.0% 7.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0.0% 0	0.900 0.900 0.903 0.902 0.900 0.903 0.902 0.903 0.903	0.485 0.494 0.927 0.412 0.445 0.494 0.412 0.441 0.494 0.446 0.744 0.497	0.444 0.448 0.444 0.447 0.447 0.444 0.442 0.445 0.444 0.441 0.446 0.444	0.415 0.717 0.403 0.414 0.417 0.703 0.415 0.417 0.403 0.415 0.417 0.444	0,492 D. 497 D. 499 J. 493 D. 498 D. 493 Z. 499 D. 498 C. 443 Z. 499 D. 498 C. 443	5,936 0,499 0,493 5,936 0,499 0,493 7,936 0,499 0,933	0.937 0.993 3.993 0.937 0.993 1.000 0.937 0.933 1.000 0.938 0.993 1.000	7,474 1,000 1,000 7,474 1,000 1,000 3,447 1,000 1,000 1,000 1,000 1,000 1,000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.400 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.940 1.460 1.000 1.960 1.400 1.600 1.960 1.400 1.600 1.900 1.400 1.600		0.44# 0.449 1.000 0.449 1.000 1.000 0.448 1.000 1.000 0.448 0.499 0.499
	U(FR,CM.) 0,500 0,200 0,100	0,401 0,412 0,917 0,010	20000	0.000	000000	0.000 0.000	0.424 0.914 0.427 0.918 0.407 0.911 0.712 0.811 0.114 0.701	0.590 0.704 0.412 0.951 0.421 0.951 0.421 0.954	0.410 0.41 0.414 0.414 0.414 0.414	777.000 744.000 745.00	0.672 0.938 0.902 0.938 0.902 0.944 0.940 0.944	0.745 0.431	0.000	0,925 0.944 0,979 0.944 0,941 0.931 0,942 0.986	0.477 0.488	0.442 0.441	0.34	0,111 0,114 0,146 0,146 0,146 0,146 0,146 0,144	0.314 0	1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.010 1.000	000011000000000000000000000000000000000	0.778 0.938	0.434 0.443 0.434 0.444 0.434 0.434 5.434 0.434	0.444 0.401 0.434 0.401 0.413 0.413 0.413 0.413
	5 000 2,000 1,000	0.423 0.745 0.835 0.517 0.424 0.884 0.517 0.747 0.884 0.51 0.771 0.884	2452	1672		54644	20000	33443		33333	0.194 0.185 0.704 0.371 0.535 0.486 0.395 0.517 0.101 0.515 0.634 0.795 0.516 0.103 0.608	22222		0.774 0.444 0.414 0.405 0.444 0.430 0.905 0.430 0.735 0.437 0.420 0.735 0.877 0.420	20000		0.874 0.931 0.954 0.845 0.931 0.957 0.865 0.934 0.939 0.913 0.534 0.973	33335	2222		0.44 0.44 0.44 0.41 0.44 0.44 0.45 0.48 0.44 0.44 0.44	22355		72434	0.454 0.481 0.490 0.917 0.481 0.481 0.900 0.454 0.476 0.889 0.457 0.471 0.815 0.447 0.477	66666
	PREQ. 50.00 20.00 10.00	\$5000 \$117 (a.) to 0.441 \$5000 \$221 (c.) to 0.451 \$5000 \$120 (c.) to 0.451 \$5000 \$120 (c.) to 0.451 \$5000 \$120 (c.) to 0.451 \$5000 \$120 (c.) to 0.451	6,301 (.474 0.559 6,244 (.422 0.514 6,141 (.307 0.412	7.54. 7.54.	100 (100 01) 100 (100 01) 100 (100 01)	200 (15 cm) 200 (1	1,000 1,000 0,000	200 COM 0250	100 100 100 100 100 100 100 100 100 100	2410 2411 2711 2711 2711 2711 2711 2711 2711	1010 1871 ABT	0.131 (.2% 0.387 0.187 0.	0.20s C.402 0.615 0.20s C.415 0.547 0.212 C.418 0.500 0.315 C.518 0.633	6.00 com 50.00 c	11.15 C.35 0.443 11.11 1.00 0.725 11.21 0.00 0.725 11.21 0.00 0.725	26 0 24 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.131 (/3) 0.824 0.134 (/3) 0.134 0.123 (/2) 0.134 0.125 (/10 0.144									

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	0.005 0.002 0.001	0.455 0.438 0.984 0.453 0.437 0.988 0.450 0.477 0.488 0.455 0.477 0.487 0.437 0.487 0.487	0.015 0.016	0.934 0.470 0.48	0.951 0.978 0.988 0.944 0.977 0.988 0.954 0.975 0.947 0.950 0.975 0.998	1	0.974 0.984 0.984 0.913 0.984 0.991 0.914 0.914 0.91 0.972 0.914 0.913	0.474 0.441 0.443 0.475 0.441 0.444 0.475 0.442 0.445 0.475 0.445 0.445	****	******	88888	1.000 1.006 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	88888	******	88888	88688	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	38888	10000	888	0.444 1,000 1,000 0.448 1,000 1,000 0.448 0.444 1,000 0.448 0.444 1,000	0.001 000 1.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1.000 1.000	0.000 0.000 0.000	0.998 0.999 1.000 0.992 0.999 0.999 0.992 0.999 0.999 0.998 0.999 0.999	0.448 0.444 1.000 0.444 0.444 1.000 0.447 0.444 0.444 0.448 0.444 0.444
	2.050 0 020 0.010	0.401 0.684 0.424 0.774 0.881 0.423 0.479 0.481 0.423 0.779 0.481 0.424 0.779 0.481 0.424	0.450 0.724 0.825 0.457 0.724 0.826 0.472 0.734 0.817 0.472 0.794 0.841	0.740 0.857 0.700 0.725 0.857	0.744 0.845 0.414 0.745 0.845 0.414 0.757 0.857 0.404 0.413 0.447 0.414	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.410 0.447 0.445 0.489 0.432 0.434 0.483 0.426 0.932 0.472 0.435 0.437	0.407 0.434 0.454 0.403 0.441 0.441 0.411 0.440 0.441 0.411 0.447 0.441	0.515 0.451 0.470 0.615 0.444 0.474 0.444 0.474 0.483 0.440 0.474 0.461	0.910 0.984 0.993 0.914 0.999 0.994 0.994 0.995 0.997 0.994 0.999 0.991	0.445 0.448 0.444 0.442 0.444 0.444 0.446 0.444 0.000 0.446 0.444 0.000	0.777 1.006 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	0.444 1.080 1.080 0.444 1.080 1.080 0.444 1.080 1.080 0.444 1.080 1.080	1.800 1.080 1.000 1.000 1.800 1.000 1.000 1.080 1.000 1.088 1.800 1.090 1.608 1.090 1.090	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000	0.444 1.000 1.000 0.444 1.000 1.000 0.449 0.444 1.000 0.448 0.444 1.000	0.447 0.449 0.444 0	0,447 0,444 1,800 0,417 0,444 1,800 0,417 0,444 1,800 0,417 0,444 1,800	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.41 0.41 0.44 0.40 0.41 0.44 0.40 0.41 0.44 0.40 0.41 0.44	0.44 0.44 0.41 0.44 0.44 0.41 0.44 0.44 0.44 0.44 0.44 0.44	0.410 6.484 8.482 0.453 0.414 8.484 0.454 0.414 0.443 0.463 0.484 0.491 0.463 0.463 0.491	0,924 0.995 0.994 0,924 0.998 0.994 0,949 0.993 0.973 0.998 0.994	0.784 0.719 0.714 0.714 0.719 0.714 0.715 0.710 0.714 0.715 0.717 0.714
	UPPR CAL) 0.500 0.200 0.100	0.402 0.714 0.402 0.715 0.427 0.727 0.548 0.705			0.53	0.705 0.854 0.710 0.855 0.770 0.855 0.780 0.855	0.770 0.641	0.749 0.851 6.80+ 0.841 0.427 6.840 0.802 0.859	0.824 0.878 0.841 0.903 0.877 0.915 0.884 0.921	0.855 0.914 0.414 0.855 0.914 0.414 0.409 0.451 0.471 0.417 0.498 0.474 0.451 0.498 0.474	0.477 0.442 0.441 0.441 0.441 0.441 0.442 0.442 0.442 0.444	0.440 b.444 b.448 0.444 6.446 6.444 0.447 6.444 6.444 0.448 0.444 1.046	0.992 0.994 0.998 0.991 0.994 0.998 0.994 0.998 0.999 0.993 0.997 0.999	0.775 0.798 0.779 0.795 0.798 0.994 0.797 0.799 0.999 0.797 0.799 0.799	0.446 0.444 1.000 0.446 0.444 1.000 0.446 0.444 1.000 0.448 0.444 1.000	0.99 0.999 1.000 0.993 0.997 0.998 0.993 0.947 0.998 0.993 0.947 0.998	0.442 0.441 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444	0.415 0.445 0.775 0.415 0.445 0.445 0.415 0.445 0.445 0.415 0.445 0.445 0.415 0.445	0.977 0.989 0.994 0.979 0.998 0.994 0.979 0.998 0.995 0.977 0.999 0.999	0.919 0.953 0.961 0.921 0.943 0.960 0.937 0.910 0.944 0.922 0.941 0.928	0.455 0.477 8.467 0.421 0.959 0.914 0.403 8.494 0.472 0.415 8.494 0.472	0.917 8.956 0.978 0.917 8.956 0.935 0.990 0.942 0.947 0.921 0.941 0.978 0.960 0.988 0.999			
7	: 20cm' :	20100 03	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.020 0.103 0.227 0.015 0.075 0.127 0.015 0.075 0.177 0.047 0.156 0.274 0.054 0.175 0.177	0.022 0.107 0.220 0.019 0.098 0.216 0.029 0.110 0.214 0.048 0.153 0.248	54555	0.224 0.444 0.597 0.224 0.417 0.553 0.214 0.402 0.542 0.225 0.422 0.544	7777	0.324 0.582 0.631 0.414 0.582 0.4% 0.483 0.440 0.734 0.492 0.642 0.734 0.491 0.441 0.735	0.405 0.734 0.404 0.415 0.734 0.412 0.404 0.405 0.403 0.707 0.414 0.473 0.746 0.478 0.473	0.813 0.890 0.931 0.875 0.931 0.939 0.901 0.949 0.931 0.815 0.937 0.984	0.914 0.917 0.181 0.914 0.987 0.997 0.916 0.988 0.994 0.918 0.999 0.994	0.452 0.477 0.484 0.451 0.474 0.485 0.448 0.483 0.495 0.462 0.496 0.468 0.465 0.481 0.488	0.470 0.484 0.491 0.481 0.492 0.493 0.481 0.490 0.494 0.484 0.492 0.494	0.985 0.993 0.494 0.488 0.993 0.994 0.488 0.993 0.997 0.489 0.493 0.997	0.454 0.472 0.484 0.454 0.472 0.487 0.451 0.474 0.487 0.451 0.474 0.484	0.949 0.673 0.985 0.933 0.965 0.989 0.933 0.943 0.971 0.903 0.943 0.971	0.412 0.434 0.414 0.442 0.439 0.415 0.482 0.432 0.438 0.881 0.431 0.434 0.842 0.537 0.441	0.777 2.940 0.974 0.889 0.934 0.740 0.880 0.942 0.844 0.886 0.996 0.990 0.746 0.862 0.913	0.651 0.185 0.043 0.682 0.001 0.870 0.741 0.842 0.898 0.707 0.818 0.878 0.755 0.044 0.882	0.822 0.894 0.930 0.709 0.816 0.878 0.641 0.783 0.852 0.705 0.832 0.871 0.742 0.838 0.889	0.449 0.811 0.875 0.429 0.811 0.872 0.623 0.734 0.832 0.712 0.817 0.877 0.825 0.898 0.935	0.554 0.740 0.824 0.557 0.678 0.754 0.543 0.684 0.782 0.575 0.705 0.784 0.544 0.484 0.784	0.417 0.194 0.645 0.462 6.734 0.811 0.469 0.779 0.245 0.462 0.769 0.831 0.777 0.865 0.409	0,74 0,852 0,891 0,070 0,120 0,120 0,120 0,120 0,120 0,100 0,100 0,110 0
	AVERAGED OVER		200 - 200 -			\$577 6575 6575 6	33333	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.016 C.092 0.027 C.015 0.026 C.015 0.026 C.027	0.144 C.155 0.141 C.141 0.711 C.170 0.711 C.170	0.34 C.027	123 C-25	7860.0 0.40) C.804 0.934 7870.0 0.808 C.807 0.934 7880.0 0.812 C.918 0.949 7960.0 0.823 C.912 0.945	7410.0 0.618 C.919 0.951 7720.0 0.602 C.410 0.955 7730.0 0.403 C.456 0.495 7790.0 0.412 C.458 0.474	0.90g C.93 6.91g C.93 0.515 C.94 0.99 6.94	0.642 0.612 0.613 0.748 0.748 0.748 0.748	0.152 C.822 0.152 C.833 0.155 C.833 0.155 C.833			8210.0 0.224 C.394 0.532 8220.0 0.284 C.441 0.530 8230.0 0.315 C.314 0.6440 8230.0 0.384 C.341 0.548	#260.0 0.444 C.645 0.749 #210.0 0.227 C.418 0.402 #240.0 0.226 C.418 0.544 #3760.0 0.326 C.421 0.544		9362.0 0.246 c.454 0.541 8370.0 0.178 c.335 0.451 8390.0 0.178 c.335 0.454 4400.0 0.145 c.336 0.424		25.555 25.555 25.555
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ATMOSPHERE PRESSURE	0 050 0.020 0.010	0,495 0,495 0,499	3.794 0.994 1.000 0.994 0.994 1.000 0.994 0.994 0.900 0.994 0.994 0.994 0.994 0.994 0.994 0.995 0.994 0.999	0.974 0.949 1.000 0.948 0.934 1.000 0.941 0.948 0.439 0.998 0.999 1.000	0.947 0.999 0.419 0.926 0.949 0.949 0.987 0.915 0.998 0.987 0.415 0.091	0.435 0.494 0.495 0.996 0.494 0.495 0.943 0.495 0.495 0.943 0.497 0.995	0.492 0.498 0.499 0.492 0.797 0.499 0.986 0.991 0.497 0.462 0.794 0.497	0.041 0.094 0.094 0.041 0.996 0.095 0.041 0.996 0.095 0.045 0.995 0.995	0.444 D.403 D.403 0.445 D.403 D.403 0.400 D.404 D.403 0.403 D.404 D.403 0.403 D.403 D.403	0.941 0.942 0.996 0.487 0.995 0.998 0.990 0.994 0.998 0.990 0.994 0.998	0.991 0.994 0.998 0.991 0.996 0.998 0.930 0.946 0.998 0.486 0.914 0.997	0.487 0.445 0.487 0.485 0.544 0.487 0.485 0.704 0.497 0.485 0.704 0.937 0.785 0.433 0.937	0.44.0.445 0.447 0.44.0.445 0.447 0.48.0.445 0.447 0.40.0.445 0.447	0.487 0.492 0.492 0.982 0.492 0.998 0.980 0.991 0.993 0.985 0.981 0.993	0.952 0.914 0.920 0.451 0.927 0.438 0.950 0.981 0.990 0.938 0.989 0.963 0.938 0.988 0.963	0.933 0.974 0.986 0.932 0.962 0.963 0.932 0.962 0.934 0.912 0.953 0.934 0.934 0.944	0.915 0.967 0.981 0.936 0.914 0.925 0.937 0.987 0.985 0.959 0.987 0.989	0.88 0.41 0.93 0.85 0.85 0.92 0.76 0.85 0.92 0.83 0.85 0.91	0.613 0.911 0.939 0.936 0.946 0.911 0.907 0.911 0.911 0.879 0.913 0.940	0.914 0.934 0.917 0.844 0.937 0.942 0.859 0.924 0.955 0.876 0.934 0.942	0.819 0.413 0.444 0.844 0.412 0.445 0.826 0.902 0.946 0.247 0.A87 0.932 0.815 0.401 0.433	0.801 0.815 0.921 0.740 0.816 0.921 0.738 0.870 0.918 0.719 0.830 0.890	0.80 0.41 0.41 0.70 0.41 0.61 0.61 0.71 0.61 0.71 0.62 0.86	0.730 0.839 0.845 0.620 0.782 0.860 0.628 0.789 0.860 0.707 0.874 0.886 0.593 0.744 0.831	0.507 0.416 0.719 0.416 0.514 0.709 0.316 0.514 0.400 0.316 0.409 0.471
6	UPR.CM.)	0.968 0.485 0.492 0.962 0.280 0.293 0.495 0.280 0.288 0.495 0.480 0.289 0.216 0.480 0.289	110-00 100-000-0	0.485 0.484 0.484 0.484 0.484 0.484 0.419 0.484 0.484 0.415 0.446 0.485 0.416 0.445	0.911 0.330 0.305 0.911 0.918 0.903 0.312 0.914 0.914 0.912 0.934 0.978	0.95 0.98 0.98 0.95 0.98 0.98 0.95 0.99 0.98 0.95 0.97 0.98	0.442 0.443 7.495 0.442 0.413 7.495 0.495 0.451 0.233 0.402 0.453 0.434 0.414 0.414 0.444	0.417 0.467 0.467 0.418 0.481 0.480 0.478 0.467 0.483 0.478 0.461 0.493	0.914 0.944 0.917 0.914 0.95 0.919 0.926 0.925 0.981 0.920 0.925 0.985 0.921 0.919 0.915	0.401 0.910 0.062 0.400 0.431 0.474 0.405 0.434 0.434 0.417 0.461 0.461	0.972 0.905 0.902 0.924 0.964 0.961 0.927 0.944 0.961 0.909 0.953 0.974	0.404 0.404 0.474 0.492 0.447 0.474 0.403 0.443 0.474 0.894 0.448 0.471	0.919 0.960 0.917 0.923 0.967 0.979 0.928 0.965 0.980 0.911 0.913 0.973	0.417 0.938 0.936 0.400 0.447 0.458 0.411 0.414 0.453 0.411 0.639 0.939 0.711 0.811 0.923	0.756 0.859 0.913 0.808 0.884 0.917 0.756 0.844 0.910 0.756 0.851 0.902	0.839 0.887 0.925 0.731 0.437 0.887 0.704 0.814 0.873 0.704 0.814 0.873	0.151 0.450 0.000 0.652 0.781 0.051 0.121 0.912 0.490 0.824 0.447 0.433	0.455 0.784 0.935 0.470 0.628 0.726 0.386 0.559 0.648 0.531 0.677 0.767 0.543 0.735 0.618	0.603 0.714 0.614 0.738 0.832 0.901 0.634 0.801 0.862 0.626 0.750 0.823	0.448 0.747 0.845 0.418 0.748 0.827 0.542 0.445 0.788 0.594 0.731 0.813 0.602 0.734 0.814	0.448 0.442 0.761 0.504 0.471 0.784 0.470 0.442 0.744 0.405 0.598 0.704 0.445 0.418 0.724	0.44 0.604 0.704 0.40 0.54 0.707 0.34 0.51 0.664 0.313 0.48 0.612 0.350 0.318 0.637	0.243 0.404 0.718 0.243 0.471 0.548 0.203 0.185 0.524 0.276 0.488 0.600	0.354 0.449 0.627 0.254 0.427 0.554 0.257 0.414 0.544 0.178 0.440 0.544	0.074 0.222 0.383 0.047 0.135 0.278 0.020 0.049 0.146 0.030 0.044 0.191 0.188 0.324 0.435
AT 0	5.000 2.000 1.000	0.415 0.415 0.447	0-012 (1-45) 0-171 0-11 0-101 0-175 0-11 0-101 0-175 0-101 0-101 0-101 0-175 0-101 0-101 0-175 0-101 0-101 0-175 0-101 0-101	0.407 0.332 0.473 0.416 0.336 0.471 0.771 0.436 0.404 0.771 0.436 0.404 3.471 0.437 0.402	0.850 0.135 0.451 0.854 0.125 0.950 0.75 0.75 0.750 0.70, 0.701 0.864	3.416 C.609 0.418 5.826 C.401 3.418 5.703 C.455 0.429 C.752 0.41 0.415	0.770 0.767 0.533 0.727 0.443 0.452 0.745 0.713 0.624 0.799 0.710 0.837 0.707 0.836 0.401	0.653 C.776 9.675 0.613 0.779 0.613 0.613 0.791 3.622 0.623 0.644 3.614 0.505 0.633 0.605	0.494 D.184 0.399 3.647 0.405 3.653 0.677 0.604 0.677 0.456 0.70 0.667	5.521 0.501 0.734 5.521 0.701 0.617 5.545 0.134 0.631 5.615 0.772 0.657	0.027 5.102 C.604 9.446 0.171 0.413 0.499 0.194 0.369 0.401 0.752 0.834 0.346 5.752 0.834	0.517 0.74) 0.844 0.545 0.745 0.854 0.624 0.764 0.844 0.621 0.754 0.834	0.613 D.191 D.166 0.613 D.804 D.874 0.619 D.814 D.867 0.619 D.190 D.861	0.61 0.92 0.910 0.61 0.172 0.817 0.55 0.116 0.810 0.424 0.60 0.120 0.150 0.140 0.120	0.34 0.54 0.664 0.34 0.611 0.721 0.74 0.612 0.721 0.74 0.55 0.645	0.424 0.410 0.723 0.734 0.437 0.423 0.278 5.444 0.598 0.283 0.444 0.595 6.395 0.444 0.595	0.162 0.537 0.644 0.225 0.197 0.533 0.326 0.501 0.625 0.472 0.645 0.746 0.478 0.620 0.734	0.00 0.115 0.517 0.00 0.215 0.310 0.013 0.114 0.257 0.123 0.276 0.106 0.131 0.313 0.131	0.145 0.117 0.178 0.324 0.225 0.455 0.101 0.472 0.592 0.224 0.184 0.513 0.173 0.314 0.445	0.201 0.310 0.313 0.178 0.131 0.444 0.136 0.282 0.411 0.198 0.151 0.413	0.041 0.221 0.134 0.045 0.224 0.147 0.043 0.190 0.123 0.024 0.131 0.234 0.044 0.170 0.303	0.042 0.184 0.310 0.035 0.112 0.246 0.031 0.114 0.258 0.025 0.042 0.190	0.021 0.134 0.287 0.023 0.031 0.043 0.031 0.031 0.045 0.034 0.037 0.148	0.000 0.004 0.171 0.000 0.034 0.134 0.000 0.035 0.134 0.000 0.034 0.143	0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.001
WATEŔ VAPOR	30 00 20:00 10 00	11111 11	100 100 100 100 100 100 100 100 100 100			75456									35335	2000	9.02 C.124 9.02 C.124 9.03 C.124	56666		0.001 C.010 0.014 0.001 C.014 0.014 0.001 C.016 0.039 0.001 C.016 0.030		000000000000000000000000000000000000000	0.000 0.000	200000000000000000000000000000000000000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
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ATMOSPHERE PRESSURE 3° K #1001	0.050 0 020 0 010 0.996 0.999 0.999 0.991 0.999 0.999	000-1 000-1 000-0 000-1 000-1 000-0 000-1 000-1 000-0 000-1 000-1 000-0 000-1 000-1 000-0	0.994 0.999 0.994 0.994 0.999 0.994 0.994 0.999 0.994 0.994 0.994 0.994 0.994 0.994 0.994	0.99 0.999 0.998 0.999 0.998 0.999 0.998 0.999 0.998 1.005 1.905	0.999 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 0.000 1.000 1.000	0.999 1.000 1.000 0.999 0.999 1.000 0.999 1.000 1.000 0.999 0.999 1.000	0.999 1.000 1.000 0.999 1.000 0.999 1.000 1.000 0.999 0.999 1.000	0001 056 0 066 0 966 0 066 0 066 0 966 0 066 0 066 0	0.994 1.000 1.000 0.994 1.000 1.000 0.995 0.998 0.998 0.998 0.998 0.998	0,096 0,008 0,009 0,404 0,008 0,004 0,004 0,009 0,004 0,004 0,009 0,004	0.994 0.999 0.999 0.994 0.997 0.999 0.995 0.997 0.999 0.991 0.998 0.998	0.012 0.001 0.005 0.017 0.008 0.003 0.019 0.008 0.003 0.010 0.010 0.001	0.465 0.470 0.487 0.455 0.473 0.482 0.457 0.476 0.483 0.477 0.467 0.491	0.465 0.979 0.987 0.914 0.949 0.987 0.872 0.924 0.950 0.409 0.944 0.983	0.426 0.455 0.484 0.415 0.947 0.745 0.474 0.957 0.971 0.441 0.415 0.944 0.624 0.403 0.930	0.811 D.884 D.923 G.877 D.893 D.929 G.667 G.916 D.914 D.921 G.934 C.916 D.975 G.897 G.992	0.95 0.91 0.92 0.95 0.94 0.97 0.95 0.94 0.92 0.95 0.93 0.92	0.616 0.923 0.923 0.822 0.888 0.923 0.653 0.904 0.933 0.905 0.907 0.931 0.865 0.929 0.955		33337	22222	0.415 0.445 0.461 0.422 0.463 0.421 0.465 0.401	0.80 0.978 0.918 0.788 0.796 0.850 0.488 0.796 0.850 0.471 0.881 0.850
20 =30(0 500 0.200 0 100 0.975 0.947 0.995 0.960 0.990 0.995		0.988 0.993 0.495 0.998 0.997 0.998 0.998 0.997 0.998 0.998 0.997 0.999	000100000000000000000000000000000000000	0.005 0.007 0.009 0.008 0.009 0.009 0.008 0.009 0.009 0.009 0.009 0.009 0.009	0.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000 0.000 0.000 1.000	0.997 0.999 0.999 0.997 0.999 0.999 0.998 0.499 0.999 0.408 0.499 0.999		0.000											0.529 0.657 0.754 0.529 0.667 0.754 0.709 0.726 0.797 0.710 0.810 0.465 0.659 0.773 0.437	0.494 0.794 0.857 0.637 0.453 0.820 0.554 0.492 0.774 0.545 0.754 0.754 0.624 0.755 0.825	0.447 0.749 0.855 0.448 0.805 0.865 0.724 0.825 0.877 0.448 0.784 0.847 0.540 0.729 0.805	0.623 0.756 0.828 0.635 0.747 0.837 0.634 0.766 0.637 0.684 0.776 0.635	0.565 0.71% 0.798 0.517 0.673 0.760 0.46% 7.651 0.732 0.16% 0.545 0.753	0.462 0.627 0.227 0.257 0.537 0.557 0.229 0.421 0.557 0.229 0.431 0.557
Ψ	5 000 2,000 1,000 5.4% 6,919 6,960 6,911 6,949 6,948	0.02 t 0.05 t 0.					0.080 0.080 0.071 0.080 0.081 0.080 0.085 0.085			6.747 0.866 C.018 0.770 0.851 0.903 0.710 0.851 0.903 0.914 0.958 0.977															0.051 0.185 0.327 0.005 0.035 0.187 0.005 0.038 0.187 0.007 0.033 0.107
ATER V	50 00 20,00 10 00 1.555 0.718 0.857 0.556 0.772 0.859	0.426 0.430 0.382 0.466 0.433 0.303 0.482 0.433 0.413 0.703 0.81 0.421 0.703 0.81 0.421	0.773 0.84 0.423 0.773 0.98 0.423 0.777 0.98 0.957 0.778 0.40 0.457	0.767 C.030 C.071 0.767 C.012 C.051 0.774 O.00 G.042 0.779 O.00 G.042	0.651 0.457 0.947 0.651 0.457 0.978	0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655 0.655	0.654 0.911 0.484 0.664 0.618 0.914 0.785 0.911 0.950 0.785 0.915 0.955 0.777 0.978 0.975	0.761 6.887 0.497 0.701 6.941 0.897 0.701 6.872 0.821 0.402 6.833 6.893 0.710 0.812 6.899	0.654 0.651 0.004 0.054 0.601 0.940 0.714 0.650 0.903 0.514 0.612 0.403 0.555 0.432 0.433	0.15¢ C.5s¢ 0.46¢ 0.265 q.451 0.517 0.434 d.593 0.690 0.434 d.593 0.690 0.452 f.191 0.844	0.430 0.704 0.889 0.558 0.718 0.883 0.420 0.407 0.708	0.151 6.055 0.755 0.102 0.010 0.755 0.102 0.010 0.755 0.115 0.015 0.755	0.179 0.074 0.779 0.421 0.420 0.735 0.399 0.604 0.723 0.334 0.345 0.694 0.275 0.400 0.430	0.235 0.476 0.517 0.229 0.439 0.577 0.722 0.436 0.587 0.171 0.304 0.512	0.000 0.500 0.550 0.000 0.200 0.010 0.100 0.000 0.507	0.13+ 0.3+ 0.45 0.03+ 0.12+ 0.25 0.012 0.05+ 0.13 0.05/7 0.169 0.28/	0-027 0-137 0-230 0-027 0-124 0-251 0-024 0-145 0-246 0-006 0-065 0-144	0.000 0.000 0.021 0.000 0.000 0.000 0.000 0.000 0.000	0.001 0.100 0.100 0.001 0.100 0.100 0.001 0.000 0.100 0.010 0.000 0.100	0.001 0.056 0.136 0.001 0.014 0.050 0.004 0.050 0.134 0.005 0.056 0.120	0.000 0.014 0.055 0.001 0.014 0.057 0.000 0.017 0.055 0.000 0.017 0.055	0.001 0.021 0.081 0.002 0.035 0.110 0.002 0.025 0.115 0.000 0.007 0.001	0.000 0.007 0.017 0.000 0.000 0.051 0.000 0.009 0.051		
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J(PR.CM	0.500 0.200 0.100 0.005 0.006 0.000 0.005 0.006 0.000		0.083 C.483 C.483 C.487 C.483 C.484 C.483 C.484 C.484 C.483 C.484 C.484	11111	0.929 0.940 0.473 0.901 0.913 0.95 0.914 0.915 0.972 0.910 0.915 0.972	1111	*****	20000	2000	42226	10000	0.234 0.151 0.234 0.234 0.173 0.286 0.234 0.454 0.255 0.415 0.416 0.751	0.350 0.189 0.275 0.354 0.155 0.354 0.055 0.181	0.071 0.160 0.104 0.223 0.078 0.189 0.078 0.189	5.252 0.167 6.340 0.502 6.221 0.517 6.221 0.517	5.234 5.342 5.175 5.342 5.255 5.345 5.255 5.327	45555	\$4.00°	0.252	20 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.749 0.837 2.755 0.823 2.617 0.823 2.617 0.823	1200 1000 1000 1000 1000 1000 1000 1000	00000	6.659 0.919 0.944 0.916 0.949 0.948 0.929 0.919 0.973 0.918 0.953 0.975	
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20cm

OVER

AVERAGED

AVERAGED OVER 20cm ⁻¹	(1119. 30.00 20.00 10.00 5.000 2.000 0.500 0.500 0.000 0.050 0.050 0.010 0.005 0.005 0.005																				
WATER VAPOR AT 0.20 ATMOSPHERE PRESSURE T=300°K	PMEQ. 50,00 30.00 10 00 5,000 2,000 1,000 0,500 0,300 0,100 0,030 0,030 0,010 0,000 0,000 0,001	0.540 C.544 C.731 C.545 D.547 D.735 D.741 C.745	CATALOGY CATA			0.15 6.27 6.27 6.27 6.27 6.27 6.27 6.27 6.27															
	FREG. 59,00 70,00 10,00 5,000 2,000 1,000 0,500 0,500 0,100 0,030 0,030 0,030 0,030 0,003 0,003 0,003 0,000 1	2.455 G-416 G-715 G-191	0.4% 0.4% 0.7% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4% 0.4	3.55 6.00 5.31 C.57 6.37 6.36 6.46 6.46 5.47 6.37 6.48 6.49 6.49 6.49 6.49 6.49 6.49 6.49 6.49	CAST CAST CAST CAST CAST CAST CAST CAST	0.223 0.410 0.533 0.424 0.434 0.435 0.441 0.440	CAN CAMP CAN	CARL CARE CARE CARE CARE CARE CARE CARE CARE	ELIN CALL CALL CALL CALL CALL CALL CALL CAL	CALL CALL CALL CALL CALL CALL CALL CALL	CARL CARE CALL CALL CALL CALL CALL CALL CALL CAL	CALL CAST CAST CAST CAST CAST CAST CAST CAST	CASA CASA CASA CASA CASA CASA CASA CASA		100 CH 10	6.15 CAN	8871 08771 0	1001 1001 1001 1001 1001 1001 1001 100	2011 COLD COLD COLD COLD COLD COLD COLD COLD	2.516 CASTO	

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1770 - 1771 - 17

ATMOSPHERE PRESSURE	=300° K
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		0.005 0.002	0,973 0,985 0,971 0,986 0,972 0,986 0,970 0,988	0.937 0.932 0.932 0.932 0.933 0.933	0.441 0.471		0.945	0.987 0.983 0.988 0.983 0.985 0.982 0.989 0.994	0.987 0.993	0.985 0.491 0.985 0.492 0.989 0.395 0.986 0.395	0.445 0.446 0.445 0.446 0.945 0.447 0.995 0.997		90000	80000	1,000 1	1,000	0001	1,000 1	1,000 1	1.000 1	1.000 1.000	0.044 1.000		0000		0.991 0.999	166.0 166.0 166.0 166.0 166.0 166.0
		0.050 0 520 0.010	0.899 0.939 0.938 0.686 0.939 0.937 0.900 0.939 0.939 0.892 0.914 0.959 0.892 0.939 0.959	0.814 0.922 0.447 0.844 0.402 0.932 0.794 0.649 0.402 0.720 0.859 0.897 0.778 0.858 0.901	0.829 0.893 0.426 0.838 0.886 0.930 0.896 0.816 0.914 0.815 0.882 0.917	0.876 0.924 0.449 0.854 0.409 0.938 0.863 0.928 0.931 0.899 0.939 0.959 0.874 0.423 0.444	0.673 0.922 0.948 0.673 0.923 0.943 0.670 0.923 0.943 0.681 0.927 0.953 0.913 0.944 0.953	0.944 0.416 0.940 0.952 0.971 0.981 0.944 0.989 0.940 0.989 0.940 0.915 0.989	25453	0.979	10000	11111	0.494 0.494 0.494 0.498 0.494 0.494 0.498 0.494 1.000 0.98 0.494 1.000	88888	88888	60000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	88888	00000	0.998 0.998 1.000 0.997 0.999 0.999 0.997 0.999 0.999 0.991 0.999 0.999	*****	0.941 0.994 0.398 0.991 0.994 0.998 0.993 0.996 0.998 0.991 0.996 0.998	*****	0.984 0.994 0.998 0.986 0.995 0.998 0.986 0.995 0.998 0.996 0.998 0.998	00000	0.469 0.494 0.483 0.482 0.490 0.495 0.479 0.484 0.495 0.462 0.495 0.495	0.440 0.444 0.441 0.48 0.494 0.495 0.482 0.491 0.495 0.488 0.494 0.494
			0.680 0.793 0.854 0.678 0.799 0.855 0.691 0.799 0.856 0.650 0.789 0.856 0.659 0.777 0.845	2145	0.622	12267	22225	90000		0.831 0.894 0.934 0.442 0.401 0.431 0.852 0.407 0.943 0.464 0.414 0.945	0.867 0.916 0.941 0.891 0.932 0.452 0.902 0.939 0.959 0.902 0.940 0.959 0.900 0.938 0.958	0.413 0.458 0.911 0.932 0.954 0.971 0.951 0.911 0.481 0.955 0.973 0.983 0.911 0.984 0.990	0.913 0.984 0.992 0.983 0.994 0.993 0.984 0.994 0.994 0.984 0.993 0.994 0.985 0.993 0.994	0.442 D.444 D.444 D.447 D.444 D.444 D.447 D.444 D.444 D.447 D.444 D.444	0.995 0.997 0.998 0.996 0.998 0.999 0.995 0.998 0.999 0.995 0.998 0.999	0.915 0.998 0.999 0.998 0.998 0.999 0.998 0.999 1.000 0.988 0.999 0.499	0.49% 0.99% 1.000 0.49% 1.000 1.000 0.49% 1.000 1.000 0.49% 1.000 1.000	0.445 0.444 0.448 0.445 0.447 0.448 0.494 0.497 0.448 0.494 0.447 0.448	0.994 0.994 0.994 0.992 0.994 0.994 0.991 0.994 0.998 0.988 0.994 0.998	0.945 0.045 0.945 0.945 0.995 0.995 0.044 0.992 0.995 0.544 0.991 0.995	0.930 0.493 0.493 0.985 0.442 0.495 0.986 0.993 0.996 0.985 0.492 0.493 0.986 0.482 0.493	0.445 0.471 0.983 0.450 0.472 0.483 9.441 0.474 0.487 0.955 0.474 0.984	0.475 0.984 0.941 0.945 0.974 0.984 0.946 0.949 0.982 0.944 0.973 0.982	0.4% 0.478 0.488 0.4% 0.473 0.483 0.4% 0.4% 0.4% 0.4% 0.4% 0.4%	0.930 0.931 0.931 0.902 0.931 0.958 0.904 0.951 0.959 0.912 0.949 0.965 0.912 0.945 0.963	0.952 0.452 0.462 0.952 0.953 0.453 0.952 0.453 0.962 0.954 0.954 0.954 0.954 0.965 0.965 0.965 0.965	0.962 0.176 0.005 0.956 0.974 0.003 0.932 0.957 0.972 0.055 0.959 0.092
•	20cm ⁻¹	5.000 2.000 1.000	35333	2223	0.091 0.242 0.381 0.109 0.746 0.405 0.004 0.217 0.318 0.114 0.251 0.333 0.194 0.389 0.501	22552	0.198 0.172 0.505 0.189 0.385 0.501 0.199 0.368 0.499 0.256 0.417 0.541 0.375 0.538 0.645	20000	55555	0.673 0.763 0.698 0.760 0.737 0.610 0.759 0.791	0.240 0.613 0.764 0.645 0.603 0.662 0.807 0.662	0.44a 0.40a 0.44a 0.42a 0.64a 0.42a 0.93a 0.932	0.440 0.473	0.411 0.445	20.50 20.50	00.00 00		0.594 0.594 0.594 0.596 0.506 0.506 0	0.514 0.940 0.914 0	2000	0.977 0.485 0.965 0.977 0.948 0.979 0.944 0.478 0.923 0.948	0.410 0.418 0.915 0.425 0.915 0.542 0.920 0.544	0.444 0.442 0.403 0.434 0.403 0.434 0.403 0.434	0.420 0.445 0.020 0.432 0.874 0.412 0.905 0.934 0.445 0.461	0.82 0.80 0.83 0.81 0.83 0.81 0.82 0.81	90.00	0.869 0.919 0.445 0.232 0.908 0.936 0.779 0.854 0.908 0.795 0.803 0.903
	AVERAGED ONER	FREQ. 50 00 20,00 10 00	0.001	0.001 6.02	0000 0000 0000 0000 0000 0000 0000 0000 0000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.002 0.003	0.113 C.273 0.093 C.283 0.084 C.281	0.138 C.204 0.000 C.204 0.000 C.204 0.000 C.204	2011	0.172 0.133 0.133 0.130 0.130 0.130 0.130	200 0 250 0.00 0 250 0	0.702 C.805 0.774 C.855 0.775 C.855 0.777 C.855	0.413 6.434 0.434 0.434 0.434 0.434		0.45 C.45 0.42 C.45 0.43 C.45 0.43 C.45 0.43 C.45	0.41 0.47 0.41 0.47 0.41 0.47 0.41 0.47 0.41 0.47	0.00	0.635 C.438 0.631 C.922 0.638 C.922 0.638 C.922	0.000	0.462 C.416 0.409 C.24C 0.410 C.865 0.787 C.865	\$2000	0.705 C.812 0.534 C.716 0.531 C.676 0.536 C.713	0.514 C.74 0.514 C.704 0.475 C.612 0.582 C.713	0.425 0.555	0.521 C.673 0.445 C.603 0.530 C.663 0.530 C.665	6468.0 0.608 C.7C 0.813 470.0 0.82 C.1R 0.77 440.0 0.43 C.10 0.83 640.0 0.479 C.623 0.715 850.0 0.594 0.723 0.793
ESSURE	. ◀	0 003 0 003 0.001	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 0.999 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	0.949 1.000 1.000 0.949 1.000 1.000 0.999 1.000 1.000 0.979 1.000 1.000	1.000 1.000 1.000 0.999 1.000 1.000 0.999 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 0.999 1.000 1.000 0.999 1.000 1.000 0.989 1.000 1.000	0.999 1.000 1.000 0.999 1.000 1.000 0.999 1.000 1.000 0.999 1.000 1.000	0.998 1.000 1.000 0.998 1.000 1.000 0.999 0.999 1.000 0.999 1.000 1.000	0.999 1.000 1.000 0.999 1.003 1.000 0.999 1.000 1.000 0.999 1.000 1.000 0.999 1.000 1.000	0.44# 1.000 1.000 0.49# 1.000 1.000 0.49# 1.000 1.000 0.49# 1.000 1.000 0.49# 0.49# 0.49#	0.998 0.999 0.999 0.984 0.949 1.000 0.998 1.000 1.000 0.999 1.000 1.000	0.999 1.000 1.000 0.999 1.000 1.000 0.999 1.000 1.000 0.999 0.999 1.000	0.949 1.000 1.000 0.944 0.739 1.000 0.996 0.999 1.000 0.998 0.999 1.000	0.999 0.999 1.000 0.999 0.999 1.000 0.999 0.999 1.000 0.998 0.999 1.000	0.404 1.000 1.000 0.448 0.449 1.000 0.448 0.449 1.000 0.496 0.498 0.494	0.994, 0.498 0.988 0.495, 0.498 0.494 0.495, 0.498 0.494 0.495, 0.498 0.497, 0.498	0.404 0.401 0.400 0.401 0.404 0.408 0.401 0.404 0.408 0.981 0.408 0.401 0.401 0.408 0.401	0.992 0.994 0.948 0.943 0.995 0.993 0.995 0.998 0.999 0.996 0.998 0.999	0.941 0.441 0.445 0.972 0.945 0.941 0.945 0.980 0.917 0.988 0.995 0.944 0.942 0.995	0.083 0.005 0.002 0.000 0.008 0.000 0.000 0.000 0.003 0.000 0.009	0.484 0.445 0.445 0.485 0.442 0.445 0.982 0.491 0.445 0.984 0.492 0.494 0.485 0.482 0.495	0.479 0.490 0.444 0.446 0.490 0.495 0.471 0.986 0.493 0.473 0.986 0.492	0-972 0-985 0-991 0-976 0-98- 0-990 0-986 0-981 0-990 0-985 0-977 0-986 0-981 0-779 0-986	1446	10000	24477
איחבאב ייא		0.050 0 020 0 00.0	0.998 0.993 0.998 0.999 0.998 0.999 0.998 0.999	0.949 0.994 0.944 0.994 0.944 1.000 0.944 1.000	0.445 0.438 0.498 0.498 0.498 0.499	0.444 1.600 0.447 0.444 0.441 0.444 0.044 1.000	0,479 0,090	00.444	0.44 0.44 0.44 0.44 0.44 0.44		0.444 0.447	0.002 0.002 0.003	0.736 0.006	00.000	0.946 0.948	0.00	0.442 0.445 0.445 0.445 0.746 0.447 0.474 0.467	0.945 0.990 0.978 0.975 0.985	0.474 0.481 0.481 0.484 0.484 0.484	0.461 0.97	0.460 0.480	0.472 0.442 0.452 0.450 0.450 0.450 0.450	0.940 0.940	0.034 0.034	2652	0.851 0.909 0.939 C.466 0.686 0.921 0.827 0.886 0.423 0.836 0.899 0.932 0.772 0.856 0.901	0.724 0.822 0.878 0.850 0.778 0.840 0.800 0.774 0.840 0.734 0.724 0.724 0.739 0.827 0.878
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	N 005=	0 300 0.	60000		00000	*****		20000		*****	*****	0.922 0.924 0.944 0.944 0.944 0.949 0		0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40		0.451 0	*****	2000	******	0.755 0.462 0.655 0.740 0.724 0.918 0.774 0.818	20000	0.021 0.890 0.925 0.747 0.854 0.905 0.774 0.834 0.883 0.776 0.855 0.898	20000	£2224	0.518 0.648 0.849 0.518 0.648 0.781 0.488 0.445 0.745 0.502 0.704 0.705 0.501 0.724 0.805	25355	0,333 0,502 0,674 0,249 0,432 0,559 0,119 0,349 0,434 0,180 0,344 0,434 0,409 0,534 0,633
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WAIEK VAP		PREG. 50 00 20,00 10 00		4.45. C.40.	2,511 C.65 2,511 C.65 2,613 C.65	0.123 C.12				500 CO		35333	33333	33333		33333			20117	23853	12722			100.0 0.414 (.073 0.184 100.0 0.611 (.041 0.134 100.0 0.602 (.024 0.138 100.0 0.602 (.026 0.611	90000	10-8 0.000 0.012 0.03 10-8 0.000 0.010 0.04 10-0 0.000 0.010 0.04 10-0 0.000 0.000 0.000	110.0 0.000 0.000 0.001 1.0.0 0.000 0.000 0.001 1.0.0 0.000 0.000 0.001 1.0.0 0.000 0.000 0.001 1.0.0 0.000 0.000
		-	22322	32327	*****		22222	33333	23333		11111	*****	22223	*****	11111	*****	22222		*****	13115							
		0002 0007 2:004	0.045 6.948 8.909 0.944 1.000 1.000 0.949 1.000 1.000 0.947 0.949 0.909		2000	*****	0.446 0.494 1.000 0.446 0.444 1.000 0.446 0.444 1.000 0.446 0.444 1.000		0.000		0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05	0.332 0.455	0.41 0.45	0.2140	0.413 0.44	0.942 0.953	0.423 0.432 0.423 0.432 0.442 0.448 0.472 0.448	0.456 0.478	0.414 0.982	0.00	0001 0001 6660	0.142 1.000 1.000 0.412 1.000 1.000 0.912 1.000 1.000 0.917 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000
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	40		0.915 0.913 0.940 0.915 0.915 0.990 0.915 0.905 0.905 0.915 0.915 0.919	0.421 0.918 0.385 0.402 0.41 0.80 0.407 0.415 0.416 0.914 0.400 0.421	0.91* 0.41* 0.41 0.947 0.41 0.41 0.44 0.42 0.41 0.44 0.44 0.47	0.345 0.314 0.385 0.346 0.449 0.980 0.348 0.445 0.946 0.348 0.346 0.446		1111	22.00	21611	22000		0.11 0.60 0.711 0.42 0.612 0.711 0.42 0.71 0.82	22.22	25000	12111	0.341 0.704 0.754 0.340 0.341 0.674 0.341 0.643 0.774 0.747 0.840 0.841 0.701 0.809 0.844	25225	24000	0.061 0.013 0.010 0.011 0.024 0.051 0.011 0.027 0.012 0.001 0.039 0.040 0.020 0.032 0.040	*****		0.411 0.445 0.445 0.410 0.445 0.493 0.410 0.445 0.993 0.410 0.745 0.993	0.409 0.404 0.407 0.407 0.404 0.407 0.404 0.404 0.408 0.404 0.404 0.409		0,993 0,994 0,959 0,995 0,994 0,978 0,972 0,914 0,998 0,972 0,994 0,998	0,449 0,914 0,947 0,449 0,492 0,948 0,481 0,492 0,495 0,481 0,492 0,495
		3,000 2,000 1,000	0.110 0.014 0.017 0.011 0.017 0.014 0.011 0.017 0.014 0.012 0.017 0.010 0.011 0.010 0.011	0.274 0.412 0.414 0.724 0.414 0.614 0.701 0.401 0.605 0.791 0.405 0.405	0.64 0.43 0.650 0.62 0.42 0.450 0.62 0.42 0.450 0.62 0.450 0.62 0.450	0.442 0.403 0.435 0.419 0.444 0.421 0.410 0.461 0.421 0.825 0.481 0.424 0.610 0.481 0.424	0.42.0 0.40.0 0.42.0 0.	0.118 C.816 0.027 0.718 C.816 0.027 0.702 0.001 0.816 0.452 0.772 0.834 0.415 0.343 0.824	0.419 0.117 0.824 0.419 0.131 0.824 0.526 0.631 0.720 0.526 0.631 0.730	0.3% 0.5% 0.6% 0.3% 0.4% 0.5% 0.2% 0.4% 0.5% 0.2% 0.4% 0.5%	0.121 0.210 0.412 0.121 0.211 0.413 0.112 0.211 0.403 0.121 0.210 0.428	0.051 0.152 0.354 0.070 0.204 0.352 0.051 0.191 0.352 0.051 0.174 0.302 0.051 0.204 0.335	0.041 0.181 0.292 0.093 0.111 6.191 0.221 0.404 0.518 0.231 0.494 0.537	0.001 0.234 0.334 0.017 0.645 0.314 0.001 0.311 0.535 0.002 0.626	0.027 0.118 0.031 0.144 0.034 0.174 0.034 0.283		0.114 0.305 0.056 0.314 0.186 0.337 0.300 0.503 0.300 0.503	0.176 0.338 0.238 0.138 0.238 0.504 0.238 0.504	0.315 C.542 0.350 0.050 0.350 0.050 0.351 0.083		0.845 0.903 0.434 0.903 0.433 0.948 0.903 0.943 0.944 0.802 0.438 0.958	0.85 0.422 0.54 0.85 0.458 0.455 0.877 0.426 0.451 0.895 0.437 0.455 0.907 0.443 0.942	0.923 0.654 0.949 0.915 0.950 0.949 0.915 0.950 0.949 0.915 0.457 0.957	0.943 0.949 0.941 0.941 0.943 0.915 0.915 0.945 0.945 0.945 0.945 0.945	0,941 0,980 0,987 0,987 0,987 0,987 0,986 0,996 0,996 0,996 0,996 0,996 0,998	0.914 0.485 0.494 0.914 0.494 0.494 0.495 0.491 0.485 0.481 0.481 0.481 0.481 0.481	0.914 0.183 0.182 0.915 0.415 0.183 0.918 0.193 0.113 0.923 0.457 0.475
		PREG. 50.00 20.00 10 00	2000	6.33 6.33 6.33 6.33 6.33 6.33 6.33 6.33		2000	0.152 C.613 0.103 C.553 0.104 C.553 0.104 C.552			53533	10000	6.65 6.65 6.65 6.65 6.65 6.65 6.65 6.65	36899	2007	35888	30075		50156	3222	13333		*****			*****		

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	0 005 0 002 0.001	0.949 0.969 0.979 0.938 0.958 0.958 0.918 0.955 0.988 0.927 0.955 0.988	0.694 0.934 0.954 0.694 0.934 0.954 0.694 0.938 0.954 0.654 0.938 0.933	0.862 0.926 0.913 0.652 0.950 0.93 0.652 0.950 0.93 0.653 0.950 0.850 0.954 0.950	0.850 0.905 0.936 0.865 0.914 0.926 0.861 0.839 0.926 0.816 0.885 0.916 0.614 0.684 0.918	0.607 0.679 0.914 0.789 0.654 0.899 0.635 0.756 0.899 0.431 0.567 0.696 0.443 0.584 0.676	0.707 0.784 0.835 0.926 0.938 0.973 0.932 0.959 0.972 0.932 0.959 0.972	0.91c 0.9v4 0.965 0.8% 0.921 0.9v5 6.8% 0.900 0.93v 0.8% 0.900 0.93v	0.000	0.450 0.950 0.955 0.900 0.911 0.959 0.914 0.948 0.947 0.916 0.917 0.963 0.926 0.933 0.963	127.00		000'1 000'1 000'1 000'1 000'1 666'0 000'1 000'1 666'0 666'0 066'0 266'0	99999	44888	86666	88888	99999	88888	88888	50000	0.999 0.999 1.000 0.998 0.998 0.998 0.998 0.999 0.999 0.997 0.999 0.999	0.995 0.999 0.999 0.992 0.999 0.050 0.992 0.999 0.999 0.993 0.999 0.999	0.994 0.994 0.994 0.994 0.997 0.994 0.993 0.997 0.994 0.995 0.998 0.994	0,907 0,000 0,000 1,000 1,000 1,000 0,999 1,000 1,000 0,997 0,099 0,999	0.000 1.000 1.000 0.000 1.000 1.000 0.000 0.000 0.000 0.000 0.000 0.000
	0.050 0.020 0.010	0.8% 0.928 0.8% 0.928 0.8% 0.8% 0.8% 0.8% 0.8% 0.6%	0.850 0.850 0.775 0.800	0.756 0.433 0.754 0.431 0.770 0.795 0.770 0.631 0.771 0.835	0.71 0.70 0.70 0.70 0.70 0.74 0.00 0.70	0.510 0.731 0.570 0.650 0.374 0.520 0.344 0.520 0.240 0.538	0.572 0.641 6.859 0.882 0.850 0.900 0.837 0.901	0.827 0.822 0.72 0.72 0.097 0.779 0.091 0.779	0.084 0.773 0.030 0.707 0.035 0.779 0.705 0.775 0.777 0.017	0.426 0.456 0.427 0.477 0.437 0.462 0.633 0.493	0.466 0.919 0.462 0.940 0.420 0.940 0.920 0.940	0.955 0.989 0.976 0.976 0.975 0.947 0.975 0.947		0.000 1.000	1,000	1,000 1,000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1,000	00000	20000	986'0 266'0 566'0 866'0 266'0 566'0 866'0 866'0 566'0 866'0 866'0 766'0	0.992 0.998 0.998 0.990 0.998 0.998 0.990 0.998 0.998 0.988 0.998 0.998	200000	0.00 c	0,444 0,494 0,494 0,494 0,994 0,494 0,497 0,989 0,449 0,485 0,081 0,994 0,786 0,781 0,494	0,995 D,998 C,999 0,993 C,998 C,998 0,998 C,998 C,998 C,988 C,998 C,986 C,998
	8	0.050	20000	0.520	0.152		0.563	0.527	95.55	0.00		00.000	0.078 0.078 0.091	*****	200000	80000	000000	000000	00000	*****	0.003	0.000	0.040	0.00		0.0000
	* biPR.CM.] 0.500 0.700 0	0.526 0.678 0.53 0.631 0.400 0.546 0.400 0.578	0.277 0.153 0.277 0.153 0.277 0.152 0.181 0.314	0.236 0.412 0.290 0.336 0.191 0.335 0.270 0.444	0.151 0.180 0.180 0.150 0.251 0.705 0.251	0.081 0.21 0.081 0.055 0.001 0.055	0.109 0.247 0.254 0.456 0.353 0.555 0.310 0.555 0.310 0.515	0.30 0.447 0.130 0.377 0.130 0.273 0.115 0.273	0.100 0.201 0.111 0.212 0.112 0.277 0.200 0.378	0.277 0.557 0.554 0.509 0.556 0.557 0.556 0.551	0.537 0.077 0.539 0.720 0.653 0.746 0.653 0.746	0.785 0.759 0.886 0.701 0.705 0.718 0.796 0.915	0.94.3 0.96.5 0.94.1 0.96.5 0.94.1 0.946 0.945 0.995	0.981 0.981 0.981 0.983 0.991 0.993 0.991 0.991	0.000 0.000	0.999 1.000 0.999 1.000 0.999 1.000 0.999 1.000	0001	0001	0.000 1.000	0.095 0.097 0.097 0.095 0.095 0.095 0.095 0.095	0.041 0.002 0.041 0.090 0.091 0.048 0.019 0.081	0.973 0.934 0.986 0.979 0.986 0.979 0.981 0.976	0.071 0.062	0.015 D.085 0.016 O.055 0.010 O.055 0.010 O.055	0.000	0.082 0.085 0.076 0.085 0.057 0.075 0.057 0.075
ΞE	2.000 1.000	252 0.393 199 0.322 122 0.237 187 0.788 186 0.704	051 0.156 053 0.182 055 0.089	0.043 0.121 0.054 6.098 0.054 0.002 0.054 0.185	0.011 0.053 0.077 0.061 0.016 0.064 0.010 0.052		0.010 0.0%2 0.016 0.120 0.012 0.194 0.095 0.224	0.067 0.167 0.076 0.089 0.01% 0.057 0.007 0.059	0.004 0.036 0.004 0.034 0.012 0.001 0.015 0.001	0.057 0.155 0.116 0.213 0.11 0.229 0.117 0.259	0.340 0.115 0.340 0.175 0.364 0.305 0.21 0.355	0.598 0.101 0.048 0.780 0.751 0.810 0.701 0.489	0.578 0.917 0.577 0.973 0.978 0.955 0.978 0.965	955 0.975 472 0.984 973 0.990 986 0.993	944 0.994 943 0.997 993 0.997	0.40. 0.498 0.40. 0.498 0.40. 0.998 0.40. 0.999	000000 00000 00000 00000 00000	0.949 1.000	200'0 Sea'0 Rea'0 Sea'0 Rea'0 Sea'0	0.990 0.945 0.484 0.992 0.984 0.991 0.982 0.988	0.972 0.981 0.984 0.972 0.984 0.972 0.984 0.972	0.911 0.92	0.41 0.959	445 0.063 472 0.840 551 0.83 682 0.88	975 0.093 975 0.093 975 0.093	951 0.975
R: 20cm ⁻¹			0.000	6.000	62.00	900000	0.000	00000	0.000	90.00	0.12 0.13 0.24 0.25	35555	0.100 0.101 0.401 0.400	55.55	0.000	00000	00000	1334	0.000	20000	2000	0.80 0.80 0.80 0.80 0.80 0.80 0.80	92000	2222	25.00	20000
OVER	20.00 10 00	0.0000	00000	00 0.000 0.000 00 0.000 0.000 00 0.000 0.000 00 0.000 0.000	00000	99999	90000	96669	99999	900000	10000	32525	22222	2445	20000	25.00	22223	24 0.901 0.981 01 0.167 0.961 05 0.901 6.900 05 0.910 0.910	200.00	11 0.447 C.789 10 0.919 0.765 11 0.275 0.755 11 0.215 0.975	2420	24 0.415 0.611 17 0.774 0.641 24 0.775 0.641 24 0.757 0.878	25 0.411 0.462 25 0.417 0.467 25 0.445 0.467	0.00 0.13 0.10 0.10 0.10 0.10 0.10 0.10	200000	25 0.455 0.4
AVERAGED	FREQ. 50.00							3626.0 0.000 3626.0 0.000 3630.0 0.000 3640.0 0.000	3870.0 0.000 5980.0 0.000 5980.0 0.000 3490.0 0.000	35000 0000 35000 0000 35000 0000	1970.0 0.000 1970.0 0.000 1980.0 0.000 1990.0 0.004	1020.0 0.050 1020.0 0.050 1050.0 0.101 1050.0 0.134	00000 0.302 0070.0 0.352 0070.0 0.352 0000.0 0.521	200000000000000000000000000000000000000	*170.0 0.777 *170.0 0.777 *170.0 0.784 *170.0 0.784	\$220.0 0.624 \$220.0 0.634 \$250.0 0.631 \$250.0 0.651	1270.0 0.857 1270.0 0.872 1270.0 0.882 1270.0 0.882		*356.3 0.908 *340.0 0.909 *370.0 0.903			\$3000 0.000 \$3000 0.000 \$3000 0.000 \$3000 0.530	\$500.0 0.725 \$500.0 0.725 \$500.0 0.735	\$650.0 0.670 \$650.0 0.470 \$650.0 0.448 \$650.0 0.448		4710.0 0.716 4720.0 0.735 4730.0 0.735 4730.0 0.670 4750.0 0.520
AVE																										
	0.005 0,002 0,001	86888	88888	86668	88888	30000	88888	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	66666	1.000 1.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000 1.000 1.000 1.000	83388	88888	50000	10000	0.000	22222	2444	25555	0.992 0.996 0.997 0.982 0.992 0.997 0.985 0.992 0.992 0.992 0.992	20000	0.99	0.985 0.990 0.995 0.985 0.991 0.995 0.985 0.492 0.998 0.985 0.498 0.998	0.981 0.929 0.931 0.983 0.990 0.993 0.984 0.990 0.993 0.982 0.998 0.993	26222	0.000
	0.020 0.010				000 1 000 000 1 000 000 1 000 000 1 000				0001 0001	0000	0.996 0.999 0.935 0.998 0.997 0.998 0.997 1.000 0.999 1.000	000000	*****						13555	22222	53455	20000	20000	0.962 0.972 0.962 0.974 0.962 0.974 0.963 0.974 0.963 0.973	20000	912 0,935 685 0,936 685 0,936 782 0,918
	0,050	90000	2000	20000	00000	30000	86666	99996	00000	30000	9999	20000	*****		00000			0.95 0.97 0.45 0.97 0.42 0.97 0.92 0.95	20000	0,000		20000	20000	20000	00000	00000 00000 00000
7=300° K	UPPECA.) 0.500 0.200 0,100	0,484 0,421 0,999 0,987 0,995 0,998 0,988 0,998 0,998 0,998 0,998	0,003 0,046 0,008 0,003 0,004 0,008 0,003 0,004 0,008 0,003 0,004 0,000	0,402 0,425 0,991 0,992 0,993 0,993 0,992 0,993 0,993 0,993 0,993	00000	20000	0.494 1.000 1.000 1.000 1.000 1.000 0.994 1.000 0.994 1.000 0.994 0.994	2222	*****	0.094 0.336 0.997 6.992 0.994 0.994 6.992 0.996 0.998 6.991 0.386 0.998 6.986 6.993 0.998	0.040 0.042 6.043 6.043 0.470 0.043 6.040 0.047 0.946 6.040 0.495 0.007	0.000 0.001 0.001 0.001 0.445 0.001 0.014 0.058 0.003 0.000 0.047 0.070 0.012 0.045 0.002	6.97. 6.937 6.993 6.97. 6.947 6.993 6.97. 6.987 6.993 6.97. 6.987 6.993	C.978 0.948 D.993 D.974 O.948 D.993 D.972 O.945 D.991 D.959 O.945 D.978 D.959 O.975 D.978	0.95e 0.97e 0.981 0.95e 0.97e 0.980 0.95g 0.977 0.941 0.95g 0.95e 0.975	0.431 0.435 0.475 0.419 0.405 0.405 0.403 0.472 0.466 0.403 0.472 0.481 0.406 0.477 0.481	30100	0.471 0.921 0.945 0.462 0.911 0.937 0.478 0.423 0.945 0.798 0.405 0.488	0.192 0.142 0.856 0.764 0.850 0.883 0.764 0.850 0.883 0.764 0.015 0.883	22.000	0.742 0.465 0.465 0.714 0.410 0.463 0.767 0.414 0.437 0.415 0.419 0.423 0.410 0.475 0.412	D. 278 D. 849 D. 972 D. 787 D. 850 G. 908 O. 735 D. 874 D. 874 G. 787 D. 814 D. 898 D. 194 D. 888 D. 908	0.60% 0.41% 0.92% 0.653 0.41% 0.92% 0.650 0.90% 0.93% 0.71% 0.28% 0.91% 0.70% 0.65% 0.89%	0.705 0.410 0.910 0.705 0.410 0.910 0.705 0.410 0.910 0.705 0.910 0.910	3,754 9.041 0.867 3,721 0.413 0.671 2,685 0.793 0.851 9,658 0.751 0.820	0.574 0.746 0.846 0.539 0.179 0.804 0.515 0.651 0.754 0.502 0.619 0.755
Щ	000 1.000	0.000	20000			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2022		20000						6,442 6,506 6,936 6,812 6,895 6,931 6,802 3,875 6,912 6,785 6,814							0.552 0.715 0.552 0.015 0.552 0.000 0.552 0.000	2222	33333	0.578	25.55
	5.000 2.0		30000				0.435 0.448 C.037 C.098 C.038 0.448 C.038 0.448								20000	2000									3333	0 2 0 0 0
	20.00 10.00	0.176 0.316 0.176 0.216 0.176 0.257 0.176 0.257			22775	C. 244 C. 284 C. 244 C. 284 C. 244 C. 284 C. 244 C. 284			A. 35 C. 25			5.47 4.9.4 6.40.5 4.494 6.70.5 6.434 6.70.5 6.434	6.150 C.150 C.150 C.150 C.150 C.150 C.150 C.150	6.75 C.979 6.75 C.979 6.75 C.975	2012 1.75 2012 1.75 2012 1.75 2012 1.75	0.354 0.341 0.043 0.355 0.354 0.055 0.360 0.547 0.062 0.344 0.647 0.784	0.403 C.704 0.375 C.334 0.375 C.334	0.00 0	0.017 0.018 0.186 0.019 0.286 0.103 0.655 0.104 7.283 0.210 0.317 0.517	C. 154 D. 647 C. 748 C. 154 D. 531 C. 531 C. 154 D. 531 D. 657 F. 234 D. 539 D. 657	0-105 0-255 0-554 0-653 0-117 6-221 0-663 0-128 0-145 0-110 0-242 0-145	0.745 C.VIN 0.745 C.VIN 0.146 0.735 0.166 0.735	6.75 6.15 6.75 6.15 6.75 6.15 6.75 6.25 6.75 6.25	0.139 0.274 0.130 0.274 0.130 0.274	0.195 0.726 0.054 0.171 0.053 0.056 0.056 0.170	0.024 0.157 0.025 0.040 0.005 0.037 0.007 0.914
	\$0.00	9.45	4444											13333			52622 21933	5.0 0.214 0.455 5.0 0.205 0.451 5.0 0.104 0.231 5.0 0.104 0.231	36636 29333	3555 53333		-2600	20000		20020	0.000
	FREO	2222	18313	2222	11111	2,122	35333	33333	2022.2	22222	22222	2222	244	2222	2000	2447	52525	50021 40021		22527	22222	2240.0 2240.0 2240.0 2200.0 200.0	000000	22222	25000	21200 21200 21200 21000 21000 21000 21000
	0.002 0.001	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	200 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1,000 1	1.000 1.000 0.900 1.000 1.000 1.000 1.000 1.000	0.000 1.000 0.000 1.000 0.000 1.000 0.000 1.000	200000000000000000000000000000000000000	5,000 5,000	0.270 0.460 0.071 C.040 0.071 C.040 0.071 C.047	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.000	2000 C. 000 C. 0	0.023 0.015	240 0 00 00 00 00 00 00 00 00 00 00 00 00	0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90	0.814 0.814 0.913 0.901 0.918 0.918 0.978 0.918 0.948 0.954 0.924 0.948	22 0.24 22 0.24 22 0.24 23 0.44	0.030 0.930 0.970 0.031 0.957 0.971 0.030 0.957 0.970 0.310 0.953 0.975	25 0.010 25 0.010 25 0.010 25 0.010	100000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.00 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.012 0.005	200000	00000000000000000000000000000000000000	2000
	0 900	93333				******	20000	20000		22.22	2000			20000							2262	00000	*****	******	0.995 0.998 0.978 0.949 0.788 0.949 0.784 0.949	2000
	0.020 0 010	2001	88888	0.999 0.999					0.424 C.932 0.931 0.932 0.833 0.933				25675		10000	1000			1000	3242	0.00	25000	20000	*****	20000	0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
	100 0.030	2007-1						33777	25.72	3333	15513			56333					30030	20303		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0		2000	40000	85 00 00 00 00 00 00 00 00 00 00 00 00 00
	UPP.CM) 0,500 0,200 0.1	0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041 0.041	22,50	*****	66466	20222		20.00	5.000 7.702 1.027 5.00 7.00 0.773 5.00 7.70 0.773 5.00 7.00 7.70 5.00 7.00 7.70 5.00 7.00 7.70		5.55 7.55 5.55 5.55 7.55 5.55 5.55 7.55 5.55 5.55 7.55 5.55 5.55 7.55 5.55	35555	55193		35555	6.00 0.270 0.00 0.270 0.00 0.070 0.00 0.070 0.00 0.070	11111		25252	35555	40000	0.000	22440	0.910 D.945 0.965 0.905 0.918 0.95 0.406 7.937 0.95 0.402 0.952 0.955 0.900 0.957 9.955	2000	0.950 0.464 0.9 0.922 0.978 0.9 0.470 0.981 0.9 0.481 0.985 0.6
	2.000 1.000	2.931 2.994 5.936 2.994 5.904 2.994 5.904 2.994 5.904 2.994	3,945 3,995 3,995 6,995 6,995 6,995 6,995 6,995 6,995	2007 C-001	0.000 0.000	2001 1000 0000 0000 0000 0000 0000 0000	5.75 5.25 5.75 5.25 5.75 5.25 5.75 5.25 5.76 5.25	0.041 0.726 2.555 1.001 2.557 1.001 2.547 2.003	2000 STATE	32339 22438	1000 C. 1111	1000 1000 1000 1000 1000 1000 1000 100	224 0.00 254 0.00 254 0.155 256 0.156 256 0.156	10000 10000	97C19 01014 01014 01302 01014 01302 01014 01302	2.010 0.010 0.121 0.010 0.100 0.100 0.000 0.100		1,17 (-30 1,197 (-32) 1,107 (-42) 1,107 (-43)		55 C.58	2.572 2.573 2.573 2.577 2.577 2.575	42555 2255 2255	1222	0.831 0.472 0.832 4.490 0.809 0.441 0.793 0.481	20000	12 0.052 12 0.052 13 0.052 14 0.052
	5.000	10000	11000		2000	55555	3533	34315		97353	35355	33555	35.55	11111	36553	3555		3333	33555	98223	33333	11335		31715	33336	6.447 0.427 0.437 0.427 0.437 0.427 0.437 0.427
	20 00 10.00				0.454 0.007 0.474 0.007 0.475 0.007 0.475 0.007	255	33445	24466 21116	100 CO	200 COM	300000	1,03c 9,00c 1,03c 9,00c 1,00c 9,00c 9,00c 1,00c 9,00c	2.00 C.000 2.000 C.000 2.000 C.000 2.000 C.000 2.000 C.000		1000000 1000000 1000000000000000000000		1000		2.01. 5.05. 2.02. 3.06. 2.03. 5.06. 0.00. 0.127		27.5 7.75 27.5 7.75 27.5 7.75 27.5 7.75 27.5 7.75 27.7	\$50,000 \$10,00	200 CO	25.0 0.05. 25.0 0.05. 25.0 0.05. 25.0 0.05.	0.5/7 C.54 C.72 C.52 C.72 C.73 C.72 C.73	1.755 0.783 1.773 0.857 1.839 0.877 1.839 0.877
	8			12223	22322		3353			115.	4444	34.55	118/10	13253				# 33 93	12331				37.53	12242		
	FAEG.	55555	2000 2000 2000 2000 2000 2000 2000 200	25225	22222	25225	22222	55575	1350.0	11111	11111	32222	37.57.5	2222	35.45	22222	22223	2222	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	22225	20000	22222	2000	12224	2222	22222

WATER VAPOR AT 0.05 ATMOSPHERE PRESSURE

SVETE EFFER FEFEE EFFEE EEREE EREES EEREE EEREE EEREE EREES EEREE EEREE EEREE EREES EREES EREES EREES EREES EREES EREES EREES EREES

AVERAGED OVER 20cm ⁻¹	20.00 10.00																										
	0.005 0.002 0.001	1,000 1	1.000 1.000 1.000 1.000 0.999 1.000 0.999 1.000		1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000															,						
	0.050 0.020 0.010	0.499 0.999 0.999 0.999 0.999 1.000 0.999 0.999 1.000 0.949 0.999 0.999	0.999 1.000 0.997 0.733 0.995 0.993 0.994 0.993	0.994 0.994 0.994 0.994 0.999 0.999 0.998 0.999	0.435 0.436 0.436 0.436 0.436 0.436 0.436 0.436 0.436																						
T=300°K	U(PR.CM.)	0.491 0.445 0.997 0.492 0.495 0.995 0.492 0.495 0.997 0.989 0.494 0.996	0.992 0.594 0.986 0.995 0.976 0.485 0.976 0.987	0.475	0.934 0.927 0.923 0.923 0.930 0.933 0.930 0.933	0.010 0.001 0.000 0.010 0.001 0.000 0.010 0.001 0.000																					
	5.000 2,000 1.000	0.96e 0.980 0.989 0.96e 0.981 0.987 0.96e 0.981 0.987 0.46E 0.918 0.984 0.495 0.972 0.481	####	0.017 0.448 0.864 0.418 0.848 0.964 0.408 0.982 0.486 0.405 0.480 0.487	*****	0.965 0.476 0.486 0.495 0.476 0.666 0.498 0.462 0.475 0.497 0.462 0.475																					
	FREC: \$0.00 20.00 10.00	#350.0 C.#40.C.511 0.451 #370.0 C.#44.C.51.0.455 #370.0 C.#44.C.411 0.455 #370.0 C.#41.C.411 0.451 #400.0 C.#41 C.411 0.451		3335		190.3 191 10 1910																					
•	0.603 € 003 0.001	0.444 0.444 1.400 0.444 0.444 1.600 0.444 1.600 1.600 0.444 1.600 1.600 0.444 1.600 1.600	88888	0.441 1.400 1.000 0.441 1.000 1.000 0.441 0.441 1.000 0.441 0.441 1.000				*****				0.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000	88888	88883		6656	1,002 1,30 1,000 1,	900	90000	93398	88888	86666	88868	00000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	90000	
	0.050 0.020 0.010	0.981 0.995 0.998 0.952 0.998 0.998 0.954 0.998 0.998 0.995 0.998	*****		######################################	******	3,466 G.433 G.434 3,432 B.493 G.434 3,432 B.40 B.403 5,432 G.432 8,430 G.438 G.472	*****	*****		*****	5.041 5.046 6.047 5.041 5.046 6.047 6.049 6.009 6.009 6.040 6.009 6.009	*****	*****		*****	0071 85670 8667 10071 85670 8667 10071 86670 8667	20000	88238	965599	63666	88888	88888	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	20225	0.419 0.419 1.000 0.419 1.000 1.000 0.419 1.000 1.000 0.418 0.444 0.444	
	U(PR.CM) 0.500 0.200 0.100	0.485 0.424 0.448 0.486 0.481 0.481 0.487 0.481 0.489 0.411 0.481 0.489 0.415 0.481	*****				1490 0.010 0.440 0.441 7.442 0.402 0.422 0.442 0.444 0.443 0.444	0.745 0.484 0.495 0.945 0.414 0.415 0.945 0.444 0.474 0.947 0.948 0.474	0.44 0.44 0.46 0.44 0.44 0.47 0.44 0.44 0.41 0.44 0.41 0.41	0.431 0.454 0.472 0.435 0.461 0.473 0.435 0.442 0.473 0.428 0.454 0.470	0.437 0.402 0.474 0.434 0.446 0.472 0.435 0.446 0.473 0.435 0.473 0.482	0.951 0.971 0.951 0.954 0.975 0.985 0.957 0.975 0.985 0.958 0.975 0.985	0.410 0.482 0.442 0.410 0.482 0.940 0.412 0.484 0.990 0.417 0.498 0.992	0.981 0.988 C.993 0.984 0.991 C.934 0.987 7.992 C.993 0.984 0.998 C.993 3.981 C.948 0.992	0.981 2.983 0.991 0.981 0.991 0.991 0.981 0.991 0.991 0.988 0.991 0.991		5,430 0,445 5,444 5,430 0,445 6,444 0,441 0,494 0,444 0,441 0,494 0,444			86688	88888	600000			0.994 C.994 C.994 0.992 C.994 C.994 0.791 D.994 C.971 0.795 D.795 C.997 0.991 C.995 C.997		
	5.000 2.000 1.000	0.656 2.628 0.450 2.452 0.453 6.453 3.422 0.450 5.484 0.663 6.426 3.944 0.665 0.416 0.440	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	24699	3,440 5,000 3,400 3,464 7,400 0,400 3,402 5,400 6,744 6,447 0,404 5,445 2,440 0,404	144.10	3.602 4.476 9.424 5.602 4.476 9.415 6.735 2.473 9.440 6.434 6.154 9.623 5.447 9.615 6.739	000000000000000000000000000000000000000	0.85 0.85 0.81 0.81 0.81 0.81 0.81 0.81	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	200 00 00 00 00 00 00 00 00 00 00 00 00	\$200 \$200 \$200 \$	0.71	0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45	2000 2000 2000 2000 2000 2000 2000 200	64666	3.9% 0.4% 0.4% 5.9% 0.4% 0.4% 9.4% 0.4% 0.4%	****	*****	3,949 0,437 0,416 3,494 0,437 0,496 5,494 0,484 0,498 0,494 0,494 0,494	0,494 0,448 0,499 0,493 C,598 0,498 0,492 0,548 0,498 0,492 0,548 0,498	*****	0.991 0.445 0.497 0.592 0.494 0.494 0.586 0.493 0.494 0.684 0.494 0.494	0.144 0.447 0.493 0.144 0.447 0.493 0.944 0.937 0.193 0.944 0.982 0.193 0.482 0.493	0.461 0.489 0.444 0.463 0.418 0.466 0.458 0.475 0.464 0.451 0.475 0.484	31133	
	FAEG. 50 00 20.00 10.00	2,142 C.748 0.814 2,142 C.484 0.814 5,142 C.484 0.814 5,444 C.714 0.812	0.08# 0.78# 0.95# 0.703 0.802 0.86# 0.703 0.802 0.857 0.88# 0.795 0.85# 0.805 0.735 0.80#	2010 1-11 20 0 10 10 10 10 10 10 10 10 10 10 10 10	1,552	14.00 C.04+ 0.730 0.480 C.44+ 0.741 1.77 C.42+ 0.720 0.533 c.474 0.781	0.447 C.444 0.744 0.448441 0.714 0.227 0.175 0.521 0.111 0.233 0.747	0.134 C.242 0.333 0.731 C.443 0.204 0.442 C.413 0.211 0.424 C.413 0.214	0.511 (.450 0.711 0.511 (.450 0.744 3.428 (.554 0.647 0.480 (.651 0.744 0.487 (.628 0.774	0.444 C.622 0.734 0.464 C.622 0.723 0.454 C.522 0.723 0.434 C.534 0.878 0.431 C.534 0.878	0.414 C.024 0.122 0.419 C.020 G.721 0.464 C.020 D.713 0.514 C.123 D.749 0.594 C.123 D.749	2.541 93 0.734 2.381 2.713 0.794 2.522 2.70, 2.421 6.532 2.094 0.774 0.403 2.728 0.401	0.231 C.824 0.877 C.474 C.734 0.847 C.735 C.435 0.835 C.735 C.435 0.881	0.731 C.842 0.750 0.423 C.883 0.423 0.423 C.883 0.423 0.724 C.883 0.423	0.483 C.484 0.484 C.484	0.647 (.945 0.935 0.647 (.945 0.935 0.646 (.941 0.947 0.646 (.941 0.947	0.481 2.177 0.55. 0.471 0.424 0.438 0.401 0.444 0.561 0.401 0.704 0.561	2.412 C.414 0.472 2.412 C.494 0.472 0.414 1.741 0.471 1.451 1.491 0.471	5.43 C.421 0.480 C.445 C.444 C.444 L.545 C.474 C.644 L.546 C.474 C.644 D.565 C.974 O.465	6.979 C.946 0.932 C.557 C.948 0.931 C.555 C.912 0.935 C.586 C.991 0.935 U.584 C.991 0.935	0.141 6.906 0.494 6.584 6.901 0.935 0.544 6.901 0.935	0.414 C.941 0.442 0.474 C.946 0.542 0.474 C.943 0.490 0.474 C.444 0.491 0.467 C.466 0.481	0.145 C.175 0.544 0.450 C.142 0.948 0.457 C.075 0.442 0.119 C.075 0.493	C.W. 0.97. C.W. 0.95. C.W. 0.95. C.W. 0.97.	0,635 C. 938 0,472 0,616 C. 422 0,455 0,616 C. 912 0,415 0,659 E. 914 0,414 0,834 E. 924 0,914	0.45 C.44C 0.45 0.414 C.441 0.665 0.485 C.403 0.414 0.457 C.405 0.414	

WATER VAPOR 0.05 ATMOSPHERE PRESSURE

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	56.0	0.0986 0.0973 0.0973 0.0973 0.0973 0.0973	33413	33333	75122	30400	*****	£3553 56555		*****	00.000	1,000	888888	88888	0000000	90001	8865	200011	00001	988888	000000	1,000 1,000 1,000 1,000 1,000 1,000	****	\$000 \$000 \$110 6110 6110 6110 6110 6110	8888
	0.005 0.002	0.956 0.979 0.956 0.973 0.955 0.973 0.955 0.975 0.955 0.956 0.956 0.956 0.956 0.956	0.921 0.951 0.918 0.949 0.900 0.937 0.919 0.946	0.900 0.938 0.900 0.932 0.692 0.932 0.675 0.921	0.868 0.917 0.742 0.901 0.745 0.903 0.570 0.708 0.580 0.708	0.781 0.844 0.954 0.972 0.955 0.972 0.954 0.972 0.959 0.972	0.945 0.944 0.946 0.946 0.90 0.938 0.90 0.940	0.693 0.933 0.690 0.931 0.990 0.934 0.913 0.946	0,933 0.954	0.410 0	0.991 0.991 0.991 0.991 0.991 0.991	0.997 0.999 0.998 1.000 0.999 1.000 1.000 1.000	00000	22222	0001	00000		9337	96666	000111				0.987 0.988 1.000 1.000 1.000 1.000 0.987 0.998	0.04
	50 0.020 0 010	56 0.910 0.931 51 0.910 0.931 51 0.910 0.932 52 0.930 0.932 53 0.930 0.931 53 0.930 0.930 53 0.930 0.930 53 0.930 0.930 53 0.930 0.930 54 0.930 0.930 55 0.930 0.930 56 0.930 0.930 57 0.930 0.930 57 0.930 0.930	5555	12225	23 0.746 0.815 60 0.499 0.789 88 0.549 0.654 94 0.343 0.485 45 0.369 0.475	0.99	0.00	0.683 0.793 0.650 0.677 0.784 0.846 0.690 0.794 0.854 0.772 0.802 0.857 0.772 0.830 0.878	90.00	25.55	2000	1656	******	99999	88888	86666	200 1.000 1.000 200 1.000 1.000 200 1.000 1.000 200 1.000 1.000	88888	2000		90000	0.000	0.455 0.401 0.404 0.462 0.469 0.403 0.415 0.405 0.400 0.484 0.491 0.494 0.488 0.443 0.494	0.492 0.493 0.499 0.492 0.494 0.499 0.492 0.494 0.499 0.490 0.494 0.494	0.481 0.918 0.494 0.484 0.484 0.484 0.481 0.484 0.494 0.481 0.494 0.998 0.984 0.999 0.993
	CM.)	1 0.442 9.884 9.0401 9.	24.000	0.533	0 0.508 0.623 11 0.434 0.560 44 0.264 0.388 9 0.101 0.145	0.745	0 0.552 0.623 0 0.660 0.749 11 0.610 0.738 7 0.569 0.633 2 0.580 0.686	0.576 0.598 0.598	2222	44444	11325	****	*****	20000	20000	80000	88888	8888			;;;;;		54445	*****	20000
	UPR.CM.)	0.500	0.352	25.00	0.211 0,350	0.552		22.2						0.942 0.944											0.488 0.443 0.484 0.442 0.485 0.482 0.485 0.482
ا- ال	20Cm	0.239	0.013 0.134 0.275 0.031 0.128 0.246 0.030 0.119 0.227 0.051 0.181 0.310	.027 0.111 0.22 .027 0.111 0.22 .010 0.093 0.19 .010 0.054 0.13	.001 0.015 0.038 .002 0.015 0.038 .000 0.000 0.000 .000 0.000 0.002	.009 0.059 0.11 .039 0.158 0.30 .071 0.242 0.40 .094 0.272 0.424	0.054 0.204 0.349 0.024 0.118 0.237 0.014 0.039 0.187 0.014 0.079 0.171 0.007 0.057 0.145	.006 0.054 0.14 .004 0.059 0.14 .009 0.062 0.15 .018 0.082 0.17	,056 0.181 0.37 (113 0.282 0.39 (114 0.282 0.39 (146 0.295 0.48	1,280 0.451 0.51 1,334 0.512 0.62 1,304 0.540 0.65 1,418 0.578 0.678	1,593 0,725 0,79 1,691 0,796 0,63 1,723 0,823 0,67 1,713 0,659 0,90 1,618 0,486 0,42	181 0.922 0.93 192 0.927 0.93 192 0.93 0.93 194 0.95 0.97	1955 0.973 0.98 1.956 0.973 0.98 1.966 0.962 0.98 1.975 0.487 0.99	0.965 0.902 0.995 0.988 0.995 0.997 0.989 0.995 0.997 0.989 0.995 0.995	1,991 0,997 0,998 1,992 0,996 0,998 1,991 0,996 0,998 1,994 0,998 0,998	00'0 \$00'0 \$00'0 00'0 \$00'0 \$00'0 00'0 \$00'0 \$00'0	. 996 0.498 1.30 . 996 0.999 1.30 . 996 0.999 1.00 . 998 0.499 0.99	1.992 0.998 0.99 1.998 0.974 0.99 1.998 0.99 0.99 1.992 0.995 0.99	1,482 0.443 0.44 1,483 0.441 0.44 1,483 0.441 0.44 1,447 0.486 0.49	1,971 D. 942 O. 98 1,954 G. 974 G. 98 1,954 G. 971 G. 98 1,954 G. 971 G. 98 1,955 G. 977 G. 98	1, 922 0.944 0.94 1, 928 C. 955 0.94 1, 928 0.955 0.95 1, 917 0.948 0.95 1, 920 0.949 0.95	0.942 0.962 0.97 0.947 0.942 0.97 0.939 0.942 0.97 0.951 0.949 0.97	1111	20000	0.456 0.474 0.486 0.454 0.494 0.496 0.952 0.421 0.496 0.854 0.403 0.496 0.854 0.403 0.496
	, E	201600 000000 201600 000000	90000	22222	86666	0.0000	20000	90.000	****	38888	34644	92488	20101	55555	29938	32655	*****	22222	######################################	51666	#####	98953	2442	15511	22212
	AVEKAGEU #E9, 50,00 %	1510.0 0.000.0	33333	38888	98838	30000	88888	33333	20.0 0.000	2000	20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0	200 0.32 90.0 0.32 90.0 0.42 90.0 0.42 90.0 0.42	20.00	20.0 0.492 0.722 0	20.0	20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0	20.0 0.00	0.00	20.00 0.414 0	00.0 0.434 0 0.00 0 0.00 0 0 0.00 0 0 0.00 0 0 0.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20.0 0.411 6 20.0 0.475 0 20.0 0.475 0 20.0 0.475 0	0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00	10.0 0.007 0 20.0 0.393 0 30.0 0.598 0 30.0 0.588 0	65.0 0.102 0 20.0 0.402 0 30.0 0.402 0	10.0 0.462 0 20.0 0.462 0 10.0 0.767 0 150.0 0.462 0
	¥— *								<u></u>																
1	005 0.002 0.00I	00000000000000000000000000000000000000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	20000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	999 1.000 1.000 999 1.000 1.000 999 1.000 1.000 999 1.000 1.000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	000 1.000 1.000 000 1.000 1.000 000 1.000 1.000 000 1.000 1.000	0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.40% 0.00% 0.00% 0.00%	86.0 866.0 866.0 867.0 187.0 786.0	946 0.448 0.449 941 0.445 0.449 941 0.422 0.449 945 0.448 0.449	1992 0.495 0.495 1991 0.995 0.995 1985 0.995 0.995 1985 0.995 0.995	1919 0.488 0.492 1481 0.488 0.491 1482 0.491 0.491	00.0 40.0 C00.0 C0	981 0.092 0.092 981 0.088 0.092 982 0.990 0.993	0.484 0.444 0.444 0.484 0.444 0.444 0.482 0.444 0.445 0.484 0.445 0.404	*****		00000	0.978 0.988
1	0.020 0.010	***************************************	00000	20000	86668	000000	90000	00000	00000	866 O	90000		9655	24555			10000	2224	10000	#####	10000	2444	25555	*****	*****
5	100 0.050 1		0.044											0.025			0.754 0.915			0.93		0.912 0.946			0.487 0.487 0.487 0.487 0.487 0.487 0.827 0.827
T=300° K	U(PE.CM.)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		98665	7,000				*****	******		0.910 0.982 0.982 0.988	20000			******	34655	0.450 0.410 0.000.000.000.000.000.000.000.000.000	20000	0.870 0.917 0.007	2444		0.780 0.854 0.054 0.054 0.054 0.054 0.775 0.775 0.775 0.775 0.775 0.054 0.751 0.054
; <u> </u>	00 2.000 1.000		78 0.047 0.001 81 0.047 0.001 84 0.493 0.095 96 0.493 0.005	12221	2222	22225	02 0.405 0.002 04 0.404 0.405 05 0.404 0.405 05 0.405 0.405	******	20000	25775	44444	23252	24 0.957 0.977 28 0.955 0.973 22 0.952 0.973 25 0.959 0.959	22425	55555	22228	72145	77 0-210 0-710 77 0-210 0-78 70 0-27 0-715	22222	33483	11712	15 0.752 0.852 14 0.757 0.814 16 0.762 0.862 16 0.762 0.827	35555		10.002 0.701 10.0312 0.428 10.0312 0.428 10.0314 0.514 17.0314 0.528
	10.00	18182 38383	25.00	22755	20000	*****	20000	4444	16355	00.475	\$3555	100.00	20000	0.45	22626	42222		24422	20101	0.362 0.302	*****	25.000	0.421 0.400 0.485 0.410 0.482 0.409	7427	2 0.30 0.10 0.10 0.10 0.10 0.10 0.10 0.10
Y.	90.00 20.00		26776	35555	42000	2020			72777			\$ 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		2000			14.55	20243	3433					23555	0 0.01 0.11 0 0.02 0.03 0.03 0.03 0.03 0.03 0.03 0.
•		2222222 2222222 2222222222222222222222	22222		11111	######################################	22222	22222	22,525	1224	25558	1277	2000	egggg	45555	1000	1000	12222	20124	2555	1200	99999	2000	12111	900000
	0,002 0.001	\$88.888 \$1.000000000000000000000000000000000000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1.000 1.000 6.449 1.000 1.000 1.000	C.944 1.666 C.944 1.666 C.944 1.666 C.944 1.666	0.447 0.448 0.447 0.448 0.447 0.448	0.440 C.444 C.402 C.403 C.400 C.403 C.400 C.403	0.434 C.541 C.480 C.487 C.41, C.427 C.41, C.422	C. 62	2000 2000 2000 2000 2000 2000 2000 200	0.432 C.444 C.431 C.444 0.431 C.444 0.431 C.444	C.41 C.43 C.44 C.45 C.47 C.45 C.46 C.493	0.910 C. 480 0.910 C. 471 0.910 C. 472 C. 412 C. 412		0.420 c.411 0.430 c.421 0.430 c.421 0.430 c.421	C. 53 C. 53 C. 53 C. 54 C. 54	6.472 0.480 6.472 0.480 6.472 6.940 6.475 6.940 6.475 6.940	6.473 6.483 6.473 6.483 6.493 6.483 6.483 6.483	0.435 0.484 0.435 0.488 0.435 0.488 0.436 0.489	C. 401 C. 404 C. 404 C. 404 C. 404 C. 404 C. 404 C. 404	0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.	0.991 0.994 0.996 0.990 C.994 C.596 0.994 0.497 C.998 0.994 0.497 C.998 0.994 0.498 C.998	0.44	0.444 C.444 C.444 C.444 C.444 L.COO	0.114 1.680
	0,010	20000000000000000000000000000000000000	0.444 1.000	20000	0.000	0.441 0.441 0.441 0.441 0.441 0.441	0.482	0.155 0.175 0.175 0.175 0.175 0.175	0.931 0.455 0.931 0.455 0.935 0.455 0.935 0.455	C.404 D.424 C.407 D.434 C.407 D.434	0.627 0.627 0.637 0.631 0.645 0.645	0.872	0.431 0.413 0.413 0.414 0.414 0.414 0.414 0.414 0.414	0.01 0.470 0.450 0.450 0.450 0.674 0.674	0.41 0.43 0.43 0.43 0.43 0.43 0.43 0.43	0.407 0.893 0.424 0.891 0.424 0.693	0.935 0.935 0.935 0.935 0.935 0.935 0.935 0.935	0.450 0.450 0.450 0.450 0.450 0.450 0.450	0.0000		2442 2442 2442 2442 2442 2442	200000			0.000 0.000 0.000 0.000 0.000 0.000 0.000
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· ·	_	5,000 2,000 1,000	0.462 0.917 0.984 0.462 0.914 0.984 0.498 0.914 0.982 0.459 0.914 0.982	0.412 0.450 0.472 0.450 0.474 0.098 0.455 0.088	0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90	0,477 0,485 0,437 0,485 0,481 0,985 0,468 0,978 0,468 0,478	0.947 0.989	0.910	0.4% 0.327 3.4% 0.8% 0.4% 0.883 0.9% 0.115 0.4%	0.451 0.451 0.451 0.451 0.451 0.451 0.451 0.451 0.451 0.451	0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40	0.87. 0.81 0.87. 0.90 0.873 0.92 0.873 0.93 0.885 0.93	0.446 0.434 0.404 0.434 0.404 0.428 0.880 0.428	0.812		0.405 0.442 0.881 0.443 0.881 0.413 0.787 0.413	0.804 0.815 0.812 0.881 0.810 0.883 0.731 0.845 0.738 0.845	0.828 0.898 0.789 0.898 0.782 0.848 0.4802 0.848	0.174 0.849 0.177 0.821 0.178 0.654 0.838 0.698	0.559 0.710 0.559 0.641 0.500 0.644 0.612 0.751	0.481 0.787 0.734 0.484 0.734 0.484 0.493 0.794	0.112 0.825	0.613 0.719 0.614 0.710 0.519 0.718 0.519 0.483	0.314 0.434 0.318 0.483 0.418 0.410 0.418 0.410	0.345 0.489 0.420 0.519 0.343 0.515 0.418 0.581	0.423 0.324 0.364 0.324 0.346 0.324 0.378 0.348	0.187 0.354 0.485 0.137 0.2780 0.408 0.080 0.2311 0.335 0.244 0.435 0.543	
TO VOICE		PREG. 30 00 20,00 10,00	6010-0 0.878 0.423 0.414 4020-0 0.874 0.421 0.416 6010-0 0.874 0.416 6050-0 0.870 0.417 0.411	0.404	0.772 0.472 0.472 0.472 0.472 0.473 0.473	0.920 0.450 0.191 0.831 0.197 0.665 0.881 0.427	0.487 0.429 0.869 0.417 0.750 0.819 0.730 0.819	0.025	0.00	0.55 0 0.75 0 0.	0.577	20000	0.01140	0.000	0.174 0.82 0.774 0.82 0.774 0.82 0.709 0.82	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00		00000	0.55	0.212	0.11	200	0.142	0.110	0.077	100 0 000 000 000 000 000 000 000 000 0	7210.0 0.001 0.029 0.038 7270.0 0.000 0.000 0.005 7270.0 0.001 0.001 0.003 7270.0 0.001 0.101 0.107	
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		. 50,00 20,00 10,00		0.424 0.712 0.514 0.712 0.514 0.723 0.704 0.723	0.229 0.000 0.230 0.000 0.729 0.000 0.729 0.000	32525	0.725 0.822 0.715 0.814 0.414 0.793 0.414 0.793	20000	0.145 0.64 0.172 0.64 0.171 0.64 0.171 0.64	C.71. C.423 C.711 C.334 C.116 C.334 C.116 C.344	6,77, 0,20 6,04, 0,15 6,04, 0,14 6,04, 0,14 6,04, 0,15 6,04, 0,15	0.012 0.01 0.012 0.012 0.012 0.012 0.012 0.012	0.012 0.022 0.012 0.022 0.024 0.023 0.024 0.223	0.62. 0.103 0.002 0.024 0.002 0.002 0.000 0.002 0.000 0.000	0.001 0.041 0.004 0.051 0.004 0.012 0.020 0.122	0.055 0.17 0.055 0.17 0.025 0.107 1.067 0.107	0.001 9.17 0.000 0.213 0.134 0.122 0.114 0.122	2.07a 0.203 0.129 3.244 0.18a 0.364 0.18 0.381	0.238 0.428 0.428 0.421 0.428 0.441 0.465 0.441	0.172 0.624 0.517 0.644 0.517 0.645 0.567 0.705	0.147 0.81 0.878 0.871 0.815 0.812 0.410 0.441	0.810 0.871 0.820 0.878 0.839 0.894 0.833 0.894	0.847 0.404 0.414 0.414 0.414 0.411		0.425 0.954 0.419 0.950 0.408 0.412 0.423 0.412	0 0.941 0.974 0.944 0 0.952 0.971 0.940 0 0.951 0.970 0.970 0 0.939 0.942 0.972	0 0.424 0.053 0.047 0 0.13 0.14 0.44 0 0.137 0.04 0.04 0 0.184 0.028 0.44	
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WATER VAPOR AT 0.02 ATMOSPHERE PRESSURE T=300° K

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	0.050 0.020 0.010	0.418 0.444 0.944 0.484 0.934 0.934 0.487 0.921 0.435 0.887 0.421 0.455 0.453 0.485 0.435	0.854 0.857 0.927 0.854 0.910 0.936 0.881 0.867 0.927 0.787 0.860 0.900	0.825 0.867 0.919 0.817 8.841 0.915 6.786 0.856 0.298 0.823 0.883 0.916 0.824 8.867 0.919	0.736 0.857 0.657 0.737 0.868 0.408 0.736 0.836 0.870 0.736 0.837 0.880	6.715 9.811 0.863 6.544 0.715 0.837 0.518 0.453 0.571 6.314 0.415 0.577	0.654 0.722 0.780 0.664 0.930 0.952 0.693 0.933 0.933 0.895 0.933 0.933	8.463 8.919 0.943 8.414 8.880 0.914 8.785 0.859 0.899 0.773 0.452 0.694	0.764 0.845 0.464 0.761 0.894 0.484 0.772 0.854 0.494 0.779 0.854 0.897	8.841 0.911 0.914 0.841 0.911 0.914 0.870 0.917 0.941 0.875 0.929 0.940	0.913 8.965 0.961 8.936 8.936 0.969 8.936 0.960 0.972 8.968 8.963 0.973 8.961 8.976 0.963	6.944 8.977 6.985 6.977 0.984 6.990 6.998 6.998 6.991 6.985 6.991 6.994 6.985 6.995 6.995	6,993 0,995 0,997 0,993 0,997 0,998 0,995 0,998 0,999 0,998 0,999	0.000 0.000 0.000 0.000 0.000 1.000 0.000 1.000 1.000 1.000 1.000 1.000	1,000 1,000	1,000 1,000	1,000 1,000	1.000 1.000		2007 11 14 14 14 14 14 14 14 14 14 14 14 14	L. 194 C.	1.45 0.44 0.44 0.45 0.47 0.44 0.45 0.47 0.44 0.45 0.47 0.44		C. W. C.	Less Cres Cres Cres Cres Cres Cres Cres Cres Cres Cres Cres		
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20cm ⁻¹	5,000 2,000 1,000	0.310 0.560 0.668 0.310 0.586 0.603 0.236 0.512 0.550 0.266 0.555 0.569	22.23	0.000 0.275 0.400 0.001 0.274 0.361 0.001 0.277 0.351 0.159 0.310 0.417	0.043 0.785 c.310 0.047 0.224 c.359 0.046 0.195 0.316 0.041 0.136 c.247	0.025 0.104 0.211 0.004 0.054 0.142 0.001 0.014 0.054 0.001 0.014 0.044	2.04.2 0.131 0.245 0.119 0.302 0.425 0.172 0.475 0.551 0.256 0.436 0.571	0.165 0.349 0.444 C.088 0.237 0.315 0.041 C.137 0.315 0.037 0.315 0.241	2.034 G. ING C.245 2.046 B. INZ G.261 2.045 G. ISS G.274 0.040 G. ISS G.274 0.102 G.244 G. ISS	0.211 0.517 0.504 0.221 0.547 0.504 0.224 0.425 0.544 0.334 0.421 0.545	0.410 0.544 0.470 0.500 0.850 0.734 0.548 0.477 0.758 0.850 0.788 0.873	0.445 C.747 C.452 0.770 C.851 C.894 0.434 C.874 C.904 0.434 C.874 C.904	0.415 0.445 0.441 0.415 0.445 0.441 0.445 0.441 0.441	0.447 C.980 D.987 0.988 D.981 D.988 0.988 D.988 C.988 0.988 D.997 C.998				2. *** 0. *** 1. *** 0. *** 1. *** 0.	0,447 0,444 0,444 0,444 0,444 0,444 0,445 0,444 0,444 0,445 0,444 0,444							200 C. 10 C.	
AVERAGED OVER	FREG. 50.00 20.00 10.00	0.055 C.179 G.250 C.024 G.100 0.197 O.005 G.044 D.127 O.006 G.059 O.144	0.001 0.019 0.047 0.001 0.023 0.041 0.001 0.014 0.059 0.002 0.005 0.030 0.002 0.005 0.030	0.000 0.000 0.003 0.000 0.005 0.031 0.000 0.005 0.033 0.000 0.000 0.053	0.000 0.002 0.002 0.000 0.002 0.002 0.000 0.002 0.003 0.000 0.001 0.000	0.000 0	0.000 C.001 0.009 0.000 0.005 0.035 0.000 0.015 0.071 0.000 0.022 0.095	0.016 0.067 0.001 0.024 0.001 0.014 0.001 0.014	0.000 C.CC0 0.004 0.000 0.001 0.009 0.000 0.001 0.004 0.000 0.003 0.018 0.000 0.007 0.035	0.001 0.014 0.056 0.004 0.048 0.187 0.004 0.041 0.113 0.007 0.044 0.184 0.013 0.066 0.184	0.00 0.20 0.279 0.00 0.20 0.38 0.078 0.227 0.365 0.120 0.267 0.817	0.288 C.468 0.591 0.173 0.565 0.479 0.649 0.417 0.721 0.507 0.476 0.770 0.587 0.736 0.814	0.673 0.804 0.868 0.449 0.479 0.479 0.777 0.875 0.919 0.826 0.907 0.941	0.653 0.923 0.950 0.846 0.528 0.953 0.886 0.994 0.984 0.911 0.657 0.973 0.921 0.984 0.978	0.933 0.984 6.981 0.945 0.482 6.982 0.450 0.982 0.988 0.951 0.983 0.992	0.944 0.484 0.492 0.544 0.484 0.490 0.971 0.988 0.493 0.971 0.988 0.493	0.975 0.989 0.984 0.975 0.989 0.993 0.975 0.989 0.995 0.976 0.993 0.995	0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00%	0.083 0.093 0.094 0.078 0.090 0.095 0.077 0.080 0.093 0.073 0.085 0.093	0.945 0.980 0.981 0.983 0.979 0.984 0.950 0.974 0.984 0.450 0.975 0.984	0.424 6.954 0.970 0.414 0.947 0.443 0.401 0.438 0.457 0.890 0.452 0.453 0.687 0.452 0.453	0.225 0.915 t.940 0.639 0.896 6.924 0.836 0.697 0.927 0.812 0.681 0.915 0.821 0.087 0.915	0.244 0.915 0.939 0.844 0.914 0.915 0.844 0.914 0.915 0.790 0.911 0.951 0.903 0.905 0.958	0.063 0.013 0.039 0.427 0.722 0.020 0.561 0.400 0.764 0.479 0.778 0.836 0.751 0.851 0.074	0.777 0.854 0.864 0.529 0.957 0.949 0.634 0.958 6.978 0.808 0.867 0.981 0.804 0.845 0.899	#210_0 0.403 0.43# 8.45# 8.45# 8.25	
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	0.050 0 020 0 050.0	0001 0007 0060 0001 0000 0060 0000 0000	68668	66666	88888	88888	20200	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	90000	00000					0.984 G.995 E.498 C.994 D.998 G.497 C.994 D.998 G.487 G.992 C.995 G.998 G.991 G.495 G.998	17711	0.991 0.994 0.994 0.949 0.981 0.981 0.977 0.985 0.980 0.977 0.985 0.980	0.982 0.982 0.982 0.978 0.987 0.491 0.987 0.588 0.982 0.982 0.978 0.984	0.451 0.464 0.976 0.455 0.475 0.985 0.985 0.476 0.985 0.980 0.487 0.991 0.482 0.995 0.997	0.003 0.000 0.000 0.000 0.000 0.076 0.005 0.000 0.076 0.006 0.000 0.000 0.000	0.956 C.980 C.984 0.953 G.971 C.980 0.942 G.974 G.965 0.977 0.985 C.987	0.07% 0.48% 0.48% 0.5% 0.47% 0.48% 0.0% 0.47% 0.48% 0.4% 0.47% 0.48% 0.4% 0.48% 0.48%	0.025 0.042 0.067 0.025 0.065 0.069 0.078 0.006 0.000 0.072 0.045 0.008 0.005 0.078 0.085	0.444 0.481 0.487 6.470 0.482 0.487 6.484 0.481 0.482 0.471 0.483 0.486 0.487 0.480 0.484		0.417 0.447 0.977 0.433 0.436 0.471 0.414 0.447 0.943 0.412 0.443 0.943	
T=300° K	UPR.CM.1 0.500 0,200 0,100			0.996 0.997 c.498 0.998 0.998 0.999 0.998 0.999 0.999 0.998 0.999 0.999		20000	0.998 1.000 1.000 1.000 1.000 1.000 0.999 0.999 1.000 0.999 0.999 1.000	*****	0.007 0.030 0.030 0.005 0.007 0.008 0.006 0.008 0.008 0.005 0.007 0.008	0.003 0.905 0.906 0.905 0.905 0.907 0.605 0.907 0.908 0.605 0.907 0.908	0.075 0.086 0.403 0.071 0.083 0.060 0.070 0.087 0.462 0.041 0.007 0.408	0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00%	0.065 0.062 0.065 0.068 0.092 0.005 0.085 0.092 0.095 0.065 0.092 0.095	0.484 0.994 0.595 0.986 0.991 0.995 0.985 0.991 0.964 0.985 0.997 0.998	0.978 0.987 0.991 0.975 0.986 0.990 0.977 0.986 0.990 0.987 0.982 0.988	0.946 0.480 0.980 0.961 0.974 0.481 0.977 0.980 0.990 0.977 0.984 0.990	*****				****			0.467 0.934 0.454 .0.059 0.404 .0.401 0.404 0.40	*****	1,638 0,645 0,425 1,795 0,847 0,405 1,737 0,638 0,678 1,737 0,628 0,674	
<u>π</u>	5.000 2.000 1.000	0.982 6.988 0.985 6.999 0.986 6.999 0.986 6.999	0.000 0.000		0.001 C.004 0.001 C.000 0.001 C.000	0.000 0.000		**************************************	0.002 C.005 0.003 C.002 C.004 C.001 C.004 C.001	0.000 C. 000 0.000 C. 000 0.000 C. 000 0.000 C. 000	0.954 0.958 0.954 0.958 0.954 0.956 0.955 0.956 0.955 0.950		500 C		2,455 C. 055 2,455 C. 055 2,455 C. 055 2,415 C. 955 2,415 C. 955		46482	-	2000		20055	C. 640 0.845 0.755 0.818 0.755 0.818 0.760 0.828 0.810 0.863	0.000 0.000 0.000 0.000 0.000 0.000	0.804 0.854 0.804 0.863 0.818 0.842 0.747 0.854	52555	0.354 0.444 0.777 0.577 0.421 0.424 0.435 0.435 0.435 0.435 0.435 0.435 0.435 0.441	
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	50 00 20,00 10,00	0.479 C.087 A.040 C.485 C.485 C.480 C.485 C.485 C.303 C.485 C.485 C.303	0.002 0.370 0.003 C-004 C-017 C-044 C-015 C-044 C-060 O-055 C-021 C-063	0-458	2.40. C.912 C.952 2.70. C.911 B.937 C.44C C.892 C.927 F.803 C.915 C.927	0.759 0.871 0.309 0.759 0.831 0.877 0.759 0.812 0.960 0.767 0.864 0.960	0-51- C-702 6-179 0-53- C-645 9-751 0-52- C-649 C-756 0-515 0-647 C-752 0-55- C-644 C-752	6-397 0-514 0-653 6-651 0-655 0-527 6-234 0-623 0-527 6-234 0-623 0-527 6-234 0-631 0-665	0.27 6.281 0.412 0.04 6.185 f.70 0.05 6.117 6.274 0.018 6.117 6.218	6-211 G.OT C-18. 6-Cd C.GG C-187 6-CG C-GG C-187 1-GF C-107 C-181	1001 C-914 C-925 C-001 C-914 C-925 C-001 C-925 C-925 C-001 C-925 C	6-60 C.00 6-20 C.00 C.00 C.00 C.00 C.00 C.00 C.00 C.	C-CCC C-00% 0-02% C-007 C-01% 0-05% C-04% L-14% 0-27% C-04% C-14% 0-40% C-04% C-14% 0-40%	5.021 0.037 5.193 5.021 0.037 5.035 5.031 0.033 6.033 5.030 0.033 6.033 5.030 0.033 6.033	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.000 0.002 0.019 0.003 0.002 0.121 0.003 0.000 0.105 0.003 0.021 0.044	0.332 0.036 0.043 0.001 0.017 0.043 0.001 0.015 0.018 0.001 0.015 0.018	0.513 0.077 0.173 0.517 0.591 0.163 0.517 0.514 J. 166 0.527 0.516 0.189 0.552 0.167 0.264	0.058 C.190 0.130 0.057 C.191 0.325 0.061 G.239 0.384 0.107 0.304 0.415 0.127 0.304 0.415	0.111 G.272 C.103 G.103 G.243 G.339 O.744 G.334 G.437 G.175 G.350 G.174 O.200 C.340 G.444	0.345 0.558 0.578 0.395 0.548 0.677 0.775 0.550 0.700 0.273 0.556 0.568 0.317 0.655 0.568	0.351 0.524 0.639 0.330 0.504 0.619 0.638 0.601 0.700 0.489 0.638 0.727 0.535 0.671 0.752	0.521 0.655 0.739 0.565 0.707 0.704 0.559 0.688 0.768 0.572 0.703 0.768	0.629 0.749 0.817 0.653 0.744 0.828 0.623 0.736 0.605 0.557 0.775 0.786 0.403 0.723 0.800	0.000 G.780 G.841 0.790 G.640 G.963 0.624 G.665 G.917 G.828 G.667 G.919 G.700 G.862 C.919	0.777 C.859 0.883 0.253 0.284 0.914 0.250 0.904 0.93 0.244 0.914 0.938 0.244 0.914 0.958	
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300° K	UPR.CM.] 0,500 0,200 0,1					0.000 0	0.423 0.443 0.043 0.043 0.043 0.043 0.043 0.043 0.044 0		00000	0.450 0.415 0.000	0.476 0.485 0. 0.476 0.487 0. 0.474 0.487 0. 0.474 0.484 0.	0.477 0.986 0. 0.475 0.985 0. 0.475 0.986 0. 0.476 0.986 0.	0.980 0.988 0.098 0.008 0.008 0.008 0.008 0.008 0.008 0.008 0.008 0.008 0.008 0	******	0.455 0.472 0.000 0	0.944 0.927 0.927 0.944 0	0.434 0.471 0.434 0.454 0.444 0.484 0.444 0.484 0.444 0.484	0.012	33355	32555	0.900 0.437 0.000 0.437 0.000	2222	0.177 0.42	0.027 0.889 0.745 0.745 0.827 0.741 0.827 0.741	0.700 0.800 0. 0.640 0.736 0. 0.587 0.719 0. 0.726 0.819 0.
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; }	10.00 \$ 000	00000 00000 00000 00000	12223	1000	9999	9.000	******	25454	::::::	50200				0.451 0.430 0.657 0.699 0.828 0.852 0.797 0.850							0.611 0.708 0.583 0.684 0.531 0.649 0.508 0.649				
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	7HEO.	601000 601000 601000 601000 601000 601000 601000 601000 6010000	0.00000	2000	\$220.0 \$230.0 \$240.0 \$240.0	0.0000	22222	0.05654	000000	410.0 6140.0 6140.0 6140.0	\$310.0 \$310.0 \$310.0 \$310.0	6550.0 6550.0 6550.0 6550.0	00000	6440.0 6440.0 6440.0 6440.0	277.00	4700.0 6770.0 6770.0	6.520.0 6.520.0 6.530.0 6.530.0	44444	4910.0 6420.0 6420.0 6450.0	2440.0 2440.0 2440.0 2600.0	7010.0	701 701 701 701 700 700 700 700 700 700	111111	711000	7210-0 7220-0 7230-0 7230-0 7250-0
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WATER VAPOR	0.919 0.968 0.978 0.949 0.969 0.978 0.949 0.959 0.978 0.534 0.959 0.977	0.444 0.445 0.476 0.415 0.446 0.476 0.415 0.419 0.476 0.416 0.411 0.451	0.875 0.920 0.943 0.876 0.944 0.945 0.915 0.944 0.975 0.935 0.965 0.973	0.681 0.425 0.447 0.681 0.477 0.448 0.425 0.435 0.468 0.429 0.436 0.416	0.515 0.751 0.551 0.527 0.555 0.565 0.584 0.516 0.555 0.485 0.594 0.545																					
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UPR.CM]	0.000 0.001 0.000 0.001 0.001 0.001 0.001 0.001	0.440 0.441 0.441 0.444 0.441 0.444 0.441 0.441	000000000000000000000000000000000000000	00000	0.112 0.113 0.114 0.114 0.114 0.114 0.114	0.485	000000000000000000000000000000000000000	0.995 0.940 0.988 0.940 0.988 0.988	0.919 0.919 0.919 0.919 0.919 0.919	0.419 0.987 0.419 0.486 0.987 0.491 0.467 0.491	0.082 0.940 0.082 0.941 0.045 0.991 0.045 0.990	00000	0.434 0.434 0.434 0.444 0.444 0.444 0.444 0.444	00000	00.00	0.947 0.446 0.947 0.446 0.948 0.948 0.948 0.948	00000	0.444 0.449 0.449 1.000 0.449 1.000 0.449 1.000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	0.999 1.000 1.000 0.999 1.000 1.000 0.999 0.999 1.000 0.939 0.999 1.000	0.434 1.000	0.937 0.948 0.937 0.948 0.497 0.548	0.974 0.974	
3,000 2,000 1,000	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00	0.444 0.474 0.444 0.474 0.444 0.477 0.447 0.477		100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 10	60.00 60.00			256-06-06-06-06-06-06-06-06-06-06-06-06-06	74466	0.137 C.134 0.137 C.135 0.134 C.135 0.149 C.149	0.110 0.110 0.110 0.110 0.110 0.110 0.110	0.474	0,477 0,485 C,481 C,487 C,485 C,486 G,785 C,488	0.982 0.982	00.014	0.440 0.493 0.440 0.493 0.442 0.494 0.993 0.495	**************************************	0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444	0.448 0.449 0.448 1.000 0.449 0.449 0.449 0.449	0.000 0.000	0.948 0.949	0.545 0.947 6.494 0.946 0.948 0.494 0.946 0.949 0.949 0.946 0.949 0.948 0.949 0.949 0.949	0.00	0.48 0.48 0.48 0.48 0.48 0.48	0.000	
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OVER

AVERAGED

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OVER 2	10,00		88888	88888										9665							20000	******				00000
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	0 005 0.002 0.001	88888	88888	20000	1.003 1.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000 0.000 1.000 1.000	23623	0.000 0.007 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.002 C.002 0.000 0.000 C.002 0.000 0.000 C.002 C.002 0.000 C.002 C.002 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.542 C.467 C.441 0.542 0.464 0.414 0.714 C.744 0.414 0.831 C.487 0.432 0.734 0.438 0.846	0.729 C.200 0.645 0.729 C.200 0.675 0.727 C.20 0.681 0.714 0.727 0.880	6.51 6.44 6.145 6.51 6.44 6.145 6.47 6.44 6.748 6.51 6.10 6.140	0.5% 5.722 6.735 0.430 0.151 0.625 0.431 0.8% 0.423 0.423 0.466 0.472 0.423 0.482	0.716 0.813 0.813 0.414 0.823 0.878 0.889 0.708 0.858 0.859 0.718 0.808	0.561 0.721 0.401 0.561 0.721 0.401 0.560 0.103 0.186 0.515 0.661 0.756	0.519 0.442 0.752 0.474 0.433 0.848 0.773 0.452 0.403 0.477 0.789 0.453 0.476 0.747 0.861	C.731 C.430 C.855 O.475 O.791 O.856 O.474 C.793 O.459 O.700 O.814 O.477 C.717 C.826 O.884	6.836 6.468 0.441 0.833 6.468 0.424 0.774 6.484 6.454 0.437 6.415 0.444	C.073 C.073 C.044 C.045 C.013 C.055 C.075 C.052 C.040 C.075 C.054 C.073	0.414 0.414 0.440 0.414 0.414 0.452 0.401 0.417 0.421 0.417 0.454 0.471	0.448 0.472 0.484 0.444 0.448 0.484 0.494 0.448 0.474 0.414 0.411 0.482	0.944 0.983 0.940 0.985 0.982 0.990 0.982 0.995 0.995 0.982 0.995 0.995	0.977 0.989 0.994 0.992 0.994 0.994 0.992 0.994 0.998 0.992 0.994 0.998	0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.044 0.444 0.444	0.447 0.444 0.444 0.444 0.444 1.000 0.444 0.444 1.000 0.444 1.000 1.000 0.444 1.000 1.000	0.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1
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	316	20072	2000	12516		55535	22222	13315	10111	12212	11111	12333	17773			=====	12111	=====	*****		12000	22222	22222	####	11112	

WATER VAPOR AT 0.50 ATMOSPHERE PRESSURE

20cm⁻¹

OVER

AVERAGE OVER 20	14 C K K K C C C C C C C C C C C C C C C	88888 88888	. 2228	88888						·														
WATER VAPOR AT 0.50 · ATMOSPHERE PRESSURE T=250° K	100°0 100°0 500°0 010°0 0260°0 0560°0 001°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°0 000°		6.57 (4.58) 6.47 (5.78) 6.49 5.49 5.49 6.44 6.44 6.44 6.44 6.44 6.44 6.44 6	0071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 00071 0	881 8821 1410 1410 1410 1410 1410 1410 1410 14			-														-		
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U.ZU AIMU	I=250° K	0.50	15 0.491 0.494 0.494 19 0.494 0.494 10 0.495 0.498 0.499 11 0.495 0.498 0.499	0.997 0.499 0.998 0.999 0.998 0.999 0.998 0.999	0.994 0.998	1.000 1.000 0.446 0.440 0.442 0.446 0.443 0.444	1.000 1.000	1.000 1.000	0.442	\$55.0 786.0 \$55.0 786.0 \$55.0 786.0	0.987 0.984 0.980 0.994 0.987 0.994 0.995 0.994	2222	0.981 0.941 0.980 0.981 0.982 0.983 0.983 0.983	0.942 0.984	0.946 0.985 0.986 0.985 0.986 0.985 0.487 0.981	20000	0.842 0.904 0.842 0.904 0.912 0.905 0.912 0.905	0.119 0.425 0.119 0.425 0.410 0.14 0.724 0.815 0.652 0.909	0.751 0.836 0.720 0.815 0.744 0.845 0.599 0.724 0.506 0.855	0.137 0.618 0.139 0.105 0.743 0.705 0.703 0.735	0.797 0.673 0.797 0.673 0.681 0.789 0.674 0.788	0.568 0.720 0.585 0.708 0.688 0.708 0.683 0.795	0.687 0.745 0.624 0.714 0.554 0.402 0.568 0.705	9555	0.651 0.774 0.491 0.805 0.691 0.805 0.685 0.806 0.661 0.806	11 0.469 0.747 0.479 15 0.500 0.113 0.709 11 0.518 0.473 0.744 18 0.479 0.639 0.739	6. 0.317 0.411 0.761 0.517 0.417 0.402 1. 0.213 0.447 0.402 1. 0.249 0.440 0.517	
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AVERAGED OVER	FREG. 50,00 20,00 10,00	0.000 0.004 0.000 0.004 0.000 0.004 0.000 0.000	200000	0.000 0.004 0.000 0.004 0.000 0.002 0.000 0.002	0.000 0.003 0.000 0.007 0.002 0.028 0.001 0.013	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.025 0.128 0.025 0.132 0.012 0.031 0.013 0.034	0.043 0.150 0.024 0.115 0.030 0.142 0.042 0.182	0.034 0.144 0.063 0.202 0.036 0.163 0.038 0.138	0-137 0-187 0-324 0-137 0-794 0-430 0-230 0-409 0-537 0-748 0-423 0-546 0-247 0-431 0-550	0-409 0-583 0-691 0-462 0-622 0.719 0-553 0-697 0.783 0-552 0-777 0-797 0-875 0-804 0-865	0.698 0.817 0.874 0.785 0.864 0.909 0.767 0.868 0.915 0.446 0.784 0.857 0.656 0.771 0.861	0.709 0.867 0.429 0.889 0.949 0.968 0.284 0.945 0.967 0.894 0.947 0.948 0.403 0.453 0.473	0.442 0.912 0.944 0.247 0.914 0.944 0.854 0.931 0.957 0.854 0.921 0.950 0.854 0.922 0.934	0.491 C.447 0.469 0.914 0.459 0.475 0.937 0.469 0.981 0.931 0.965 0.478 0.541 C.470 0.482	0.941 0.971 0.983 0.940 0.970 0.983 0.945 0.974 0.983 0.912 0.947 0.981 0.942 0.972 0.984	0.435 0.464 0.480 0.882 0.433 0.454 0.874 0.930 0.453 0.673 0.425 0.450 0.673 0.924 0.449	0.11, 0.12, 0.93 0.44, 0.40, 0.43 0.44 0.40, 0.13 0.74 0.67, 0.412 0.75 0.85 0.402	0.760 C.851 0.400 0.72) 0.824 0.877 0.755 0.844 0.841 0.750 0.841 0.841	0.745 0.874 0.913 0.746 0.845 0.842 0.751 0.845 0.877 0.721 0.673 0.782	0.374 0.541 0.652 0.412 0.573 0.677 0.510 0.441 0.150 0.455 0.441 0.711	0.612 0.747 0.621 0.434 0.601 0.703 6.334 0.533 0.647 0.406 0.539 0.687	0.453 0.425 0.724 0.398 0.572 0.681 0.300 0.471 0.599 0.433 0.582 0.890 0.576 0.723 0.806	0-421 0-544 0-640 0-301 0-456 0-541 0-240 0-445 0-547 0-278 0-445 0-555 0-278 0-498 0-524	0.343 0.534 0.655 0.301 0.477 0.597 0.304 0.474 0.590 0.384 0.545 0.648 0.484 0.657 0.737	0.415 0.587 0.884 0.403 0.513 0.880 0.525 0.549 0.627 0.485 0.514 0.627
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<u>-</u>	5.000 2.000 1.000	0,412 D.947 C.965 0.907 O.945 C.965 0.841 O.913 C.946 0.876 C.425 D.946		9.99	0.947 0.449 0.481 0.629 0.889 0.422 0.408 0.877 0.913 0.918 0.939 0.470 0.908 0.941 0.944		20000	22760			22224	10000	2222	0.745 0.858 0.405 0.745 0.857 0.404 0.747 0.859 0.407 0.747 0.842 0.843	11111	0.525 0.617 0.746 C.538 0.686 0.775 C.580 0.721 0.801 D.638 0.641 0.736 0.511 0.464 0.755	*****	37462	35555		0.525				0.047 0.147 0.244 0.054 0.149 0.244 0.054 0.170 0.241 0.054 0.178 0.508 0.017 0.017 0.185	0.003 0.037 0.043 0.003 0.019 0.043 0.000 0.004 0.027 0.000 0.005 0.023 0.020 0.000 0.148
	PREG. 30,00 20 00 10,00	4010.0 0.4% 0.401 0.8% 4020.0 0.472 0.801 0.8% 9030.0 0.472 0.801 9040.0 0.470 0.871 4050.9 0.399 0.7% 0.821	0.641 0.725 0.74 6.647 0.74 6.647 0.745	0.441 6.707 0.574 6.707 0.574 6.707 0.41 4.717	0.705 0.481 0.512 0.690 0.518 0.650 0.651 0.615 0.615 0.615	0.640 C.608 0.540 C.608 0.513 G.714 0.110 0.573	0.35 0.712 0.35 0.711 0.416 0.413 0.418 0.347	0.23 C.23 0.23 C.23 0.23 C.23 0.23 C.23 0.24 C				0.28¢ 0.442 0.312 0.443 0.317 0.246 0.247 0.24	6.302 0.48 9.783 0.48 0.33 0.48 0.31 0.313 0.31 0.313	0.177 0.188 0.181 0.188 0.181 0.188		0.134 0.242 0.134 0.242 0.234 0.228 0.235 0.228	0.124 0.734 0.734 0.734 0.139 0.139 0.139	20000	0.003 0.014 0.003 0.014 0.003 0.014 0.004 0.003	0.001 0.011 0.048 0.112 0.019 0.112 0.019 0.114	0.014 0.100 0.027 0.108 0.020 0.054 0.034 0.125	35555	66.666 66.666	00000	0.000 0.000 0.000 0.001 0.000 0.001 0.000 0.001	90000
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	5 000 2,000 1,000	70077	0.410 0.419 0.418 0.410 0.715 0.418 0.402 0.725 0.798 0.718 0.417 0.870 0.629 0.847 0.930	*****	20000		11977	20712	0.335 0.519 0.611 0.288 0.483 0.611 0.211 0.341 0.528 0.137 0.310 0.455 0.348 0.328 0.470	0.047 C.184 D.294 0.043 C.184 D.294 0.043 C.184 C.274 0.047 C.188 C.274 0.047 C.188 C.274	50000	0.00+ 0.042 0.121 0.008 0.014 0.130 0.015 0.014 0.212 0.042 0.212 0.135 0.046 0.230 0.387	6.01 6.02 6.03 6.01 0.02 6.03 6.00 0.03 6.03 0.00 0.00 0.03 0.00 0.00 0.03	55555	0.023 d.099 d.201 0.089 0.226 0.381 0.197 0.281 0.402 0.99 d.197 0.259	0.034 0.134 0.334 0.034 0.145 0.250 0.034 0.144 0.284 0.107 0.286 0.444	0.04 0.223 0.357 0.107 0.237 0.345 0.141 0.334 0.489 0.229 0.418 0.349	0.127 0.504 0.624 0.400 0.570 0.679 0.445 0.447 0.793 0.519 0.779 0.844	0.644 0.784 0.848 0.704 0.815 0.874 0.704 0.815 0.874 0.748 0.647 0.899 0.778 0.678 0.920	0.910 0.434 0.447 0.910 0.434 0.473 0.911 0.973 0.985 0.911 0.945 0.980 0.912 0.948 0.947	0.403 C.442 0.462 0.418 0.455 0.972 0.418 0.955 0.972 0.415 0.444 0.975 0.415 0.405	0.414 0.417 0.467 0.414 0.415 0.415 0.417 0.417 0.414 0.417 0.414 0.417 0.414	0.474 0.484 0.494 0.490 0.492 0.494 0.489 0.494 0.498 0.489 0.494 0.498	0.984 0.994 0.494 0.978 0.994 0.994 0.978 0.994 0.995 0.495 0.994 0.995		10000
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20cm ⁻¹	5.000 2.000 1.000	0-129 0-303 C-448 0-195 0-246 C-374 0-077 0-197 0-317 0-085 0-217 C-345 0-045 0-134 0-235	95556	250000	12000	6.000 0.003 0.021 6.000 0.001 0.000 6.000 0.000 0.000 6.000 0.000 0.000	20.000	35555	0.000 0.003 0.034 0.000 0.006 0.031 0.000 0.009 0.034 0.001 0.014 0.034	72427	23252	12531	2250	20000	22222	*****	******	0.445 0.949 1.000 0.446 0.994 1.000 0.496 0.999 1.000 0.496 0.948 1.000 0.496 0.999 1.000		57045	55555	55556	0.473 0.420 0.443 0.407 0.942 0.954 0.897 0.936 0.954 0.415 0.47 0.962 0.428 0.957 0.970	0.901 0.940 0.948 0.747 0.877 0.879 0.659 0.767 0.829 0.764 0.843 0.885	0.671 0.680 0.917 0.978 0.978 0.964 0.948 0.968 0.968 0.822 0.976 0.908 0.820 0.674 0.908	0.314 0.960 0.413 0.428 0.496 0.947 0.450 0.977 0.460 0.916 0.912 0.779 0.848 0.888	
AVERAGED OVER	8	3310.9 0.000 0.001 0.043 3320.0 0.000 0.006 3330.0 0.000 0.006 3360.0 0.000 0.004 3360.0 0.000 0.004	000000000000000000000000000000000000000	88888	000000000000000000000000000000000000000	0.000	95555	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	23828	0000 00000 0000 00000 0000 00000 0000 00000	0.001 0.029 0.001 0.029 0.001 0.029 0.004 0.013	0.004 0.294 0.004 0.294 0.157 0.376 0.237 0.487	0.34 0.652 0.436 0.653 0.406 0.763 0.346 0.786	0.597 C.EG3 0.60C G.EG3 C.EG3 G.E20 C.EG3 G.E20 G.EG3 G.E20 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3 G.EG3	4160.0 0.710 0.812 0.916 4170.0 0.715 0.887 0.445 4170.0 0.717 0.897 0.447 4170.0 0.735 0.894 0.947 4200.0 0.777 0.493 0.952	0.786 C.909 0.789 C.919 0.795 C.911 0.816 C.923	0.612 0.932	0.477 0.454 0.485 0.458 0.486 0.458 0.492 0.464	0.896 C.464 0.896 C.464 0.896 C.462 0.891 0.980	0.472 0.45 0.872 0.44 0.872 0.44 0.451 0.43	20000	0.710 0.624 0.643 0.774 0.665 0.776 0.553 0.712	4500.0 0.607 0.744 0.857 4580.0 0.470 0.794 0.756 4580.0 0.470 0.794 0.756 4500.0 0.716 0.878 4600.0 0.716 0.645 0.886	2555	4460.0 0.568 0.691 6.762 6-70.0 0.613 0.401 0.935 4-80.0 0.602 0.711 0.735 4-700.0 0.603 0.711 0.770	4710-0 0.15) C.657 C.401 4720-0 0.747 C.654 0.285 4740-0 0.479 C.673 0.415 4740-0 0.490 0.453 0.412	
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	1,000 2,000 1,000	0.913 0.985 0.990 0.979 0.986 0.992 0.979 0.988 0.993 0.985 0.993 0.985 0.993	0.445 0.447			2,444 0,944 2,444 1,000 0,944 1,000 1,940 1,000	0.449 1.000	0.441 0.441	74961		######################################						97.22		55386	\$\$\$\$\$		24135	76555	00000 00000 00000 00000 00000 00000 0000	0.542 0.643 0.553 0.623 0.423 0.534 0.423 0.534	1.315 C.501 D.421 1.210 0.346 D.519 1.101 0.267 0.415 1.086 0.234 C.388	
	PREG, 30.00 20 00 10.00	2246.0 0.874 0.938 0.940 0 7220.0 0.889 0.949 0.849 2240.0 0.888 0.949 0.942 2340.0 0.888 0.849 0.972	0.931 0.484 0.924 0.432 0.487 0.485 0.432 0.487 0.485 0.456 0.487 0.485	0.41 0.47 6.48 0.41 6.45 0.48 0.44 0.48 0.49 0.44 0.48 0.49 0.44 0.49	0.410 0.481 0.485 0.480 0.485 0.481 0.413 0.485 0.488 0.413 0.483 0.489	0.464 0.988 0.497 0.475 0.493 0.497 0.476 0.493 0.497 0.476 0.440 0.442	0.924 0.442 0.496 0.916 0.493 0.947 0.959 0.987 0.992 0.934 0.987 0.492	0.75 0.96 0.48 0.91 0.91 0.48 0.93 0.967 0.979 0.92 0.941 0.974	0.663 0.918 0.914 0.863 0.914 0.914 0.840 0.917 0.957 0.831 0.915 0.937	0.6ac 0.920 0.443 0.618 0.920 0.921 0.665 0.920 0.445 0.748 0.911 0.919 0.766 0.657 0.902	0.505 0.735 0.805 0.501 0.643 0.730 0.512 0.724 0.741 0.634 0.685 0.921 0.639 0.686 0.422	0.740 0.966 0.017 0.82 0.930 0.91 0.711 0.926 0.816 0.623 0.744 0.814 0.659 0.775 0.816	0.673 0.785 0.647 0.691 0.872 0.954 0.724 0.872 0.874 0.678 0.795 0.850	0.753 C.851 C.848 0.702 C.815 C.871 0.497 C.812 C.868 0.476 C.807 C.861 0.476 C.807 C.861	0.416 0.739 0.831 0.536 0.723 C.AC2 0.535 C.636 0.782 0.455 0.631 0.732 0.467 0.531 0.732	0.14c 7.55c 0.075 0.13c 2.32c 0.048 0.162 7.55c 0.870 0.402 0.882 0.777 0.517 0.889 0.780	0.428 0.406 C.711 0.178 0.340 0.472 0.425 0.420 C.343 0.425 0.386 0.449	0.187 C.171 0.505 6.174 C.138 0.418 0.184 C.381 0.318 0.184 C.211 0.320	00r 0.0b0 0.117 0.r10 0.0b7 0.1b2 0.r45 0.136 0.251 0.114 0.362 0.492 0.411 5.618 0.735	0.239 G.430 0.383 0.239 G.430 0.557 0.117 6.284 0.594 0.11* 0.287 G.499 0.15 G.149 6.499	0.024 0.140 0.294 0.020 0.086 0.179 0.040 0.192 0.111 0.087 0.251 0.397 0.044 0.207 0.314	0.10* (.245 0.405 0.672 0.224 0.330 0.64* 0.145 0.254 0.03* 0.137 0.255 0.639 0.165 0.303	0.00 0.10 0.10 0.11 0.25 0.40 0.10 0.32 0.46 0.00 0.24 0.19 0.01 0.11 0.21	0.054 0.144 0.112 0.054 0.103 0.134 0.057 0.201 0.35 0.043 0.185 0.342	0.024 0.124 0.259 0.013 0.019 0.204 0.010 0.017 0.114 0.002 0.037 0.115	100 0.00 0.017 0.173 0	
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PRESSURE	
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		OVER	20.00		0.005 c.024 0.078 0.007 c.024 0.078 0.006 c.005 0.027 0.006 c.005 0.025	0.016 0.002 0.170 0.020 0.043 0.108 0.007 0.043 0.108 0.007 0.059 0.129	16.22	0.074 0.194 0.097 0.194 0.097 0.194 0.117 0.239	0.379 0.500	48171	*****	*****	22542			50235		20000	0.978 0.938 0.960 0.934 0.958 0.912 0.951 0.912	25.55	20161	20000	0-774 0-199 0-742 0-845 0-775 0-859 0-806 0-860	6-771 0-835 6-771 0-835 6-772 6-803 6-782 6-878 6-786 6-878	22323	0.512 0.513 0.387 0.512 0.433 0.338 0.498 0.625 0.709 0.504 0.613 0.703	0.603 C.735 0.809 0.547 0.684 0.785 0.543 0.675 0.751 0.603 C.721 0.701 0.104 0.713 0.868	0.446 C.763 0.828 0.432 0.481 0.831 0.534 0.482 0.767 0.514 0.102 0.728 0.616 0.783 0.843
		AVERAG							· <u></u> -				7776	7746.0 77760.0 7790.0	7810.0	78870 78870 78870 78870 78870 78870	2000	200000		2000 2000 2000 2000 2000 2000 2000 200	0.025	22000						
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OVER

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UPE.CM] 0.506 0.700 0.100		0.00	0.910 0.936 0.893 0.924 0.919 0.923 0.933 0.933	20000	0.933 0.938 0.970 0.938 0.941 0.973 0.944 0.958 0.971 0.931 0.935 0.975	20125	0.943 0.945 0.975 0.948 0.47 0.973 0.939 0.971 0.979 0.945 0.975 0.975				******	!!!!!	0.018 0.999 1.000 0.019 0.019 1.000 0.019 1.000 1.000 0.019 0.019 1.000	0.949 1.000 1.000 0.949 1.000 1.000 0.949 1.000 1.000 0.999 1.000 1.000	0.94* 1.000 1.000 0.94* 0.94* 0.45* 0.94* 0.94* 0.94* 0.94* 0.94* 0.94*	0.997 0.998 0.989 0.997 0.998 0.499 0.996 0.997 0.988 0.996 0.997 0.998	0.045 0.997 0.948 0.993 0.998 0.487 0.994 0.998 0.994 0.998 0.994 0.998	0.445 0.497 0.448 0.454 0.494 0.448 0.443 0.497 0.497 0.487 0.497 0.445	0.979 0.487 0.481 0.980 0.984 0.482 0.985 0.981 0.482 0.983 0.989 0.993	0.941 0.944 0.944 0.944 0.943 0.943 0.943 0.943 0.943 0.943 0.943 0.943 0.943	0.465 0.941 0.443 0.461 0.984 0.442 0.973 0.983 0.489 0.981 0.984 0.945	0.484 0.989 0.477 0.484 0.479 0.485 0.479 0.485	3.088 0.492 3.982 0.987 3.983 0.987 3.982 0.984	0.440 0.492 0.488 0.042 0.485 0.489 0.490 0.489
20cm ⁻¹	5.639 C.738 0.625 0.651 C.753 C.762 0.653 C.763 0.784 0.625 C.773 C.811 0.535 C.774 C.805 0.435 C.805 0.435 C.805 0.535 0.445 C.805 0.535 0.445 C.805		25.55	2222	0.603 0.870 C.408 0.415 0.874 0.408 0.604 0.872 C.408 0.794 C.885 0.404 0.628 0.689 0.404	20000	0.00 00 00 00 00 00 00 00 00 00 00 00 00	42222	2000	0.976 0.985 C.990 0.981 0.989 0.993 0.980 0.889 C.993 0.981 0.981 0.988	0.483 0.491 0.494 0.492 0.495 0.497 0.492 0.496 0.497 0.492 0.496 0.498	0.987 0.993 C.995 C.988 0.994 C.998 C.989 0.994 C.998 C.989 0.994 C.998	0.491 0.495 0.497 0.493 0.496 0.946 0.495 0.991 0.498 0.595 0.998 0.998	0.445 0.447 0.959 0.445 0.447 0.998 0.496 0.998 0.998 0.494 0.497 0.998	0.945 0.947 C.998 0.991 0.995 C.996 0.990 0.994 C.996 0.990 0.994 C.996	0.990 0.444 0.994 0.988 0.993 0.945 0.987 0.493 0.993 0.983 0.440 0.493 0.983 0.940 0.492	0.980 0.986 C.992 0.927 0.986 C.990 0.980 0.987 C.492 0.978 0.987 C.491	0.934 0.983 0.993 0.939 0.983 0.993 0.934 0.948 0.990 0.934 0.935 0.990	0.910 0.916 0.469 0.916 0.919 0.472 0.912 0.970 0.973 0.912 0.915 0.973	0.947 0.940 C.944 0.944 0.947 0.975 0.935 0.958 0.976 0.942 0.963 0.974	0.450 0.964 0.978 0.445 0.982 0.974 0.921 0.950 0.945 0.940 0.962 0.945 0.965 0.977 0.994	0.624	0.935 0.459 0.971 0.917 0.947 0.942 0.924 0.931 0.936 0.926 0.931 0.946	00.00
GED OVER	0.200 0.330 0.210 2.890 0.532 0.230 0.893 0.230 0.893 0.230 0.893 0.270 0.893 0.270 0.893 0.270 0.893 0.270 0.893 0.270 0.893 0.270 0.893	0.164 0.319	0.178 0.352 0.158 0.313 0.207 0.439 0.315 0.485		0.502 0.616 0.522 0.615 0.489 0.613 0.485 0.621	0.520	0.533 0.677 0.544 0.101 0.545 5.713 0.547 0.673	0.115 C.405 0.115 C.405 0.117 C.405 0.117 C.405	0.411 0.476	0.419 0.44	0.545 0.463 0.585 0.463 0.585 0.475 0.465 0.475	0.55 0.45 0.45 0.45 0.45 0.45 0.45 0.45	0.453 0.476 0.489 0.971 0.483 0.442 0.976 0.985 0.991 0.979 0.988 0.991	0.976 0.987 0.992 0.976 0.987 0.992 0.980 0.986 0.993 0.975 0.986 0.993	0.917 0.967 0.995 0.965 9.579 0.986 0.585 0.976 0.986 0.904 0.578 0.986 0.963 0.978 0.986	0.45+ 0.476 0.985 0.45+ 0.974 0.985 0.45+ 0.973 0.961 0.43 0.465 0.976 0.435 0.960 0.972	0.413 0.458 0.471 0.523 0.457 0.944 0.432 0.438 0.410 0.432 0.453 0.410	0.944 0.566 0.974 0.931 0.937 0.970 0.925 0.936 0.910 0.937 0.948 0.964 0.934 0.907 0.994	0.169 0.867 0.901 0.606 0.874 0.909 0.630 0.903 0.931 0.629 0.869 0.921 0.653 0.904 0.932	0.824 0.413 0.453 0.824 0.844 0.923 0.734 0.844 0.905 0.823 0.845 0.918 0.942 0.845 0.928	0.814 C.90C 0.924 0.817 C.881 0.915 0.707 C.817 0.816 0.870 0.882 0.916 0.844 0.426 0.948			
AVERAGED	7240.0 7240.0 7270.0 7270.0 7270.0 7270.0 7270.0 7270.0	77777	77777	7,777	75000	7550	76500	760.0	77.00.00	7760.	777	7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	79720	7400	2000 2000 2000 2000 2000 2000 2000	60000 60000 610000	12220	2002	2200 2200 2200 2200 2200 2200 2200 220	8250.c 6280.c 6280.c	99999	7350. 6370. 7100.	14444	10000
0 003 0,002 3,001	0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001 0001	0.494 1.000 1.000 0.494 1.000 1.000 0.494 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 0.444 1.000 1.000 0.944 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 0.499 1.000 1.000 0.999 1.000 1.000	0.999 1.000 1.000 0.999 1.000 1.000 1.000 0.999 1.000 1.000 0.000 0.999 1.000 1.000 1.000	0.999 1.000 1.000 0.999 1.000 1.000 0.999 0.999 1.000 0.999 0.999 1.000	0.999 1.000 1.000 0.994 0.999 1.000 0.994 1.000 1.000 0.999 1.000 1.000 0.999 0.999 1.000	0.446 0.449 1.000 0.446 0.449 1.000 0.444 0.948 1.000 0.944 0.949 1.000 0.948 0.949 0.499	0.998 0.999 0.999 0.999 0.999 1.000 0.999 0.999 1.000 0.999 0.999 1.000	0.444 1.000 1.000 0.444 1.000 1.000 0.444 0.404 1.000 0.444 0.404 0.000	0.444 1.600 1.660 0.449 0.409 1.000 0.449 0.409 1.600 0.449 0.409 1.600	0.444 1.000 1.000 0.444 1.000 1.000 0.444 0.934 1.000 0.444 0.934 1.000	0.449 1.000 1.000 0.449 0.449 1.000 0.449 0.449 1.000 0.445 0.449 1.000	0.447	0.947 0.448 0.996 0.948 0.995 0.992 0.995 0.992	0.490 0.447	0.443 0.443 0.485 0.443 0.492 0.443 0.493 0.443	0.441 0.405 0.441 0.445 0.447 0.448 0.445 0.447 0.448 0.445 0.446 0.447	0.44, 0.407 0.44 0.44, 0.497 0.497 0.493 0.44, 0.597 0.493 0.44, 0.597	#####		0.962 0.983 0.983 0.962 0.984 0.982 0.982 0.984 0.993 0.984 9.981 0.993		0.444 0.481 0.487 0.481 0.484 0.491 0.484 0.491 0.484 0.444 0.478 0.484
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FREG. 50.00 20.00 10.00	100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.414 6.485		0.441 0.74 0.712 0.613 0.712 0.613 0.641 0.77 0.641 0.71	0.462 0.773 0.550 0.755 0.574 0.775 0.531 0.671	0.22 0.25 0.22 0.25 0.23 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25	C-177 0-245 C-172 0-240 C-122 0-262 C-123 0-264	0.72 C.172	6.14 6.14 6.15 6.24 6.15 6.24 6.17 6.34	25653	0.27 C-121 0.635 C-348 0.635 0.134 0.665 0.184	0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25	0.115 0.22 0.125 0.23 0.225 0.23 0.225 0.23	2222	0.445 0.470 0.564 0.654 0.601 0.735 0.644 0.782	0.7% 0.918 0.7% 0.8% 0.7% 0.8% 0.8% 0.8%	0.022 0.03 0.041 0.041 0.033 0.034 0.035 0.034	0.022 0.032	0.459 0.459	0.48 0.480 0.483 0.484 0.483 0.484 0.483 0.484		0.483 C.484 0.478 C.484 0.478 G.484 0.488 G.484	0.914 0.914 0.914 0.914 0.914 0.914 0.914	

WATER VAPOR AT 0.01 ATMOSPHERE PRESSURE

		100'0	*****	*****	22022	15151	11555	15123	26332				#8888 #11111	88888	88888	88888	88888		88888	200000	88888	88688	99444				
		0.005 0.002	0.677 0.432 0.644 0.417 0.800 0.888 0.614 0.847		0.574 0.401 0.414 0.414 0.417 0.417	0.359 0.542 0.392 0.581 0.353 0.533 0.347 0.530	0.345 0.200 0.200 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000		C. C	00150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 01150 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 0100 010	0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15			88888	88888	88888	0001		000 1.000 000 1.000 000 1.000	1.000 1.896 1.000 1.696 1.000 1.006 1.000 1.006	000 1.000 000 1.000 000 1.000	000 1.000 1.000 1.000 0.000 1.000 0.000 1.000 0.000 1.000				0.995 C.997 0.996 C.999 0.996 C.999	
		0.030 0.010	0.72	0.335	11111	2222									2222	88888	22000				88888						
		0.050	0.543 0.715 0.482 0.457 0.414 0.605 0.414 0.605		20000	0.024 0.034 0.024 0.026 0.020 0.020 0.020 0.020	2000 0 0000 0000 0 0000 0000 0 0000	0.103 0.297 0.103 0.297 0.130 0.328 0.084 0.221	0.017 6.191 0.017 6.191 0.013 0.081	0.027 0.137 0.036 0.155 0.046 0.174 0.045 0.210	222	0.672 6.74 0.727 6.88 6.801 6.89 6.801 6.89					******				*****	0.999 0.999		0.912 0.91 0.912 0.912 0.912 0.914 0.912 0.914			5250 5250 5250 5250 5250 5250 5250 5250
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	010'0 828'9 050'0	0.776 6.843 0.401 6.737 6.843 0.811 6.725 6.837 0.881 6.725 6.837 0.881 6.645 6.739 0.80	0.644 6.744 0.815 0.724 6.621 0.437 0.634 6.744 6.417 0.637 6.653 6.455			0.076 0.925 0.451 0.073 0.522 0.546 0.074 0.921 0.447 0.062 0.914 0.941		0.072 0.920 0.076 6.524 0.089 0.931 0.089 0.933																100 Carl Carl Carl Carl Carl Carl Carl Carl	
	UPPLCAL 0,500 0,300 0,100	0.170 C.963 R.403 0.711 C.722 R.405 0.724 C.406 C.410 0.724 C.406 C.410 0.724 C.414 C.414 0.126 C.725 C.414 C.414 0.126 C.726 C.414 C.414 0.126 C.726 C.414 C.414 0.126 C.726 C.414 C.414 0.114 C.726 C.414	33533	C.132 C.523 C.644 C.255 C.437 C.546 C.412 C.533 C.667 C.563 C.667 C.566 C.376 C.566 C.662	0.340 0.341 0.840 0.351 0.334 0.654 0.324 0.334 0.655 0.316 0.337 0.652 0.467 0.621 0.311	0.454 0.732 0.823 0.431 0.734 0.823 0.634 0.734 0.825 0.735 0.734 0.884 0.552 0.734 0.884	C.243 C.787 9.785 C.627 C.235 B.423 C.687 C.793 3.647 C.744 C.642 C.89C	0-425 6-736 0-818 0-435 6-736 0-82 0-432 6-894 0-842 0-431 6-874 0-841	C-33 C-39 C-39 0.74 C-30 C-31 C-63 C-37 C-74 C-63 C-32 0-34 C-62 C-38 6-34									C.536 C.541 C.545 C.575 C.541 C.545 C.575 C.544 C.545 C.577 C.544 C.545 C.577 C.544 C.545	0.942 0.991 0.995 0.974 0.997 0.993 0.974 0.996 0.993 0.952 0.978 0.984	0.419 0.962 0.986 0.416 0.906 0.417 0.411 0.904 0.413 0.413 0.994 0.473	1947 RAT 1647 1747 RAT 1747 1747 RAT 1747 17	C.001 C.011 C.014 C.001 C.011 C.014 C.007 C.011 C.014 C.007 C.011 C.014 C.007 C.011 C.014	C.001 C.001 C.001 C.003 C.001 C.011 C.003 C.001 C.001 C.003 C.001 C.001	6,943 6,945 6,944 6,670 6,945 6,945 6,674 6,946 6,935 6,671 6,987 6,943	C.876 C.924 C.931 C.877 C.924 C.931 C.856 C.915 C.944 C.868 C.918 C.944
L- 00		670 600 600 600 600 600 600 600 600 600	0.012 C.CM 9.137 0.417 C.C33 8.137 0.612 C.C33 8.134 0.415 C.C33 9.134 0.415 C.C43 9.134	¥3553	0.021 C.107 0.222 0.020 C.102 0.214 0.022 C.100 0.201 0.031 C.127 0.236 0.002 C.216 0.346	33533	C.10¢ C.277 0.436 C.135 C.231 0.502 C.276 C.441 0.577 C.276 C.497 0.636 C.172 C.342 0.522	C.235 C.432 C.535 C.235 C.432 C.533 C.225 C.437 C.537 C.221 C.402 C.537 C.304 C.406 C.637	C.302 C.203 C.603 C.513 C.621 C.722 C.523 C.731 C.624 C.523 C.731 C.623 C.523 C.731 C.623	C.715 C.144 B.897 C.772 C.174 B.815 C.037 C.170 B.815 C.052 C.170 B.815 C.175 C.784 B.878	C.514 C.514 C.573 C.504 C.544 C.573 C.505 C.514 C.544 C.605 C.514 C.544 C.615 C.517 C.544	0.976 6.544 0.591 0.976 6.544 0.592 0.971 6.544 0.593 0.971 6.544 0.593	C.112 C.100 0.500 C.135 C.655 0.520 C.136 C.577 0.500 C.154 C.575 0.500	C.914 C.581 0.587 0.982 C.592 0.597 0.983 C.593 0.597 0.985 C.594 0.597	C.916 C.595 C.597 C.916 C.595 C.597 C.915 C.597 C.598 C.912 C.597 C.598 C.912 C.597 C.598	0.944 0.597 0.594 0.944 0.579 0.987 0.945 0.578 0.596 0.941 0.584 0.591	0.435 6.437 0.588 6.431 6.536 0.593 6.423 6.439 6.545 6.422 6.446 8.577	6.423 6.46 6.53 6.402 6.44 6.65 6.402 6.44 6.65 6.401 6.42 6.44 6.401 6.42 6.44	0.114 6.52 0.578 0.00 0.536 0.539 0.00 0.536 0.535 0.10 0.535 0.537 0.738 0.644 0.518	11813	<b>3333</b> 3		333 <b>5</b> 3	C.631 C.742 C.834 C.631 C.841 C.837 C.644 C.734 C.734 C.394 C.716 C.134 C.394 C.716 C.134	6.634 C.734 6.624 C.637 C.734 6.624 C.537 C.732 6.734 C.595 C.723 0.685 C.667 C.794 6.653
	AVEKAGED OVEK	33 33 33 33 33 33 33 33 33 33 33 33 33					35555						7840.0 0.772 C.845 6.558 7870.0 0.772 C.845 6.508 7870.0 0.777 C.845 6.572 7870.0 0.744 C.874 7.572			500 CH2		500 COS		33535		55555			MARGO G.188 G.317 D.317 MARGO G.184 G.312 G.328 MARGO G.185 G.328 G.328 MARGO G.236 G.341 MARGO G.276 G.341 MARGO G.276 G.341 MARGO G.276 G.341
PRESSURE	100.0 200.0 200.0	00000000000000000000000000000000000000	2000	1.000 1.000 0.000 0.000 1.000 0.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	200000	90050	8	0.649 C.949 1.000 C.949 C.944 1.000 0.440 1.000 1.000 0.949 1.000 1.000 0.448 C.644 1.000	*****	*****		*****		35555	#####			25335	0.462 C.463 C.593 C.471 C.486 C.593 C.473 C.496 C.595 C.473 C.486 C.595 O.415 C.486 C.593		0.949 C.486 C.493 0.977 C.486 C.493 0.977 C.485 C.493 0.977 C.481 C.493		0.491 0.419 0.484 0.404 0.493 0.474 0.486 0.442 0.489 0.414 0.44 0.475 0.474 0.461 0.478	C.914 C.93 C.574 C.914 C.934 C.508 C.914 C.934 C.572 C.914 C.944 C.580 C.914 C.944 C.583	0.872 C.934 C.643 0.617 C.848 C.600 0.673 C.838 C.600 0.678 C.831 C.870 0.793 C.873 C.914
ATMOSPHERE PR	0.050 0.020 0.010	10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00	5555	*****							*****	*****	0.447 D.445 D.447 0.447 D.444 C.447 0.446 D.544 C.447 0.460 D.711 G.447 0.485 D.711 G.445	*****	0.93 0.516 0.680 0.930 0.937 0.488 0.939 0.581 0.490 0.928 0.628 0.438	0,452 C.415 G.586 0,926 D.458 C.476 0,401 D.414 C.471 0,405 C.416 D.501	0.913 0.93 0.912 0.017 0.014 0.0 0.911 0.933 0.972 0.950 0.973 0.984	0.873 0.920 C.546 0.772 0.855 0.402 0.719 0.621 0.979 0.819 0.402 0.938	0.872 0.837 0.933 0.872 0.524 0.452 0.893 0.937 0.663 0.876 0.931 0.958 0.854 0.912 0.546	0.851 0.918 0.948 0.853 0.913 0.945 0.510 0.927 0.955 0.640 0.922 0.959	0.871 0.936 3.945 0.871 0.937 3.959 0.876 0.937 0.930 0.829 0.907 0.944 0.857 0.929 0.980		0.404 C.884 C.424 0.484 C.744 C.840 0.612 D.744 O.825 0.643 G.604 C.848 0.732 C.835 C.848	0.687 0.803 C.867 C.864 C.737 C.853 D.710 O.813 C.874 O.742 C.843 C.896 O.821 C.781 C.839	0.539 0.705 0.801 0.237 0.481 0.611 0.234 0.427 0.611 0.416 0.612 0.713
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₽¥	5 000 2,000 1,000			6-714 C-524 0-470 6-714 C-623 0-675 6-714 C-623 0-675 6-644 C-574 0-555 6-644 C-574 0-555	35555	2222	C.714 C.637 O.694 C.637 C.765 O.655 C.527 C.765 O.601 C.581 C.116 O.611 C.484 C.665 O.677	35333	53555	C.387 C.331 C.481 C.427 C.426 C.345 C.444 C.475 C.386 C.532 C.703 D.604 C.532 C.703 D.604	C. 341 C. 712 C. 724 C. 802 C. 743 C. 447 C. 512 C. 743 G. 913 C. 522 C. 445 G. 793 G. 564 C. 727 G. 813		C.674 C.702 0.470 C.684 C.615 0.480 C.701 C.624 0.681 C.701 C.705 C.682		6.17 C.16C 0.C% C.31 C.71 C.65 0.32 C.51 0.23 C.34 C.71 C.72	C. 201 C. 100 C. 22 C. 201 C. 201 C. 52 C. 191 C. 201 C. 50 C. 201 C. 201 C. 201 C. 50 C. 201 C. 201	6.239 C.448 0.381 C.143 C.324 0.452 C.263 C.435 0.568 C.402 C.594 0.228				C.125 C.789 C.29 C.125 C.789 C.29 C.106 C.233 C.394 C.043 C.164 D.706 C.041 C.764 C.356	0.054 6.184 0.312 0.056 6.184 0.332 0.057 6.183 0.333 0.054 6.183 0.253	0.037 C.134 0.244 C.015 C.073 0.157 C.007 C.034 0.071 C.018 C.044 0.173	0,001 C.C.1 0.127 0,001 C.C.2 0.127 C.001 C.C.4 0.144 C.001 C.C.2 0.174 C.001 C.C.1 0.004	000 0000 0000 0000 0000 0000 0000 0000 0000
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WATER VAPOR AT 0.20 ATMOSPHERE PRESSURE

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ΑŢ	000 1 000 1	33333	35333	C.83 C.243 C.524 0.403 C.872 0.504 C.642 C.512 0.534 C.973 C.519 0.543 C.463 C.515 C.514	C.455 C.423 D.482 C.851 C.402 D.430 G.84C C.893 D.430 C.43C C.450 D.433 C.43C C.452 D.433	33355	C.476 C.515 C.546 C.476 C.517 C.546 C.617 C.517 C.646 C.614 C.559 C.618	55555	33355	33333	C.34 C.32 C.45 C.30 C.43 C.45 C.30 C.43 C.43 C.31 C.43 C.43 C.31 C.43 C.43	33533	15555	55353	C.722 C.622 C.634 C.727 C.673 C.614 C.722 C.622 C.634 C.664 C.722 C.624	35555	C.447 C.635 C.748 C.447 C.635 C.748 C.472 C.635 C.748 C.518 C.612 C.778	C.31 C.46 C.38 C.421 C.42 C.65 C.332 C.66 C.347 C.66 C.31 O.647 O.66 C.341 O.647	C.515 C.445 G.226 G.291 C.448 G.558 G.214 C.510 G.486 G.404 C.554 G.455 G.404 C.617 G.455	C. 304 C. 446 O. 614 C. 374 C. 615 O. 718 C. 374 C. 615 O. 721 C. 484 C. 615 O. 726 C. 465 C. 617 O. 726	6.404 6.311 0.414 6.404 6.311 0.414 6.422 6.142 0.422 6.442 6.417 0.113 6.455 6.460 0.442	6.347 6.237 0.638 6.402 6.237 0.648 6.373 6.248 0.642 6.283 6.472 0.599 0.336 6.214 0.634	C.245 C.471 C.143 C.271 C.445 C.349 C.245 C.476 C.384 C.245 C.476 C.394 C.246 C.335 C.434	C.243 C.428 C.340 C.14C C.784 C.415 C.082 C.164 C.329 C.195 C.311 C.435 C.175 C.312 C.435	0.116 6.254 0.304 6.166 6.254 0.304 6.143 6.306 0.432 0.156 6.318 0.434 6.635 6.314 0.301	C.021 C.1C4 0.214 C.021 C.C67 0.149 C.022 C.C12 0.C68 C.025 C.C13 0.241
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-200° K	UPR CM.) 0 506 0 200 0 100	0.981 0.985 0.987 0.981 0.985 0.987 0.987 0.982 0.984 0.987 0.982		0.474 0.484 0.484 0.484 0.484 0.484 0.484 0.482 0.482 0.482 0.482	0.474 0.494 0.494 0.474 0.494 0.494 0.471 0.484 0.484 0.471 0.485 0.494 0.487 0.483 0.494	0.988 0.983 0.985 0.978 0.984 0.945 0.949 0.981 0.987 0.949 0.981 0.987		0.978 0.988 0.992 0.978 0.989 0.989 0.988 0.975 0.989 0.980 0.976 0.989 0.973 0.984 0.990	*****	*****	0.924 0.957 0.973 0.954 0.959 0.978 0.954 0.873 0.982 0.939 0.974 0.984		0.446 0.481 0.487 0.446 0.480 0.484 0.471 0.482 0.484 0.444 0.481 0.487					1777			0.894 0.931 0.932 0.893 0.924 0.949 0.894 0.910 0.931 0.894 0.914 0.934	7777	6.63% 6.64% 6.43% 0.63% 6.64% 6.43% 0.84% 6.86% 6.72% 0.78% 6.66% 6.60% 0.78% 6.86% 6.90%		::::::	0.423 8.748 0.817 0.533 8.472 0.734 0.436 8.594 0.497 0.400 8.594 0.873 0.564 0.707 0.781
Ė	5 000 2 000 1 000	22222		35555	*****	0.958 0.914 0.482 0.957 0.914 0.982 0.929 0.935 0.988 0.904 0.918 0.957 0.902 0.937 0.935	*****	0.422 0.452 0.467 0.467 0.467 0.454 0.413 0.417 0.412 0.412 0.412 0.412 0.413 0.413 0.413	22225		****	25555	0.812 0.413 0.413 0.884 0.424 0.414 0.934 0.440 0.458 0.894 0.414 0.415 0.898 0.415 0.415	11711	*****		11511		66666	22252		0.620 0.741 0.811 0.647 0.778 0.839 0.648 0.780 0.390 0.567 0.720 0.794 0.422 0.744 0.813	21135	11555		
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WATER VAPOR AT 0.02 ATMOSPHERE PRESSURE T-200°K

	AVERAGED OVER 20cm-1	FAEG. 30,00 70,00 10,00 5,000 2,000 1,000 0,500 0,700 0,100 0,059 0,020 0,010 0,005 0,001 0,001																
T=200° K	Cw.]	FREQ. 59.00 20.00 10.00 3.000 2.000 1.000 0.300 0.300 0.300 0.00 0.000 0.000 0.000 0.000 0.000	100 100 100 100 100 100 100 100 100 100		1.822 Oct 0.840	0001 0001 0001 0000 0000 0000 0000 000												•
	(NOTAM)	FATCA. 30.00 20.00 10.00 5,000 7,000 1,000 0,300 0,200 0,100 0,030 0,020 0,010 0,003 0,003 0,001	6.71 CATO CATO CATO CATO CATO CATO CATO CATO							100 CH 10			0001 0001 0001 0001 0001 0001 0001 000		001 001 001 001 001 001 001 001 001 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 000 00		0.410 0.410 0.440 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410 0.410	

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	AVERAGED OVER	3510.0 0.054 6.184 0.337 3520.0 0.054 6.185 0.288 3590.0 0.058 6.115 0.289 3590.0 0.018 6.012 0.225	3560.0 6.001 0.013 0.031 3570.0 0.001 0.019 0.033 3580.0 0.000 0.018 0.044 3590.0 0.000 0.000 0.031 3600.0 0.000 0.002 0.013	3410.0 0.000 0.001 0.024 3420.0 0.000 0.002 0.016 3430.0 0.000 0.001 0.009 3440.0 0.000 0.002 0.028						3910-0 0-001 0-012 0-052 3910-0 0-005 0-051 0-133 3910-0 0-005 0-040 0-140 3910-0 0-018 0-093 3950-0 0-032 0-149 0-288	390.0 0.102 C.314 0.422 370.0 0.114 C.344 0.431 390.0 0.211 C.426 0.543 340.0 0.212 C.350 0.455 4500.0 0.441 C.452 0.452	4010-0 0-525 G-711 0-807 4030-0 0-811 G-182 0-867 4030-0 0-857 G-281 0-890 4040-0 0-314 G-845 0-937	4060.0 0.813 C.813 0.95 4010.0 0.821 0.95 4080.0 0.822 C.93 0.947 4080.0 0.810 C.842 0.947 4100.0 0.886 C.952 0.916	4130-9 0.871 C.544 0.972 4120-0 0.859 C.514 0.942 4130-0 0.871 C.94C 0.942 4140-0 0.870 C.952 0.975 4150-0 0.896 C.952 0.975	0.405 C.400 0.460 0.415 C.465 0.463 0.419 C.466 0.463 0.419 C.446 0.463	0.432 0.473 0.984 0.432 0.472 0.984 0.444 0.473 0.484 0.444 0.474 0.490	0.531 C.983 0.992 0.534 C.985 0.993 0.542 0.987 0.994 0.942 0.985 0.994	0.948 C.991 0.497 0.970 C.992 0.998 0.971 C.992 0.998 0.973 C.993 0.998	0.415 C.493 0.494 0.475 C.493 0.494 0.924 0.493 0.494 0.424 C.492 0.493	4410.0 0.472 C.480 0.485 4420.0 0.471 0.489 0.484 4430.0 0.480 0.482 0.482 4440.0 0.482 0.483 0.482 4440.0 0.485 0.483 0.481	4460.0 0.494 C.918 0.984 4470.0 0.890 0.845 0.978 4480.0 0.912 0.949 0.949 4300.0 0.882 C.933 0.954	60000	4360.0 0.746 C.872 0.906 4570.0 0.843 0.845 0.925 4590.0 0.835 0.845 0.925 4590.0 0.855 0.909 0.934 4660.0 0.473 0.422 0.944	4410.0 0.433 0.494 0.927 4420.0 0.472 0.785 0.827 4450.0 0.516 0.782 0.774 4450.0 0.516 0.804 0.834	4640.0 0.753 C.827 0.479 4470.0 0.413 C.444 0.465 4840.0 0.481 2.427 0.444 4700.0 0.714 0.775 0.444	200 000 000 000 000 000 000 000 000 000
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ATMOSPHERE PRESSURE	0 050 0 050 0.010	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	86668	900.1	88888	86666	1.000	99999	0.999 1.000 1.000 0.999 1.000 1.000 0.999 1.000 1.000 0.999 0.999 1.000		0.44 0.44 0.44 0.41 0.44 0.44 0.44 0.44 0.44 0.44 0.44 1.00		0.946 0.448 0.944 0.444 0.944 0.944 0.442 0.949 0.444 0.942 0.949 0.949	0.999 0.499 1.000 0.998 0.499 0.999 0.998 0.999 0.999 0.998 0.999 0.999	0.001 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.412 0.441 0.444 0.400 0.404 0.414 0.400 0.404 0.414 0.404 0.404 0.417	0.411 0.441 0.411 0.414 0.414 0.411 0.417 0.414 0.414 0.415 0.414 0.414	0,477 0,465 0,440 0,473 0,481 0,489 0,438 0,486 0,483 0,459 0,475 0,483	0.944 0.945 0.975 0.946 0.912 0.916 0.956 0.972 0.981 0.971 0.986 0.998		0.954 0.911 0.900 0.945 0.912 0.933 0.954 0.971 0.900 0.971 0.982 0.987 0.967 0.987 0.986	*****	0.913 0.988 0.988 0.989 0.988 0.993 0.983 0.989 0.993 0.978 0.989 0.991		0.978 0.987 0.991 0.974 0.984 0.989 0.945 0.978 0.995 0.994 0.971 0.982 0.998 0.974 0.982	0.441 0.917 0.984 0.481 0.477 0.131 0.494 0.977 0.624 0.495 0.946 0.824 0.495 0.446
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WATER VAPOR AT 0.01 ATMOSPHERE PRESSURE

## APPENDIX D

WATER VAPOR TRANSMISSIONS AVERAGED OVER 50 cm⁻¹
WITH ENTRIES EVERY 25 cm⁻¹ FOR FREQUENCIES FROM

1000 cm⁻¹ TO 10,000 cm⁻¹ AT 300°K, 250°K, AND 200°K

PRESSURE	
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OVER 50cm⁻¹

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-	ER 50cm ⁻¹	5.000 2.000 1.000	2 C.601 G.756 C.823 5 C.607 G.732 G.823 7 C.879 G.814 C.736 7 C.461 G.616 G.734	0.534 0.634 0.618 0.739 0.623 0.745 0.610 0.743	9.55	0.658 C.409 0.874 0.914 0.936 0.941 0.956 0.951	40444	0.043 0.005 0.043 0.005 0.005 0.007 0.003 0.005	0.046 0.045 C.406 0.048 0.043 C.944 0.048 0.091 C.944 0.089 0.089 0.907	0.920 0.988 0.957 0.988 0.957 0.973 0.955 0.963	20000	0.935 0.959 0.935 0.959 0.902 0.902 0.912 0.903	0.045 0.005				5 0.42k 0.453 0.48k 1 0.459 0.462 0.48k 1 0.455 0.472 0.48k 2 0.456 0.48k 0.48k 1 0.447 0.48k			000000000000000000000000000000000000000	20060	5.995 5.989 0.982 6.989 0.983 5.989 0.983 6.989		0.973 0.984 0.989 0.972 0.983 0.989 0.980 0.988 0.992			
	ERAGED OVE	FREQ. 30.00 20.00 10.00		0.133 0.282 0.207 0.376 0.216 0.384 0.375 0.360	5.0 0.497 C.643 C.728 C.0 0.495 C.679 C.728 5.0 0.531 C.670 C.753 C.0 0.545 D.686 C.708 5.0 0.546 G.705 C.765		0.625 C.533 0.923 C.932 0.933 C.972 0.955 C.972		0.55 C.976 0.93 C.936 0.93 C.956 0.635 C.956	#150.0 0.931 0.957 0.970 #150.0 0.930 0.956 0.970 #250.0 0.est 0.912 0.938 #225.0 0.est 0.ete 0.935	0.653 0.005 0.631 0.695 0.781 0.652 0.750 0.629	0.784 C.856 0.807 0.873 0.824 0.884 0.824 0.885 0.809 C.875	0.632 0.691 0.633 0.690 0.630 0.660 0.786 0.661	0.772 C.e5 0.756 C.e55 0.724 C.e15 0.740 0.635	0.44 0.756 0.47 0.635 0.575 0.692 0.734 0.620	0.654 C.795 0.694 C.795 0.725 C.625 0.759 0.842	5.0 0.772 C.#51 0.#93 0.0 0.412 0.678 C.915 5.0 0.655 0.908 C.935 0.0 0.691 0.912 0.959 5.0 0.891 0.931 d.952	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910 0.910	0.687 6.992	0.982 0.982 0.982 0.989 0.978 0.988	0.0 G.945 C.928 C.985 S.C C.942 C.944 D.975 S.D D.944 C.985 G.975 S.D D.984 C.985 G.975		0.0 0.412 C.445 0.961 5.0 0.40# 0.942 0.945 8.0 0.430 0.957 0.977 5.0 0.414 0.987 0.442			
	AVER.	Ē	28282	22222	22222	25222	22222	22425	55555	2222	25555	22222	22222	33325	18282	252	2555	*****	25.55.55	33338	25555	\$2555		****			
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		0.050 0.020 0.010	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000		1.600 1.600 1.600 0.940 1.000 1.600 0.990 0.990 1.000 0.998 0.990 0.999	*****	11000	0.000	0.000	0.000 0.000 0.000 0.000 0.001 0.005 0.000 0.001 0.005 0.000 0.007 0.001	0.450 0.973 0.983 0.950 0.960 0.972 0.936 0.960 0.972 0.928 0.955 0.980	0.013 0.024 0.015 0.037 0.001 0.073 0.018 0.018 0.012 0.010 0.007 0.003	0.036 5.000 0.012 0.036 0.061 0.073 0.057 0.061 0.073 5.051 0.007 0.079 0.038 0.078 0.082	00000	0.092 C.004 D.002 D.003 C.008 C.009 C.003 C.008 C.009 C.403 C.008 D.009	*******	0.450 1.000 1.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0	40000				0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00%			0.472 0.483 0.488 0.078 0.484 0.442 0.482 0.488 0.492 0.477 0.984 0.493	0.948 0.978 0.985 0.983 0.972 0.983 0.935 0.972 0.986 0.932 0.979	0.438 0.463 0.473 0.455 0.460 0.472 0.415 0.405 0.482 0.467 0.416 0.481 0.465 0.438 0.454
T=300° K	UPR.CM1	0,500 0,200 0100	030*1 000*1 046*0	00000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	00700	00000	0.978 0.984 0.190 0.934 0.995 0.993 0.976 0.985 0.993 0.976 0.985 0.991	0.027 0.028 0.023 0.04C 0.028 0.007 0.05C 0.087 0.007 0.07E 0.087 0.091		0.662 0.911 0.957 0.634 0.693 0.934 0.805 0.835 0.959 0.704 0.836 0.699	55555	55555	25555	0.481 0.483 0.485 0.481 0.442 0.445 0.467 0.493 6.445 0.487 0.492 0.445			0.002 0.002 0.007 0.003 0.007 0.005 0.005 0.007 0.005 0.000 0.003 0.003	0.086 0.003 0.005 0.001 0.000 0.000 0.001 0.000 0.000 0.007 0.000 0.007 0.000	20000	00000	0.015 0.085 0.090 0.015 0.085 0.000 0.016 0.085 0.000 0.018 0.087 0.001	0.419 0.987 0.492 0.464 0.981 0.488 0.459 0.975 0.483 0.454 0.972 0.483	0.451 0.450 0.479 0.451 0.454 0.476 0.451 0.471 0.480 0.450 0.474 0.470 0.402 0.438 0.454	0.000 0.015 0.980 0.020 0.050 0.060 0.032 0.050 0.071 0.025 0.055 0.087 0.000 0.042	0.877 0.931 0.931 0.877 0.927 0.934 0.836 0.909 0.933 0.830 0.903 0.931 0.839 0.838 0.931	0.801 0.817 0.413 0.801 0.871 0.907 0.742 0.879 0.817 0.634 0.751 0.818 0.727 0.815 0.865
<u> 11</u>		5,000 2,000 1,606	0.085 0.085 0.095 0.001 0.005 0.007 0.004 0.000 0.008 0.005 0.007 0.008 0.005 0.007	00000	20000	*****	20000	25555	12221	0.000	0.018 0.739 0.809 0.556 0.602 0.73 0.402 0.607 0.73 0.445 0.607 0.708	2222		14150	0.914 0.945 0.981 0.946 0.973 0.981 0.957 0.977 0.982 0.955 0.977 0.983 0.905 0.978 0.985	25255	0.986 0.993 0.995 0.989 0.993 0.998 0.985 0.991 0.998 0.975 0.987 0.989	25553	20000	0.000	40000	11555	46556	15000		0.655 0.768 C.617 0.652 0.765 D.679 0.616 C.731 C.855 0.507 C.721 C.755	66666
i		FREG. 50.00 20,00 10.00	1150-0 0.021 0.001 0.001 7075-0 0.5% (* 675 E.996 1725-0 0.005 E.5E E.990 4235-0 0.005 E.5E E.993	00000	0.417 C-927 0.411 C-947 0.411 C-947 0.411 C-947		0.412 C.61 0.412 C.61 0.423 C.632 0.423 C.663	C-631 C-623 C-631 C-623 C-731 C-623 C-731 C-623 C-731 C-623 C-731 C-623 C-731 C-623	0-675 0-667 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 0-794 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		0 003 0.002 0.001	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	22444						20000			86888	98888	25000	55555	20000	0.404 0.404 0.404 0.404 0.404 0.404 0.404 0.404 0.404	0.475 0.497 0.498 0.471 0.498 0.448 0.488 0.491 0.447 0.488 0.493 0.498	2,405 G.407 G.948 5,405 G.401 G.949 5,000 G.404 G.994 5,000 G.405 G.902	0.400 0.400 0.400 0.400 0.400 0.400 0.400 0.400 0.400 0.401 0.400 0.400					*****	**************************************
		0.050 0.020 0.010	1.000 1.000 1.000 1.000 1.000 1.000 0.999 0.000 1.000 0.999 0.999 1.000	00000		00.000	22.22	2222	55555	55555	11221		00000	30000	90000	20110	2222		2222	20000	*****			1111			*****
	UPR,CA.!	0,500 0,200 0,100	D.448 D.994 1.0CC C.448 D.994 C.440 C.497 C.998 D.944 D.996 C.498 C.948	0,991 0,995 0,096 0,082 0,985 0,995 0,982 0,986 0,995 0,977 0,986 0,995 0,950 0,978 0,963	0.920 0.900 0.905 0.921 0.950 0.905 0.983 0.920 0.900 0.830 0.899 0.929 0.707 0.800 0.889	0.700 0.803 0.655 0.700 0.89 0.655 0.655 0.747 0.817 0.551 0.604 0.773	0.400 0.500 0.664 0.665 0.765 0.626 0.734 0.823 0.671 0.608 0.730 0.671	0.4079 0.623 0.7(3 0.405 0.554 0.454 0.402 0.406 0.700 0.347 0.475 0.753 0.418 0.773 0.607	0.562 0.896 0.775 0.831 0.788 0.815 0.819 0.785 0.644 0.713 0.807 0.859 0.815 0.877 0.051	0.624 0.689 0.921 0.632 0.640 0.622 0.634 0.910 0.92 0.639 0.932 0.951	0.421 0.450 0.463 0.912 0.457 0.463 0.911 0.412 0.463 0.451 0.410 0.019 0.451 0.471 0.080	0.040 0.775 0.082 0.074 0.085 0.080 0.087 0.087 0.002 0.082 0.484 0.402	0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00%	0.446 0.444 1.050 0.406 0.908 0.408 0.908 0.908 0.444 0.908 0.908 0.644	0.440 1.000 1.000 0.440 0.940 1.000 0.440 0.940 0.940 0.447 0.940 0.940	0.445 0.447 0.444 0.455 0.447 0.444 0.481 0.441 0.444 0.481 0.445 0.444	C.440 C.991 C.412 D.984 D.997 D.605 C.986 C.992 C.465 C.987 G.933 D.695 D.985 D.992 C.405	0.04C 0.48 0.487 0.474 0.094 0.085 0.047 0.460 0.464 0.066 0.481 0.482	0.912 0.914 0.974 0.915 0.919 0.911 0.919 0.918 0.513 0.815 0.920 0.913 0.887 0.927 0.914	0.000 0.001 0.075 0.000 0.000 0.070 0.000 0.000 0.050	6.889 0.931 0.951 0.889 0.039 0.950 0.912 0.914 0.861 0.904 0.939 0.857 0.905 0.937 0.935	0.836 0.931 0.031 0.936 0.903 0.931 0.936 0.836 0.939 0.737 0.836 0.847	0.444 0.738 0.854 0.427 0.743 0.811 0.512 0.811 0.735 0.513 0.811 0.747	0.505 0.851 0.719 0.110 0.514 0.687 0.187 0.514 0.625 0.187 0.115 0.620	0.35.3 0.46.3 0.730 0.421 0.75. 0.836 0.475 0.45. 0.737 0.401 0.510 0.477 0.431 3.597 0.664	0.533 0.416 0.765 0.437 0.756 0.025 0.714 0.607 0.060 0.779 0.864 0.402 0.657 0.607 0.734	0.454 0.45 0.46 0.454 0.473 0.36 0.484 0.974 0.49 0.444 0.974 0.49 0.445 0.944
		5,000 2,000 1,000	0.00% 0.00% 0.99% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00%	20000	0.834 0.603 0.923 0.771 0.818 0.800 0.682 0.782 0.839 0.573 0.703 0.777 0.130 0.567 0.484	0.10 0.10	0.157 0.212 0.338 0.535 0.557 0.538 0.656	0.237 0.35 0.106 0.253 0.272 0.311 0.314 0.434	13531	0.679 C.786 0.780 C.837 C.400 C.837	86254 33333	6.93 C.935 6.93 C.935 6.93 C.935 6.93 C.935	2000 2000 2000 2000 2000 2000 2000 200	0.00 C.000 0.00 C.000 0.00 C.000 0.00 C.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.489 C.992 C.988 C.992 C.984 C.974 C.984 C.975	0.017 G.93 G.977 G.93 G.949 G.970 G.949 G.979	600 CONTRACTOR CONTRAC		0.617 0.018 0.834 0.018 0.834 0.083 0.011 0.083	0.739 0.424 0.424 0.424 0.424 0.424 0.424 0.424 0.424	0.25 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27		200 50 50 50 50 50 50 50 50 50 50 50 50 5		13331	
		30,00 20,00 10,00	0.974 0.985 0.985 0.974 0.983 0.988 0.958 0.973 0.985 0.953 0.957 0.970	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.556 C.645 C.773 0.451 C.665 C.699 0.415 O.476 C.587 0.176 O.435 C.458 0.677 O.485 C.458	2000 00 00 00 00 00 00 00 00 00 00 00 00	0.000	000000000000000000000000000000000000000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.25 0.25 0.37 0.25 0.37 0.25 0.37 0.25	10000		0.43 0.055 0.45 0.055 0.45 0.056 0.950 0.056	0.000		0.030 0.433	0.655 C.025 C.955 0.655 C.007 C.935 0.854 C.007 C.035 C.854 C.007 0.034 C.842 C.659 0.028	0.77	0.10 0.10			0.13 0.14 0.15 0.13 0.10 0.13 0.10 0.13 0.10 0.13	\$60000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$6000 \$0000 \$0000 \$0000 \$0000 \$0000 \$0000 \$0000 \$0000 \$0000 \$0000	00000000000000000000000000000000000000	20000	20000	2222
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	UPPLCAL) 0,500 0,700 0,100	2007	0.387 0.580 0.584 0.587 0.584 0.685 0.412 0.584 0.695 0.512 0.657 0.548					0.494 0.494 0.449 0.494 0.444 0.495 0.495 0.481 0.442 0.494 0.417 0.464 0.444	*****	11111			19855					<b>!!!!!</b>			H					
	000 2 000 1.000	0.113 C.224 C.037 C.167 C.029 C.047 C.030 C.114		C.345 C.562 0.370 0.507 0.107 C.623	0.557 0.610 0.731 0.800 0.731 0.800 0.730 0.800	0.945 C.944 C.944 C.944 C.944 C.944	5.485 5.445 5.491 5.445 5.493 5.494 5.692 5.997	0.462 0.083 0.400 0.033 0.033 0.93 0.031 0.035 0.932 0.004 0.936 0.937 0.001 0.936 0.947	77777 77777 77777 77777 77777	0.816 0.875 0.703 0.856 0.736 0.857 0.736 0.810	7222	0.705 C.845 0.707 C.845	0.704 0.746 0.704 0.746 0.727 0.614	200 C C C C C C C C C C C C C C C C C C	0.587 C.758 0.587 C.719 0.587 C.719	0.774 C.856 C.825 C.885 C.825 C.885 C.827 C.885	0.402 C.435 C.437 C.452 C.433 C.452	11111 11111 111111 1111111111111111111			2000					
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	FREQ. 30 00		7425.0 0.000 7425.0 0.000 7435.0 0.000 7475.0 0.000					6055.0 0.138 6055.0 6.728 6055.0 0.728 1100.0 0.458	8175.0 0.000 8200.0 0.028 6225.0 0.228 6250.0 0.239					######################################							9650.0 0.818 9750.0 0.685 9750.0 0.676 9750.0 0.676	9775.0 0.656 9825.0 0.456 9825.0 0.403 9870.0 0.503	9925-0 0.559 9925-0 0.559 9936-0 0.651			
=250° K	1.005 0 002 0 001			55555			30000	46 0.494 0.444 47 0.444 1.000 46 0.444 1.000		-22653	33555	22222		68666	55555		88888	88888	9695				*****		10000	
	50 0 020 0.010 0.0	000 1 1000 1 1000 1	1.000 1.000 1.000 1.000 1.000 1.000	0.000 1.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.981 0.985	0.978 0.988 0.988 0.993 0.998 0.993 0.985 0.993	0.000 0.000	77 0.948 0.993 0.495 77 0.928 0.993 0.995 81 0.991 0.995 0.995 83 0.992 0.998 0.998 74 0.988 0.998 0.998	0.972 0.980 0.972 0.980 0.973 0.980 0.975 0.970	0.67% 0.41% 0.82% 0.8%5 0.77% 0.4%3 0.77% 0.4%3	0.773 0.856 0.573 0.419 0.475 0.419 0.475 0.419	0.771 C.834 0.770 0.837 0.816 0.831 0.824 0.880	0.450 0.405	0.000 0.000 0.000 0.000 0.000 0.000	1.000	1.000	0.446 0.446	00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00	20000	2000 CO.	******	0.473 0.445 0.473 0.445 0.473 0.444	0.959 0.972	0.22 0.45		
	UPR CA.)	4444	00001	0.457 0.456 0.457 0.456 0.455 0.402		0.013 0.025		6.44 0.965 6.445 0.965 6.945 0.946 6.951 0.976	0.405 0.438 0.801 0.924 0.810 0.972 0.709 0.752	0.187 0.016 0.187 0.016 0.112 0.151	0.34 0.75 0.75 0.75 0.75 0.75 0.75 0.75	0.397 0.527 0.397 0.527 0.507 0.627	0.557 0.700 0.714 0.741 0.657 0.677 0.685 0.927 0.717 0.543	0.974 0.986 0.992 0.992 0.993 0.955 0.995 0.995	0.001	700000	0.482 0.990 0.482 0.990 0.47 0.485 0.47 0.485	0.955 0.966 0.965 0.965 0.971 0.985 0.988 0.983	53377	0.451 0.475	0.00	0.451 0.417 0.838 0.451 0.839 0.461	11111 11111 11111 11111 11111 11111 1111	2000 2000 2000 2000 2000 2000 2000 200	0.550 0.700 0.700 0.500 0.700 0.500 0.700 0.500 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700 0.700	25.25
	<b>700</b>	0 C.950 0.978		10000	1 C. 834 C. 834 C. 754 C. 754 C. 755 C. 755		2222		12525	22022	20015	12224	11161				74356	27722			3333	7 C.814 0.879 7 C.814 0.879 8 C.827 0.808 8 C.673 0.756			2 C.240 0.413 2 C.240 0.413 2 C.240 0.340 5 C.140 0.340	12000
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	UPR CA)	0.500 0.200 0.100	0.525 C.674 0.614 0.525 C.674 0.762 0.410 C.576 0.482 0.443 C.602 0.702 0.539 0.682 C.766	0.542 0.664 0.786 6.638 0.752 0.825 0.643 0.752 0.825 0.602 0.730 0.824 0.602 0.738 0.854	0.780 C.858 D.895 0.784 C.854 0.895 0.618 C.854 0.918 0.852 C.907 0.918 0.854 C.895 0.926	0.889 C.537 0.933 0.943 C.537 0.993 0.943 0.944 0.978 C.973 0.985 0.991 C.986 C.985 0.991	0.494 0.494 0.994 0.491 0.996 0.994 0.495 0.494 0.994 0.495 0.497 0.994 0.494 0.496 0.994	0.998 0.998 0.999 0.998 0.999 0.999 0.599 1.000 1.000 0.994 1.000 1.000 0.994 0.999 1.000	0.593 C.948 0.955 0.592 C.996 0.955 0.989 C.994 0.987 0.585 C.994 0.987	0.984 0.491 0.445 0.586 0.992 0.485 0.567 0.982 0.985 0.956 0.972 0.983	C.93C C.97C C.94C C.937 C.942 O.974 C.939 C.963 O.974 D.913 C.949 C.925 C.913 C.945 C.962	0.513 C.559 0.925 0.915 C.552 0.975 0.615 C.555 0.925 0.545 C.555 0.975 0.545 0.955 0.975	0.533 0.532 0.985 0.503 0.573 0.985 0.505 0.573 0.987 0.505 0.541 0.987	0.547 0.010 0.081 0.028 0.057 0.017 0.019 0.052 0.007 0.019 0.051 0.067	0.680 0.926 0.950 0.781 0.657 0.699 0.910 0.932 0.959 0.910 0.935 0.958	0.675 0.922 0.947 0.675 0.922 0.947 0.693 0.934 0.956 0.925 0.936 0.956 0.925 0.936 0.976	0.543 0.963 0.983 0.554 0.974 0.983 0.561 0.977 0.583 0.541 0.977 0.785 0.572 0.984 0.985	0.975 0.985 0.990 0.976 0.988 0.991 0.980 0.988 0.993 0.983 0.990 0.994 0.990 0.994	0.449 0.440 0.444 0.449 0.449 0.949 0.449 0.449 1.000 0.449 1.000 1.000	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 0.999 1.000 1.000 0.990 0.999 1.000 0.990 0.999	0.595 C.998 0.444 0.496 C.998 0.918 0.486 C.993 0.918 C.583 C.991 0.994	0.982 0.995 0.494 0.986 0.993 0.496 0.976 0.977 0.995 0.972 0.944 0.995	0.976 0.947 0.992 0.977 0.987 0.992 0.985 0.993 0.998				
7	, moog	5,000 2,000 1,000	C. 34 0.461 C. 241 0.244 C. 154 0.276 C. 169 0.216 C. 285 0.413	0.24 0.15 0.15 0.15 0.15 0.15 0.15 0.15		C. 25 0.65 C. 25 C	000000	00.44	C. 531 D. 541 C. 541 D. 541 C. 541 D. 541 C. 571 D. 583		C. C	223000	25555	2222	2000 2000 2000 2000 2000 2000 2000 200	200	35555	55555 5555 5555 5555 5555 5555 5555 5555	20000	20000	0.554 0.595 0.595 0.595 0.595 0.595 0.595 0.595	00000	.412 C.554 0.573 .412 C.544 0.541 .412 C.544 0.541 .416 C.520 0.544	*****				
	AVERAGED OVER	FREG. 50.00 20 00 10.00	40.0 (12.1 5.01) 10.0 (12.1 5.01) 10.0 (12.2 5.01) 10.0 (12.2 5.01)	6.00 (.01 0.03 0.01 (.05 0.120 0.01 (.05 0.130 0.01 (.01 0.03)	C.(51 C.162 0.212 C.(35 C.135 G.202 0.(71 C.227 0.304 0.104 C.202 C.432 0.104 (.261 0.404	0.145 C.315 0.462 0.288 C.465 0.350 0.215 C.465 C.358 0.677 C.398 0.658 0.178 C.465 0.510	0.171 (.473 0.516 0.426 (.473 0.516 0.482 (.512 0.534 0.482 (.513 0.534 0.517 (.525 0.534	6.191 C.542 0.564 C.535 C.564 0.574 C.555 C.566 0.586 G.55 C.575 C.588 G.545 C.575 C.588	C.525 C.546 C.515 0.504 C.544 0.582 0.641 C.525 C.531 0.642 C.501 0.534 0.605 C.875 0.536	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.135 C.484 0.335 0.472 C.432 0.335 0.486 C.441 0.334 0.431 C.581 0.485	6.15 (.65 0.22 6.16 (.65 0.33 6.48 (.65 0.36 6.10 (.65 0.36	0.17 C.705 0.787 0.614 C.735 C.605 C.658 C.765 0.478 C.647 C.765 0.478 C.544 C.705 0.478	6.44 C.63 6.74 6.43 C.51 6.64 6.74 C.51 6.64 6.74 C.51 6.65	0.25 C.13 C.51 C.51 C.15 C.15 C.15 C.15 C.15 C.15	0.24C C.41S D.348 0.212 C.38C 0.317 0.275 C.452 0.574 0.413 C.374 C.278 0.40C C.635 C.278	0.1461 C.434 C.729 C.145 C.485 C.775 G.124 C.735 G.657 G.191 C.726 G.455 G.144 C.786 G.455	0.298 C.202 D.668 C.316 C.615 C.674 C.348 C.662 D.691 O.384 C.662 C.508 C.633 C.51C O.534	0.491 (.5)4 0.595 0.517 (.550 0.56 0.543 (.563 0.59 0.557 (.574 0.562 0.573 (.594 0.562	0.184 (.592 0.595 0.594 (.593 0.568 0.591 (.593 0.595 0.586 (.592 0.595 0.584 (.592 0.595	C. CAC C. CA. D.	0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60		0.141 (-55)				
RESSURE	∢	0.003 0.003 0.001	99999	66666	88888				******	0.44% 0.40% C.44% 0.40% 0.44% C.44% 0.40% C.40% C.40% 0.40% C.40% C.40%		25.000	\$55.55	10000	86668	88555	20000	99999	.0000	99559			0.498 0.400 1.000 0.448 0.440 1.000 0.490 0.440 0.540 0.403 0.441 0.540		0.416 0.487 0.542 0.481 0.491 0.595 0.481 0.491 0.495 0.481 0.491 0.595		0.445 0.486 0.474 0.416 0.412 0.482 0.438 0.464 0.477 0.874 0.423 0.449 0.874 0.437 0.459	
STACKE P		0.050 0.020 0.010	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	88888	33955			*****		0.479 0.489 0.993 0.477 0.487 0.492 0.474 0.985 0.491 0.452 0.74 0.988 0.438 0.444 0.477	*****	22333	55155	7777	10000	55555	9998		*****		*****	*****	1555		0.912 0.944 0.444 0.929 0.457 0.975 0.939 0.445 0.975 0.931 0.441 0.973 0.927 0.936 0.471	77775	0.819 0.885 0.920 0.833 0.845 0.928 0.789 0.846 0.908 0.631 0.732 0.822 0.711 0.805 0.838	
	nea.cw.	0.500 0.200 0.100	******	1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000		0.952 0.971 0.980 0.943 0.945 0.976 0.944 0.945 0.978 0.944 0.945 0.978		*****	0.455 G.412 G.481 0.453 O.412 G.481 0.456 G.576 G.984 0.559 Q.417 G.985 0.443 G.984 G.978		C.68 C.73 C.855 C.60 C.73 C.804 C.503 C.655 C.74 C.404 C.574 C.681 O.360 C.574 C.681	C-119 C-101 0.702 C-131 C-102 C-707 C-216 C-775 C-101 C-215 C-715 C-101 C-115 C-612 0.712	0.492 0.450 0.745 C.451 0.616 0.718 C.441 0.656 0.705 C.504 0.656 0.747 0.605 0.735 0.608	C-776 C-621 D-672 G-629 C-690 G-92 G-603 G-919 G-92 C-649 C-915 C-961	0.984 C.395 0.947 0.992 C.998 0.945 0.992 C.998 0.449 0.496 C.998 0.649 C.496 0.999 L.000	0.599 1.060 1.000 0.599 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	1.000 1.000 1.000 0.594 0.959 1.000 0.595 0.998 0.998 0.592 0.998 0.998	C.986 C.988 D.492 D.981 D.481 D.493 C.995 C.981 D.993 C.933 C.985 D.996 O.934 C.974 O.484	6.469 0.428 0.486 6.473 6.484 0.446 6.475 0.483 0.446 0.438 6.438 6.485	0.459 0.441 0.488 0.459 0.417 0.480 0.943 0.469 0.881 0.928 0.961 0.97¢ 0.937 0.962 0.981	0.424 C.441 0.474 C.417 C.455 C.474 C.404 C.447 0.444 0.475 C.441 0.444	0.929 0.981 0.976 0.931 0.981 0.978 0.934 0.975 0.982 0.951 0.972 0.982	0.954 0.914 0.483 0.412 0.444 0.417 0.403 0.441 0.441 0.872 0.420 0.448	0.411 0.403 0.413 0.411 0.405 0.413 0.144 0.405 0.415 0.749 0.405 0.404	0.734 C.423 C.673 0.779 C.457 0.695 0.604 C.474 0.413 C.785 C.444 G.906 0.787 C.650 C.894	0.725 C.821 C.874 0.435 C.800 D.858 0.458 C.770 D.834 0.450 G.731 D.820 0.560 G.713 0.791	0.512 0.040 0.749 0.532 0.619 0.746 0.449 0.609 0.705 0.223 0.391 0.517 0.388 0.523 0.623	
₹ ₹	•	5.000 2.000 1.000	0.923 C.534 G.584 0.923 C.532 G.588 0.932 G.536 G.493 0.934 G.481 G.493 d.934 G.484 G.593	0.462 0.490 0.597 0.482 0.592 0.994 0.472 0.593 0.594 0.473 0.594 0.599	0.472 C.543 0.448 0.472 C.546 0.545 0.441 C.544 0.541 0.841 C.544 0.546	92111	23333	0.772 C.E.7 G.E88 C.E13 C.E82 O.517 C.772 C.E53 D.E95 O.E02 G.773 D.911	*****	15555	25.75		*****						33555			11055	55955	0.485 0.444 0.781 0.547 0.444 0.738 0.547 0.404 0.738 0.515 0.444 0.732 0.424 0.563	0.165 0.532 0.643 0.485 0.394 0.643 0.48 0.639 0.239 0.448 0.659 0.209	0.333 0.310 6.628 0.284 6.484 0.591 0.284 6.436 0.531 0.272 6.395 0.519 0.177 6.233 0.461	0.115 C.234 D.384 D.117 C.344 D.402 O.017 C.118 D.314 O.011 C.635 D.125 C.105 D.265 D.272	
WAIEK VAPO		FEEG. 50.00 20.00 10.00	415.0 0.374 C.415 G.623 4135.0 C.433 C.316 G.648 4200 G.435 C.316 G.648 4235.0 C.328 C.373 G.883 4230.0 C.531 C.606 G.603				0.11 C.021 0.11 C.021 0.12 C.021 0.12 C.021	0.199 C.585 0.691 0.435 C.626 E.335 7.98 C.535 0.686 0.456 C.432 0.686	0.49) C.475 C.334 0.401 E.463 0.748 0.304 C.444 C.388 0.301 C.484 C.388 0.418 (.612 0.344	0-115 C-114 C-142 0-284 C-1445 O-103 0-225 C-431 C-133 0-116 C-313 C-134 0-105 C-317 C-294	6.03 6.03 6.73 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00	7070 1070 1070 7070 1070 1070 7070 1070 1	0.00 C.00 C.013 0.00 C.00 C.013 0.00 C.00 C.013 0.00 C.00 C.013 0.00 C.00 C.013	C. C	100 CO	C.495 C.486 D.581 C.504 C.541 D.545 C.524 C.541 D.545 C.511 C.544 D.502 C.511 C.544 D.502	6.537 (.515 6.54) 6.525 (.511 6.54) 6.504 (.531 6.54) 6.414 (.522 6.53)	6.781 C.654 G.699 6.786 C.666 D.507 C.645 C.614 D.634 C.643 C.641 D.634	0.10¢ (.791 0.444 0.133 (.624 0.674 0.491 (.795 0.657 0.424 (.714 0.614 0.405 (.771 0.604	0.207 (.734 0.211 0.227 (.481 0.370 0.461 (.420 0.318 0.392 (.361 0.688 0.412 (.357 0.688	6.36. C.33. 6.43 6.39. C.33. 6.44 6.34. C.34. 6.43 6.37. C.44. 6.35 6.34. C.33. 6.43	0.31 C.51 0.63 C.59 C.51 0.67 C.41 C.60 C.710 C.48 C.61 0.73	0.115 C.Eff 6.165 0.443 C.465 G.107 0.183 C.465 C.168 0.195 C.361 0.104 0.195 C.361 0.100	0.134 C.284 0.421 0.084 C.214 0.350 0.147 C.301 0.440 0.125 C.273 0.358 C.C72 C.375 0.358			7155.0 6.001 6.01 0.01 7155.0 0.00 6.00 0.02 7255.0 0.00 6.00 0.02 7255.0 0.00 6.00 0.02	
		0 003 0 002 0.001	1.000 1.000 1.00 1.000 1.000 1.00 1.000 1.000 1.00 1.000 1.000 1.00			76333	0,74 C.011 C.05 0,74 C.011 C.05 0,74 C.010 G.07 0,01 C.010 C.07 0,01 C.010 0.01 0,012 C.00 0.01	0.725 0.817 0.88 0.642 0.795 0.850 0.796 0.827 0.625 0.786 0.899 0.899 0.848 0.40, 0.432	0.41) C.900 C.531 0.410 G.938 C.531 0.901 G.941 C.411 0.901 G.911 G.911 0.931 G.917 G.940	0.938 0.934 0.932 0.935 0.933 0.932 0.935 0.938 0.993 0.938 0.938 0.993	0.010 C.115 C.117 0.013 C.116 C.118 0.015 C.116 C.118 0.016 C.118 C.118	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 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## APPENDIX E

WATER VAPOR TRANSMISSIONS AVERAGED OVER 100 cm⁻¹
WITH ENTRIES EVERY 50 cm⁻¹ FOR FREQUENCIES FROM
1000 cm⁻¹ TO 10,000 cm⁻¹ AT 300°K, 250°K, AND 200°K

	AVERAGED OVER 100cm ⁻¹ WINTCAL  FIRE, 55.00 26.00 15.00 5.000 26.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00 15.00	2000 0200 0200 0400 0400 0400 0400 0400	
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	T=300° K upa.cm.) 0 0.500 0.700 0.100		•
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AVERAGED OVER 100cm	~		
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	5 000 2.000 1.000	0.484 0.494 0.494 0.427 0.491 0.494 0.427 0.491 0.494 0.431 0.424 0.494	11100	66666	22.72	****	*****	<b>#</b>	17111	20000	22122	200000	20000	19774	*****	20100	22222	24550	55555		25111	*****	22484	11111	1378 0.540 0.544 1317 0.481 0.594 1317 0.481 0.594 1317 0.480 0.820	22222
	PREG. 50.00 70,00 10.00	12224	0.056 0.194 0.335 0.011 0.054 0.113 0.000 0.002 0.010 0.000 0.000 0.000	0000 0 000 0 000 0 0000 0 000 0 000 0 0000 0 000 0 000 0 0000 0 000 0 000 0	0.000 0.000 0.002 0.000 0.000 0.002 0.000 0.001 0.010 0.001 0.022 0.075 0.014 0.104 0.22	0.180 0.252 0.411 0.180 0.413 0.574 0.332 0.577 0.717 0.489 0.724 0.838 0.613 0.820 0.404	0.732 0.842 0.942 0.732 0.893 0.942 0.751 0.908 0.903 0.744 0.919 0.973	0.748 0.404 0.465 0.480 0.451 0.425 0.410 0.783 0.878 0.480 0.473 0.778 0.784 0.547 0.710	0.102 0.414 0.725 0.410 0.435 0.753 0.356 0.541 0.721 0.200 0.424 0.578 0.085 0.352 0.394	0.011 0.128 0.242 0.007 0.052 0.130 0.018 0.044 0.171 0.017 0.079 0.145	0.002 0.032 0.103 0.004 0.038 0.104 0.004 0.043 0.124 0.000 0.004 0.037	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 6.000 0.000 0.000 6.000 0.000 0.000 6.000 0.000 0.000 6.002 0.013	0.024 0.187 0.192 0.078 0.144 0.582 0.152 0.481 0.680 0.239 0.551 0.734 0.329 0.444 C 410	0.485 0.737 0.857 0.485 0.759 0.878 0.524 0.780 0.888 0.509 0.753 0.461 0.377 0.415 0.741	0.291 0.524 0.445 0.251 0.462 0.594 0.259 0.450 0.577 0.279 0.440 0.617 0.256 0.477 0.615	0.241 0.451 0.589 0.310 0.524 0.634 0.354 0.374 0.710 0.325 0.550 0.447 0.250 0.445 0.607	0.130 0.318 0.433 0.056 0.174 0.303 0.008 0.043 0.301 0.000 0.001 0.021	0.000 0.000 0.000 0.000 0.000 0.001 0.000 0.000 0.001 0.000 0.000 0.001 0.001 0.017 0.033	0.000 0.174 0.279 0.261 0.408 0.600 0.528 0.732 0.833 0.647 0.858 0.425 0.756 0.814 0.446	0.010 0.917 0.017 0.061 0.914 0.00 0.068 0.912 0.00 0.024 0.910 0.914 0.721 0.041 0.00	0.714 C.034 C.887 C.659 C.777 C.837 C.587 C.721 C.702 C.582 C.720 C.751 C.494 C.657 C.751	0.203 0.494 0.404 0.203 0.494 0.404 0.284 0.493 0.374 0.224 0.392 0.304	0.377 0.463 0.391 0.348 0.328 0.469 0.348 0.333 0.433 0.218 0.383 0.311 0.081 0.214 0.344	0.054 0.187 0.310 0.034 0.137 0.250 0.025 0.005 0.184 0.020 0.095 0.194	0.00 0.02 0.03 0.03 0.00 0.00 0.00 0.00

WATER VAPOR AT 0.20 ATMOSPHERE PRESSURE

	UPR.CAL) 0,300 0,700 0,100 0,030 0,030 0,010 0,903 0,002 0,003																									
AVERAGED OVER-100cm1	000'1 000'E.000'S 00'01 00'D																									
WATER VAPOR AT 0.05 ATMOSPHERE PRESSURE T=200°K	100'0 200'0 500'0 010'0 020'0 050 0 00'0 00'0 00'0 00'1 000'1 000'1 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 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00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'0 00'		001 001 001 001 001 001 001 001 001 001		0.10 C-10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0		0.00 0.77 0.00 0.00 0.00 0.00 0.00 0.00	0.011 0.013 0.047 0.046 0.041 0.046 0.041 0.046 0.047 0.046 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 0.044 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Space Systems Division, Air Force Systems Command, Los Angeles, California

Rpt. No. SSD-TDR-62-127 - Volume II. INFRARED TRANSMISSION STUDIES, VOLUME II: THE INFRARED ABSORPTION OF WATER

Final Report, Volume II, 20 September 1962

249 p., incl. tables and illus.

Unclassified Report

The infrared absorption of water vapor has been calculated over a wide range of path length, pressure, and temperature from 1000 to 10,000 cm $^{-1}$ . The results are presented in extensive tables which give the transmission over intervals of 2.5 cm $^{-1}$  at wave numbers below 3400 cm $^{-1}$ . The average transmission over intervals of 2.9, 50, and 100 cm $^{-1}$  is given over the complete frequency range. The calculated data representing the intensity, position, and number of spectral lines in a given frequency interval is tabulated in a form which is useful for transmission calculations. All lines

Unclassified Abstract

- 1. Absorption
- 2. Water Vapor
- 3. Infrared Spectroscopy
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from all isotopic species having an intensity greater than  $10^{-8}$  of the strongest line in an absorption region were included in the calculation. The quasi-random model for the representation of band spectra is discussed in detail. Among its features are the possibility of representing the absorption by a series of lines which are arranged neither at random nor in a regular way.

Unclassified Abstract

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